DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA

OFFICE OF DESIGN POLICY & SUPPORT INTERDEPARTMENTAL CORRESPONDENCE

FILE P.I. # 132986-

OFFICE Design Policy & Support

BRST0-0189-01(030)

Gwinnett County

GDOT District 1 - Gainesville

DATE May 12, 2016

SR 120/Duluth Hwy @ Singleton Creek

Bridge Replacement

FROM

for Brent Story, State Design Policy Engineer

TO SEE DISTRIBUTION

SUBJECT APPROVED REVISED CONCEPT REPORT

Attached is the approved Revised Concept Report for the above subject project.

Attachment

DISTRIBUTION:

Hiral Patel, Director of Engineering

Joe Carpenter, Director of P3/Program Delivery

Genetha Rice-Singleton, Assistant Director of P3/Program Delivery

Albert Shelby, State Program Delivery Engineer

Darryl VanMeter, State Innovative Delivery Engineer

Bobby Hilliard, Program Control Administrator

Cindy VanDyke, State Transportation Planning Administrator

Eric Duff, State Environmental Administrator

Bill DuVall, State Bridge Engineer

Andrew Heath, State Traffic Engineer

Angela Robinson, Financial Management Administrator

Lisa Myers, State Project Review Engineer

Charles "Chuck" Hasty, State Materials Engineer

Lee Upkins, State Utilities Engineer

Richard Cobb, Statewide Location Bureau Chief

Brent Cook, District Engineer

Brandon Kirby, District Preconstruction Engineer

Robby Oliver, District Utilities Engineer

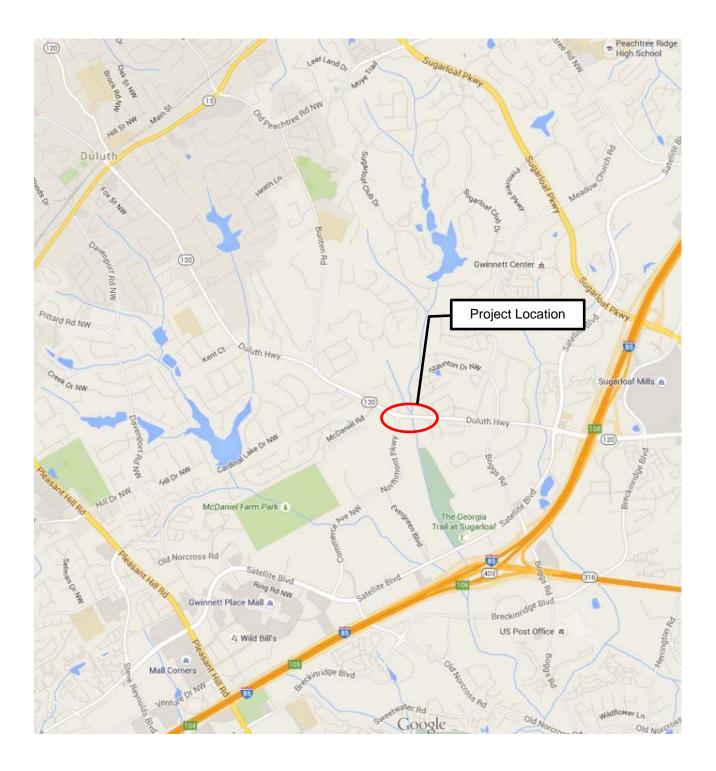
Anthony Tate, Project Manager

BOARD MEMBER - 7th Congressional District

DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA PROJECT CONCEPT REPORT

Project Type: Bridge Replacement	P.I. Number:	132986
GDOT District: 1	County:	Gwinnett
Federal Route Number: N/A	State Route Number:	120
Project Number:	N/A	
•		•
The project consists of the replacement of the SR 120	bridge over Singleton Creek	to the south of the
existing structure as well as 0.4 miles of realignment		
Submitted for approval:		
	hael Baker International, Inc.	1/2-1-11
e can		1/27/2016
Consultant Designer & Firm		Date
albert V. Shills		3.1.16
State Brogram Delivery Engineer		Date
11	*	9/11/11
Anthour 100		9/0/16
GDOT Project Mariager		Date
Recommendation for approval:		
* Evil Dugg /VIP		3-17-16
State Environmental Administrator		Date
VI CI - I I I	1	2-211 11
Christopher Kaymond	IKLE	5-29-16
State Traffic Engineer		Date
* Lisa MUERS		3-18-16
Project Review Engineer		Date
G. C.	•	
Canal Hallan - F		D.A.
State Utilities Engineer		Date
District Engineer		Date
K Bill DuVall		4-22-16
State Bridge Engineer	7	Date
Cizio Diluge Eligineei		Date
MPO Area: This project is consistent with the	MPO adopted Regional Trans	sportation Plan
(RTP)/Long Range Transportation Plan (LRTF)).	Parmatti mi
Rural Area: This project is consistent with the	ē ·	a Transportation Diag
(SWTP) and/or is included in the State Transp		
Oi 14 and on a mondadd in the diate mainsp	ortagon improvement i rogian	
Conflue & VaiRRe		3-21-16
State Transportation Planning Administrator		Date
U		
	PI	
* Recommendations on	TilP	
VER REPERINGUITIFICITIES CONTINUES	1116	

PROJECT LOCATION MAP



PLANNING AND BACKGROUND

Project Justification Statement:

The bridge on SR 120 (Duluth Highway) over Singleton Creek, Structure ID 135-0023-0, was built in 1938. The original bridge consists of three spans of steel beams on concrete caps and concrete columns. This bridge was designed using an H-15 vehicle, which is below current design standards. The overall condition of this bridge would be classified as satisfactory. The deck is in fair condition with the concrete edge beams exhibiting cracking and spalling throughout the structure. The superstructure is in good condition. The substructure is in satisfactory condition with minor concrete deterioration consisting of cracking and spalling of the concrete cap at bent 2 and abutment 4. The bridge is classified as having an unknown foundation and therefore could be at risk for scour. Due to the structural integrity of the bridge pertaining to the design vehicle, deterioration of the edge beams throughout the structure and the unknown foundation of the substructure, replacement of this bridge is recommended.

Existing conditions:

Existing SR 120 consists of two 12-foot lanes with variable width paved shoulders. Left and right turn lanes provided at the existing intersections. The existing bridge over Singleton Creek consists of two 12-foot lanes with no shoulders. There is a signalized intersection of SR 120 and Northmont Pkwy 450 feet west of the existing bridge. There is existing sidewalk to the east and west of the bridge. Overhead electric transmission lines and a gas line are located on the south side of the road through the project corridor. A sanitary sewer line follows Singleton Creek perpendicular to SR 120. The north side of the bridge is protected under a restrictive covenant by the Corps of Engineers and cannot be impacted without significant costs and impacts to the schedule.

Other projects in the area: None							
MPO: Atlanta Regional	Commission (A	ARC)					
TIP # : GW-290							
TIA Regional Commis	ssion: Atlanta R	egional Comm	ission				
Congressional Distric	ct(s): 7						
Federal Oversight:	□ PoDI	⊠ Exempt	☐ State Funded	☐ Other			
Projected Traffic: ADT 24 HR T: 8 % Current Year (2015): 25,300 Open Year (2020): 26,600 Design Year (2040): 32,450 Traffic Projections Performed by: Michael Baker International, Inc., Approved 8/14/2015 Functional Classification (Mainline): Urban Minor Arterial Street							
Complete Streets - Bicycle, Pedestrian, and/or Transit Standard Warrants:							
Warrants met:	□ None	⊠ Bicycle	□ Pedestrian	☐ Transit			
Bicyle Warrants – The corridor includes bicycle generators including residential development. The project is a new bridge. Pedestrian Warrants - The corridor inludes pedestrian generators including residential neighborhoods. Transit Warrants – The route is not located along a transit corridor per Gwinnett County transit maps.							
Is this a 3R (Resurfac	ing, Restoratio	n, & Rehabilit	ation) Project?	No ☐ Yes			

Pavement	Evaluation	and	Recommen	dations
I avcilicit	L valuation	ana		uations

Initial Pavement Evaluation Summar	y Report Required?		□ No	
Intial Pavement Type Selection Repo	ort Required?	\boxtimes No	☐ Yes	3
Feasible Pavement Alternatives:	\bowtie HMA		□ H	MA & PCC

DESIGN AND STRUCTURAL

Description of the proposed project:

The project consists of replacement of the existing SR 120 bridge over Singleton Creek. The total project length is 0.4 miles. The project is located in Gwinnett County, 1.2 miles east of the City of Duluth. The new bridge will include two 12' lanes plus a center turn lane and sidewalks for pedestrians.

Major Structures:

Structure	Existing	Proposed
135-0023-0	75 feet long, 26.5 foot wide deck with	150 foot long bridge with three 50-foot
SR 120 over	two 12 foot lanes and no shoulder.	spans. The total width is 63.42-foot
Singleton Creek	Suffieciency rating of 58.7 per	including two 12-foot travel lanes and
	inspection dated 1/31/2014.	a 14-foot center turn lane with 2-foot
		gutters and 5.5-foot raised sidewalks.

Mainline Design Features: SR 120 - Urban Minor Arterial

Feature	Existing	Standard*	Proposed
Typical Section			
- Number of Lanes	2	4	2
- Lane Width(s)	12-ft	11-12-ft	12-ft
- Median Width & Type	None	24-ft Raised	14-ft Flush
- Outside Shoulder or Border Area Width	Varies	10-16-ft	16-ft
- Outside Shoulder Slope	Vaires	2%	2%
- Inside Shoulder Width	N/A	N/A	N/A
- Sidewalks	5-ft	5-ft	5-ft
- Auxiliary Lanes	Left & Right turn	None	Left & Right turn
	lanes		lanes
- Bike Lanes	None	None	4-ft
Posted Speed	45 mph		45 mph
Design Speed		45 mph	45 mph
Min Horizontal Curve Radius	1650	711	2000
Maximum Superelevation Rate	6%	4%	6%**
Maximum Grade	6.3%	7%	6.3%
Access Control	By Permit	By Permit	By Permit
Design Vehicle		WB-40	WB-40 (Min)***
Pavement Type	Ashpalt		Ashpalt

^{*}According to current GDOT design policy if applicable

SR120 @	Northmont Pkwv -	Existing S	ignalized l	Intersection

	Lighting r	eguired:	⊠ No	☐ Yes
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^{** 6%} SE rate will be used to match existing. 4% will be used on all new location areas.

^{***} Turning movements for WB-67 will be analyzed to/from SR 120 to Northmont Pkwy south due to the number of industrial businsess located in this area.

Off-site Detours Anticipated: ⊠ No □ Yes □ Undetermined							
Transportation Management Plan [TMP] Required: □ No □ Yes If Yes: Project classified as: □ Non-Significant □ Significant							
TMP Components Anticipated: ⊠ TTC □ TO □ PI							
Design Exceptions to FHWA/AASHTO c	ontrolling criter	ia antic	ipated:				
Undeter- Appvl Date							
FHWA/AASHTO Controlling Crite		m			(if applicable)		
1. Design Speed							
2. Lane Width							
3. Shoulder Width		_					
4. Bridge Width							
5. Horizontal Alignment							
6. Superelevation							
7. Vertical Alignment							
8. Grade							
Stopping Sight Distance							
10. Cross Slope							
11. Vertical Clearance							
12. Lateral Offset to Obstruction	\boxtimes						
13. Bridge Structural Capacity	\boxtimes						
Design Variances to GDOT Standard Cr		<u>d:</u>	11 14	ı			
GDOT Standard Criteria	Reviewing	No	Undeter-	Vas	Appvl Date		
GDOT Standard Criteria 1. Access Control/Median Openings	Office	No 🖂	mined	Yes	Appvl Date (if applicable)		
1. Access Control/Median Openings	Office DP&S	\boxtimes	mined				
 Access Control/Median Openings Intersection Sight Distance 	Office DP&S DP&S		mined				
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle 	Office DP&S DP&S DP&S		mined				
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction 	Office DP&S DP&S DP&S DP&S DP&S		mined				
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips 	Office DP&S DP&S DP&S DP&S DP&S DP&S		mined				
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge 	Office DP&S DP&S DP&S DP&S DP&S		mined				
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage 	Office DP&S DP&S DP&S DP&S DP&S DP&S DP&S DP&S		mined		(if applicable)		
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage Roundabout Illumination Levels 	Office DP&S DP&S DP&S DP&S DP&S DP&S DP&S DP&S		mined		(if applicable)		
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage Roundabout Illumination Levels Complete Streets 	Office DP&S DP&S DP&S DP&S DP&S DP&S DP&S DP&S		mined		(if applicable)		
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 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage Roundabout Illumination Levels Complete Streets ADA & PROWAG GDOT Construction Standards GDOT Drainage Manual 	Office DP&S DP&S		mined		(if applicable)		
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage Roundabout Illumination Levels Complete Streets ADA & PROWAG GDOT Construction Standards 	Office DP&S		mined		(if applicable)		
 Access Control/Median Openings Intersection Sight Distance Intersection Skew Angle Lateral Offset to Obstruction Rumble Strips Safety Edge Median Usage Roundabout Illumination Levels Complete Streets ADA & PROWAG GDOT Construction Standards GDOT Drainage Manual GDOT Bridge & Structural Manual Note: A flush median is used for SR 120 be	Office DP&S DP&S DP&S DP&S DP&S DP&S DP&S DP&S	X X X X X X X X X	mined	ojects ar	See note below e programmed to		
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Railroad Involvement: None

Utility Involvements: Georgia Power Distribution— Electric AT&T (Transmission and Distribution) — Telecommunications Atlanta Gas Light — Gas Gwinnett County Department of Water Resources — Water & Sewer Charter — Telecommunications Jackson EMC — Electric Level 3 — Telecommunications Zayo Telecom - Telecommunications								
SUE Required:	□ No	⊠ Yes	☐ Undetermined					
Public Interest Detern	nination Policy	and Procedure	recommended?	☑ No	☐ Yes			
Right-of-Way (ROW): Required Right-of-Way Easements anticipated:	anticipated:	☐ None	⊠ Yes □	width: 100-19 Undetermine Other				
	Anticipated Displacements	anticipated:	impacted parcels: Businesses: Residences: Other: al Displacements:	0 0 0				
Location and Design a	approval:	☐ Not Required	d ⊠ Require	ed				
Impacts to USACE pro	operty anticipat	ed? □ No		ermined				
ROUNDABOUTS None								
CONTEXT SENS Issues of Concern: N		UTIONS						
Context Sensitive Sol	utions Propose	d: None						
ENVIRONMENT Anticipated Environm GEPA: □	ental Documen		□ EA/FONSI	□ EIS				
MS4 Permit Complian As outlined in the attack reduction in total paven drainage area 5 is locat construction without im which can be located w included in the construction	ned MS4 Concept nent area, meanined directly adjact pacts to those profithin the existing	ot Layout, of the fing no post constitution to a townhor operties. Drainate R/W on the nort	five identified draina ruction BMPs will b ne neighborhood an ge Area 3 will requ	ne required. A nd would not p ire post constr	fourth area, ermit uction BMPs			
Environmental Bermit	o/Varianasa/Ca	mmitmonto/Coo	rdination anticina	.4ad.				

	nvironnentai Pennis/variances/commitments/coordination anticipated.						
Ρ	ermit/ Variance/ Commitment/ Coordination						
	Anticipated	No	Yes	Remarks			
1.	U.S. Coast Guard Permit	\boxtimes					
2.	Forest Service/Corps Land	\boxtimes					

3. CWA Section 404 Permit		\boxtimes	Wetland impacts				
4. 33 USC 408 Decision	\boxtimes						
5. Tennessee Valley Authority Permit	\boxtimes						
6. Buffer Variance		\boxtimes	Possible for Singleton Creek				
7. Coastal Zone Management Coordination	\boxtimes						
8. NPDES		\boxtimes					
9. FEMA		\boxtimes					
10. Cemetery Permit	\boxtimes						
11. Other Permits	\boxtimes						
12. Other Commitments	\boxtimes						
13. Other Coordination	\boxtimes						
Environmental Comments and Information: NEPA/GEPA: The CE has not been started outside of special studies being completed. No out of the ordinary issues are anticipated. No 4f resources are present in the project corridor. Ecology: An ecology survey has been completed and identified two wetlands and three buffered waters. No suitable habitat was identified for T&E species. An aquatic study has been completed and the determination was that Singleton Creek is not suitable habitat for potentially affected species. The property to the north of the project on either side of Singleton Creek is a wetland preservation area protected under USACOE restrictive covenant no. 2005-01245. History: A historic survey has been conducted of the project corridor and no resources were identified. Archeology: An archaeological survey has been conducted of the project corridor and no resources were identified. Air Quality: Is the project located in a PM 2.5 Non-attainment area? □ No □ Yes Is the project located in an Ozone Non-attainment area? □ No □ Yes Carbon Monoxide hotspot analysis: □ Required □ Not Required □ TBD The project is exempt from the conforming plan because it is a widening of an existing bridge with no change to the number of travel lanes. Noise Effects: A noise impact assessment report (screening) is required. Public Involvement: No formal public involvement is anticipated at this time.							
Major stakeholders: Gwinnett County, City of Duluth, Traveling Public, L CONSTRUCTION	ocal Hor	neowner	s				
ssues potentially affecting constructability/con	structio	n schedu	ule: No issues identified				
Early Completion Incentives recommended for o	consider	ation: 🛭	☑ No ☐ Yes				

COORDINATION, ACTIVITIES, RESPONSIBILITIES, AND COSTS

Initial Concept Meeting: The ICM was held on 6/5/2002 and the CR was first approved on 2/11/2003. The original CR and included ICM meeting minutes are attached. Due to the length of time since the original concept was developed, the changes to the project corridor and the additional requirements of Concept Reports it was decided to complete a new Concept Report instead of a Concept Validation and/or Concept Revision.

Concept Meeting:

The Concept Team Meeting was held on 12/18/2015 at the District 1 Office and the project site. The meeting mintues are attached.

Other coordination to date: None

Project Activity	Party Responsible for Performing Task(s)
Concept Development	Michael Baker International, Inc.
Design	Michael Baker International, Inc.
Right-of-Way Acquisition	GDOT
Utility Coordination (Preconstruction)	Michael Baker International, Inc.
Utility Relocation (Construction)	Utility Companies
Letting to Contract	GDOT
Construction Supervision	GDOT
Providing Material Pits	GDOT
Providing Detours	N/A
Environmental Studies, Documents, & Permits	Michael Baker International, Inc.
Environmental Mitigation	GDOT
Construction Inspection & Materials Testing	GDOT

Project Cost Estimate Summary and Funding Responsibilities:

	Breakdown of PE	ROW	Reimbursable Utility	CST*	Environmental Mitigation	Total Cost
Funded By	GDOT	GDOT	GDOT	GDOT	GDOT	
\$ Amount	\$300,000	\$492,000	\$928,500	\$3,072,019	\$48,280	\$4,840,799
Date of Estimate	3/15/2013	1/14/2016	1/27/2016	4/20/2016	10/21/2015	

^{*}CST Cost includes: Construction, Engineering and Inspection, Contingencies and Liquid AC Cost Adjustment. CE&I of 5% of CES total and Contingency of 10% of CES plus CE&I cost included.

ALTERNATIVES DISCUSSION

Alternative selection:

Preferred Alternative: Replace the bridge to the south of the existing alignment							
Estimated Property Impacts: 10 Estimated Total Cost: \$4,840,799							
Estimated ROW Cost:	\$492,000	Estimated CST Time:	24 months				
Rationale: This alternative meets the project goals by replacing the existing deficient bridge while allowing							
traffic to be maintained on the existing structure							

Project Concept ReportPage 9 County: Gwinnett

No-Build Alternative: The existing bridge will be left in place with no improvements					
Estimated Property Impacts:	None	Estimated Total Cost:	\$0		
Estimated ROW Cost:	\$0	Estimated CST Time:	N/A		

Rationale: The No-Build alternative fails to meet the project need of replacing the existing substandard width bridge.

Alternative 1: Replace the bridge to the north of the existing alignment					
Estimated Property Impacts:	11	Estimated Total Cost:	Not analyzed		
Estimated ROW Cost:	Not analyzed	Estimated CST Time:	24 months		

Rationale: This alternative cannot be accomplished without impacting the property to the north of the existing bridge which is protected by the Corps through a restrictive covenant. This alternative would also impact Intermittent Streams 1 & 4.

Alternative 2: Replace the bridge on the existing alignment						
Estimated Property Impacts:	3	Estimated Total Cost:	Not analyzed			
Estimated ROW Cost:	Not analyzed	Estimated CST Time:	36 months			

Rationale: This alternative would require construction of a temporary detour bridge in order to remove the existing bridge and reconstruct it at the required elevation above the design year flood event. Construction of the temporary paving and bridge would occur generally in the same location as the southern or northern alternative resulting in similar levels of impacts with the additional costs associated with temporary construction.

Comments: None

LIST OF ATTACHMENTS/SUPPORTING DATA

- 1. Concept Layout
- 2. Typical sections
- 3. Detailed Cost Estimates:
 - a. Construction including Engineering and Inspection and Contingencies
 - b. Completed Liquid AC Cost Adjustment forms
 - c. Revisions to Programmed Costs & Contigency Summary
 - d. Right-of-Way
 - e. Utilities
 - e. Environmental Mitigation
- 4. Crash summaries
- 5. Traffic diagrams
- 6. Capacity analysis summary
- 7. Summary of TE Study
- 8. SI&A Report
- 9. Concept Level Hydrology Study for MS4 Permit
- 10. Pavement Study
- 11. Minutes of Concept meetings

APPROVALS

Concur: Highletel

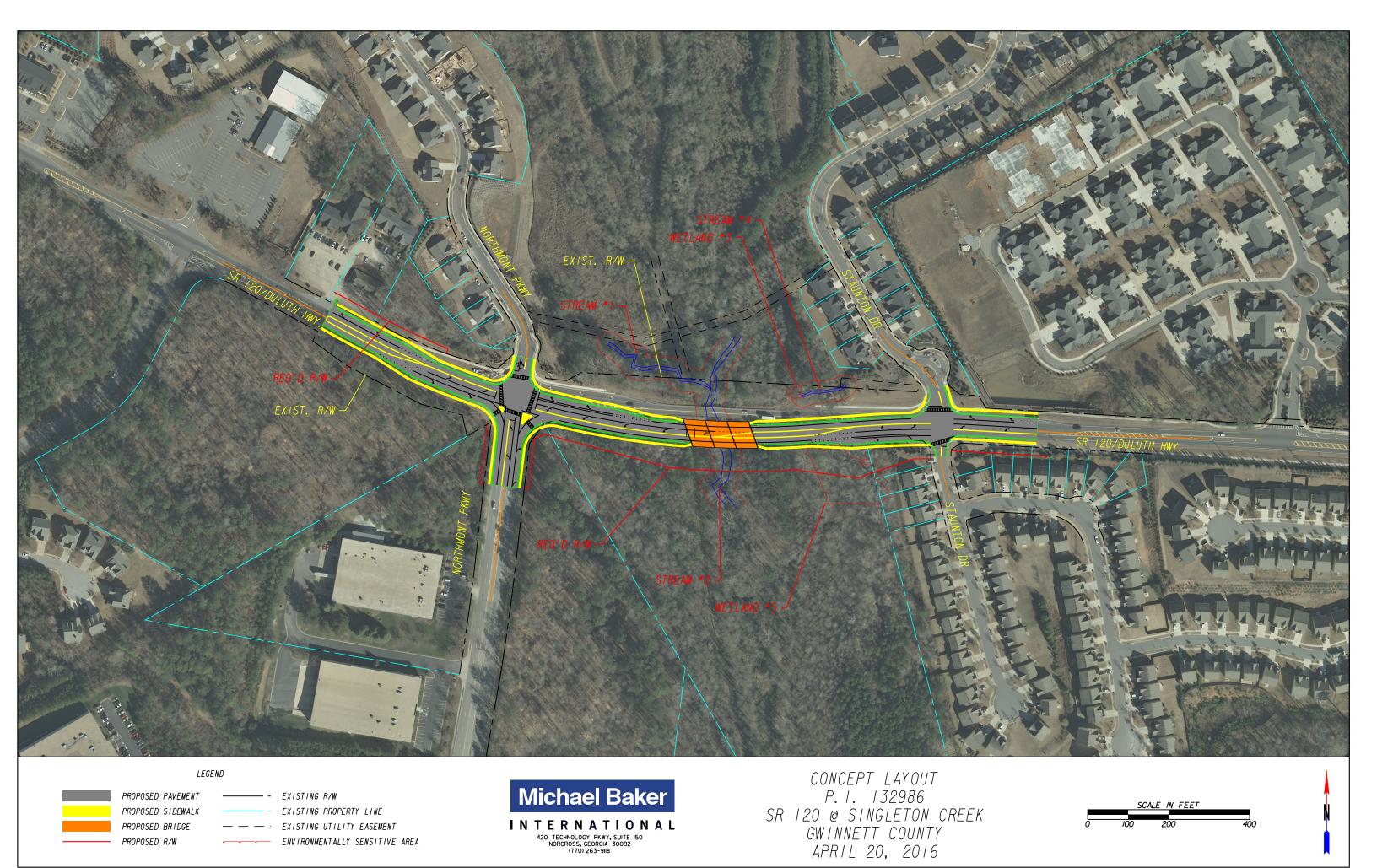
Director of Engineering

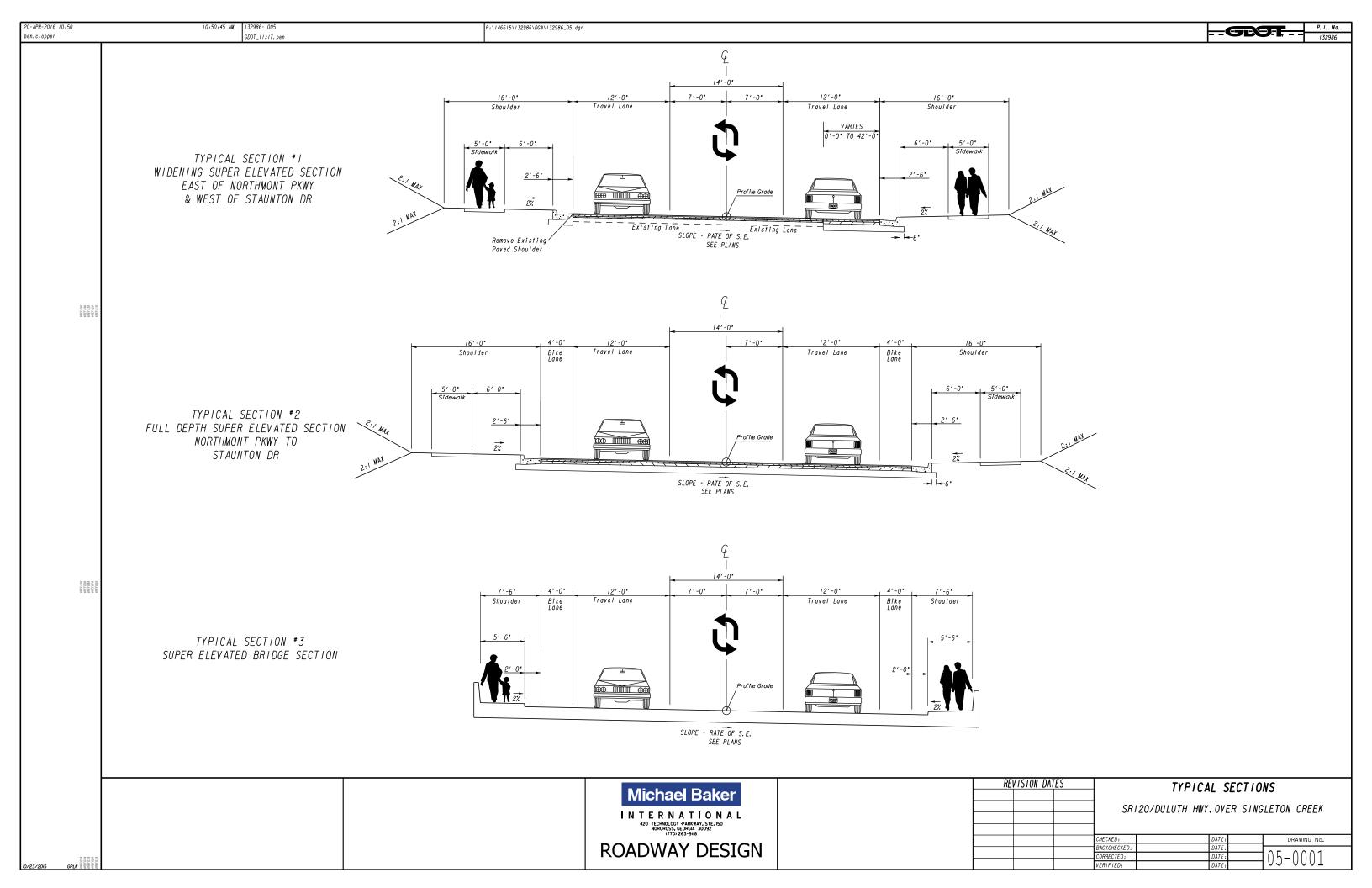
Approve: Mayaret B. Pull

Chief Engineer

5.10.16

Date





DATE : 04/20/2016

PAGE : 1

JOB ESTIMATE REPORT

JOB NUMBER : 132986 SPEC YEAR: 13

DESCRIPTION: SR 120 AT SINGLETON CREEK

ITEMS FOR JOB 132986

LINE	ITEM	ALT	UNITS	DESCRIPTION	QUANTITY	PRICE	AMOUNT
	150-1000		LS	TRAFFIC CONTROL - 132986 FIELD ENGINEERS OFFICE TP 1 GRADING COMPLETE - 132986 GR AGGR BASE CRS, INCL MATL AGGR SURF CRS RECYL AC PATCHING, INCL BM RECYL AC LEVELING, INC BM&HL RECYL AC 12.5MM SP,GP2,BM&HL RECYL AC 25MM SP,GP1/2,BM&HL RECYL AC 12.5MM SP,GP1/2,BM&HL RECYL AC 12.5MM SP,GP1/2,BM&HL		200000.00	
0010	153-1100		EA	FIELD ENGINEERS OFFICE TP 1	1.000	85000.00	85000.00
0015	210-0100		LS	GRADING COMPLETE - 132986	1.000	400000.00 26.47	400000.00
0020	310-1101		TN	GR AGGR BASE CRS, INCL MATL	2500.000	26.47	400000.00 66190.03
0025	318-3000		TN	AGGR SURF CRS	100.000	26.07	2607.54
0029	402-1801		TN	RECYL AC PATCHING, INCL BM	200.000		
0030	402-1812		TN	RECYL AC LEVELING, INC BM&HL	1000.000	91.24	18000.00 91243.69
0035	402-3130		TN	RECYL AC 12.5MM SP,GP2,BM&HL	1100.000	95.35	104886.31
0040	402-3121		TN	RECYL AC 25MM SP,GP1/2,BM&HL	2700.000	77.40 84.67	208989.29
0045	402-3190		TN	RECYL AC 19 MM SP,GP 1 OR 2 ,INC BM&HL	1400.000	84.67	118549.23
0049	407-0010		LF	ASPH-RUB JOINT/CRACK SEAL TP M	500.000	1.14	572.16
0050	413-0750		GL	TACK COAT REINF CONC APPROACH SLAB MILL ASPH CONC PVMT/ 2 DEP	1200.000	3.00 169.49	3600.00
0055	433-1000		SY	REINF CONC APPROACH SLAB	210.000	169.49	35593.59
0060	432-0208		SY	MILL ASPH CONC PVMT/ 2 DEP	8292.000	4.00	33168.00
0065	446-1100		LF	PVMT REF FAB STRIPS, TP2,18 INCH WIDTH	1500.000	6.48 70.17	9732.12
0070	441-0754		SY			70.17	4631.22
0075	441-0104		SY	CONC MEDIAN, 7 1/2 IN CONC SIDEWALK, 4 IN CONC CURB & GUTTER, 6X30TP2 WATERPROOFING PVMT JTS & CRACK 1 FT	2019.000	23.56	47571.96
0800	441-6022		LР	CONC CURB & GUTTER, 6X30TP2	3819.000	15.36 2.00 123.76	58662.36
0084	445-0500		LF	WATERPROOFING PVMT JTS & CRACK 1 FT	500.000	2.00	1000.00
0085	634-1200		EA	RIGHT OF WAY MARKERS	21.000	123.76	2598.97
0090	641-1100		LF	GUARDRAIL, TP T	36.000	83.11	2992.06
0095	641-1200		LF	GUARDRAIL, TP W	400.000	83.11 18.87	7548.67
0100	641-5001		EA	WATERPROOFING PVMT JTS & CRACK 1 FT RIGHT OF WAY MARKERS GUARDRAIL, TP T GUARDRAIL, TP W GUARDRAIL ANCHORAGE, TP 1 GUARDRAIL ANCHORAGE, TP 12 BARRIER FENCE (ORANGE), 4 FT STM DR PIPE 18,H 1-10 FLARED END SECT 18 IN, ST DR CATCH BASIN, GP 1 DROP INLET, GP 1 DRY SWALE EDGE DRAIN TEMPORARY GRASSING MULCH CONSTRUCTION EXIT CONS & REM INLET SEDIMENT TRAP MAINT OF TEMP SILT FENCE, TP C	2.000	970.58	1941.17
0105	641-5012		EA	GUARDRAIL ANCHORAGE, TP 12	2.000	2444.75	4889.52
0110	643-8200		LF	BARRIER FENCE (ORANGE), 4 FT	1570.000	1.42	2243.06
0115	550-1180		LF	STM DR PIPE 18,H 1-10	544.000	1.42 48.25	26249.93
0120	550-4218		EA	FLARED END SECT 18 IN, ST DR	5.000	632.73 2376.46	3163.67
0125	668-1100		EA	CATCH BASIN, GP 1	7.000	2376.46	3163.67 16635.26 4102.21
0130	668-2100		EA	DROP INLET, GP 1	2.000	2051.10	4102.21
0134	999-3155		LF	DRY SWALE EDGE DRAIN	100.000	69.36	6936.44
0135	163-0232		AC	TEMPORARY GRASSING	2.000	540.88	1081.77
0140	163-0240		TN	MULCH	128.000	540.88 238.89	30578.71
0145	163-0300		EA	CONSTRUCTION EXIT	2.000	1336.92	2673.85
0149	163-0550		EA	CONS & REM INLET SEDIMENT TRAP	10.000	152.14 1.45	1521.43
0150	165-0030		LF	MAINT OF TEMP SILT FENCE, TP C	2565.000		3719.97
0155	165-0101		EA	MAINT OF CONST EXIT	2.000	570.22	1140.45
0159	165-0105		EA	MAINT OF INLET SEDIMENT TRAP	10.000	54.72	547.24
0160	167-1000		EA	CONSTRUCTION EXIT CONS & REM INLET SEDIMENT TRAP MAINT OF TEMP SILT FENCE, TP C MAINT OF CONST EXIT MAINT OF INLET SEDIMENT TRAP WATER QUALITY MONITORING AND SAMPLING WATER QUALITY INSPECTIONS	10.000 2.000	570.22 54.72 225.02	450.05
0165	167-1500		MO	WATER QUALITY INSPECTIONS	24.000	301.31	14096.98
0170	171-0030		LF	TEMPORARY SILT FENCE, TYPE C	5130.000	3.45 933.08	17733.95
0175	700-6910		AC	PERMANENT GRASSING	3.000	933.08	2799.26

STATE HIGHWAY AGENCY

DATE : 04/20/2016

ESTIMATED TOTAL:

PAGE : 2

JOB ESTIMATE REPORT

======	==========				:=========	========
0180	700-7000	TN	AGRICULTURAL LIME	9.000	150.20	1351.88
0185	700-8000	TN	FERTILIZER MIXED GRADE	3.000	583.36	1750.10
0190	700-8100	LB	FERTILIZER NITROGEN CONTENT	144.000	3.23	465.97
0195	700-9300	SY	SOD	5144.000	4.86	25033.79
0200	711-0100	SY SY SF	TURF REINFORCING MATTING, TP 1	1840.000	2.50	4600.00
0205	716-2000	SY	EROSION CONTROL MATS, SLOPES	3010.000	1.22	3697.33
0210	636-1041	SF	HWY SIGNS, TP 2MAT, REFL SH TP 9	300.000	37.04	11114.26
0215	636-2070	LF	GALV STEEL POSTS, TP 7	400.000	8.02	3210.86
0218	652-0094	EA	PVMT MARKING, SYMBOL, TP 4	2.000	96.77	193.56
0219	653-0110	EA	THERM PVMT MARK, ARROW, TP 1	2.000	74.13	148.27
0220	653-0120	LF EA EA EA LF	THERM PVMT MARK, ARROW, TP 2	26.000	74.13 84.07 118.03 0.56	2185.86
0225	653-0130	EA	THERM PVMT MARK, ARROW, TP 3	1.000	118.03	118.03
0230	653-1501	LF	THERMO SOLID TRAF ST 5 IN, WHI	5450.000	0.56	3062.14
0235	653-1502	T.F	THERMO SOLID TRAF ST, 5 IN YEL	3930.000	0.50	2229.09
0240	653-1704	LF	THERM SOLID TRAF STRIPE, 24, WH	128.000	6.75	864.41
0245		LF	THERM SOLID TRAF STRIPE, 8,WH		2.13	
0250		GLF	THERMO SKIP TRAF ST, 5 IN, WHI	650.000	0.37	244.00
0255		SY	THERM TRAF STRIPING, WHITE	122.000	4.62	563.70
0259	653-6006	SY	THERM TRAF STRIPING, YELLOW	731.000	3.90	2852.67
0260	654-1001	EA	RAISED PVMT MARKERS TP 1	55.000	5.08	279.50
0265	654-1003	EA	RAISED PVMT MARKERS TP 3	72.000	4.53	326.56
0270	657-1085	LF	PRF PL SD PVT MKG,8,B/W,TP PB	400.000	7.34	2936.01
0275	657-6085	LF	PRF PL SD PVMT MKG,8,B/Y,TPPB	800.000	6.82	5461.38
0280	639-4004	EA	STRAIN POLE, TP IV	4.000	7963.30	31853.20
0285	647-1000	LS	TRAF SIGNAL INSTALLATION NO - 1	1.000	60000.00	60000.00
0290	540-1101	LS	REM OF EX BR, STA NO - 23+80	1.000	29900.00	29900.00
0295	543-9000	LS	CONSTR OF BRIDGE COMPLETE - 1	1.000	761100.00	761100.00
	 TOTAL					2604747.97
INFLATED ITEM TOTAL 2604747.9					2604747.97	
TOTAL	S FOR JOB 13298	36				
ESTIM	ATED COST:					2604747.97
CONTI	NGENCY PERCENT	(0.0):				0.00

2604747.97

PROJ. NO. P.I. NO.

DATE

DIESEL

LIQUID AC

132986 4/20/2016 CALL NO.

62,496.00

INDEX (TYPE)

REG. UNLEADED

DATE INDEX

Apr-16 \$ 2.037

\$ 2.120

\$ 336.00

Link to Fuel and AC Index:

http://www.dot.ga.gov/doingbusiness/Materials/Pages/asphaltcementindex.aspx

LIQUID AC ADJUSTMENTS

PA=[((APM-APL)/APL)]xTMTxAPL

Asphalt

Price Adjustment (PA)			62496	\$
Monthly Asphalt Cement Price month placed (APM)	Max. Cap	60%	\$ 537.60	
Monthly Asphalt Cement Price month project let (APL)			\$ 336.00	
Total Monthly Tonnage of asphalt cement (TMT)			310	

ASPHALT	Tons	%AC	AC ton
Leveling	1000	5.0%	50
12.5 OGFC		5.0%	0
12.5 mm	1100	5.0%	55
9.5 mm SP		5.0%	0
25 mm SP	2700	5.0%	135
19 mm SP	1400	5.0%	70
	6200	•	310

BITUMINOUS TACK COAT

Price Adjustment (PA)			\$	1,039.07	\$	1,039.07
Monthly Asphalt Cement Price month placed (APM)	Max. Cap	60%	\$	537.60		
Monthly Asphalt Cement Price month project let (APL)			\$	336.00		
Total Monthly Tonnage of asphalt cement (TMT)			5	5.154121106		

Bitum Tack

Gals	gals/ton	tons
1200	232.8234	5.15412111

PROJ. NO.						CALL NO.	
P.I. NO.	132986						
DATE	4/20/2016						
BITUMINOUS TACK CO	OAT (surface t	reatment)					
Price Adjustment (PA)						0	\$ -
Monthly Asphalt Ceme	ent Price mont	th placed (APM)		Max. Cap	60%	\$ 537.60	
Monthly Asphalt Ceme	ent Price mont	th project let (AP	L)			\$ 336.00	
Total Monthly Tonnag	e of asphalt ce	ement (TMT)				0	
Bitum Tack	SY	Gals/SY	Gals	gals/ton	tons		
Single Surf. Trmt.		0.20	0	232.8234	0		
Double Surf.Trmt.		0.44	0	232.8234	0		
Triple Surf. Trmt		0.71	0	232.8234	0		
		_			0		

\$

63,535.07

TOTAL LIQUID AC ADJUSTMENT

DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA

INTERDEPARTMENT CORRESPONDENCE

FILE	P.I. No.		132986	OFFICE	Office of Program	
DD C IE		mæ.	TON.			Delivery
	CT DESCRI					
SK 120/1	Duluth High	way	@ Singleton Creek 1.5 Mi E of Duluth		DATE	April 20, 2016
					DATE	April 20, 2010
From:	Albert Shel	by	PE, State Program Delivery Engineer			
rioni.	Albeit Silei	.Uy,	1 E, State 1 Togram Denvery Engineer			
To:	•		State Project Review Engineer			
	via Email N	/Iail	box: CostEstimatesandUpdates@dot.	ga.gov		
Subject:	REVISION	IS T	O PROGRAMMED COSTS			
y				MGMT LE	Γ DATE	Jun-19
PROJEC	T MANAGI	ER	Anthony Tate			
				MGMT RO	W DATE	Jun-18
PROGR	AMMED C	OS'	TS (TPro W/OUT INFLATION)		LAST	ESTIMATE UPDATE
CONSTI	RUCTION	\$	3,388,357.72		DATE	2014
RIGHT	OF WAY	\$	214,731.65		DATE	2005
RIGITI	OF WAT	Ψ	214,731.03		DAIL	2003
UTILITI	ES	\$			DATE	
REVISE	ED COST ES	STI	<u>MATES</u>			
CONSTI	RUCTION*	\$	3,072,018.98			
RIGHT	OF WAY	\$	492,000.00			
UTILITI	ES	\$	928,500.00			
*Cost C	Contains	10	% Contingency			

REASONS FOR COST INCREASE AND CONTINGENCY JUSTIFICATION:

Cost adjustments are due to update of the project concept report. Contigency of 10% is based on the allowable range for a Bridge Replacement from the Risk Based Cost Estimation memo dated 4/30/2014

CONTINGENCY SUMMARY

A. CONSTRUCTION COST ESTIMATE:	\$ 2,604,747.97	Base Estimate From CES
B. ENGINEERING AND INSPECTION (E & I):	\$ 130,237.40	Base Estimate (A) x 5
c. CONTINGENCY:	\$ 273,498.54	Base Estimate (A) + E & I (B) x See % Table in "Risk Based Cost Estimation" Memo
D. TOTAL LIQUID AC ADJUSTMENT:	\$ 63,535.07	Total From Liquid AC Spreadsheet
E. CONSTRUCTION TOTAL:	\$ 3,072,018.98	(A + B + C + D = E)

REIMBURSABLE UTILTY COSTS

UTILITY OWNER	REIMBURSABLE COST
GCDWR W&S	\$ 300,250.00
GPC - Distribution	\$ 411,500.00
Jackson EMC	\$ 216,750.00
TOTAL	\$ 928,500.00
ATTACHMENTS: (File Copy in the Project Cost Estimat	re Folder)
Detailed Cost Estimate Printout From TRAQS	
Liquid AC Adjustment Spreadsheet	

GEORGIA DEPARTMENT OF TRANSPORTATION PRELIMINARY ROW COST ESTIMATE SUMMARY

Project: BRSTO-0189-01(030)

1/14/2016

Date:

Revised: County: Gwinnett PI: 132986 Description: SR 120/Duluth Highway@ Singleton Creek Project Termini: SR 120/Duluth Highway@ Singleton Creek Existing ROW: Varies Parcels: 10 Required ROW: Varies \$262,500.00 Land and Improvements Proximity Damage \$0.00 Consequential Damage \$0.00 Cost to Cures \$0.00 Trade Fixtures \$0.00 Improvements \$55,000.00 \$37,500.00 Valuation Services Legal Services \$81,750.00 Relocation \$20,000.00 \$0.00 Demolition \$90,000.00 Administrative TOTAL ESTIMATED COSTS \$491,750.00 TOTAL ESTIMATED COSTS (ROUNDED) \$492,000.00 **Preparation Credits** Hours Signature Prepared By: CG#: 286999 01/14/2016 (DATE) Approved By: 01/14/2016 (DATE) CG#: 286999

NOTE: No Market Appreciation is included in this Preliminary Cost Estimate

DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA

INTERDEPARTMENT CORRESPONDENCE

FILE

BRST0-0189-01(030), Gwinnett Co

OFFICE

GAINESVILLE

PI No. 132986-

SR 120/Duluth Hwy @ Singleton Creek 1.5 Miles E of Duluth

FROM

Robby Oliver, Distr. Utilities Eng.

DATE

January 27, 2016

TO

Albert Shelby, P.E., State Program Delivery Engineer

ATTN

Anthony Tate, Project Manager

SUBJECT

PRELIMINARY UTILITY COST ESTIMATE

As requested by your office we are furnishing you with an Preliminary Utility Cost estimate for the subject project.

FACILITY OWNER		NON-REIMBURSABLE	REIMBURSABLE
Atlanta Gas Light		\$295,550	\$0
AT&T Telephone - Local		\$386,550	\$0
AT&T Long Distance		\$8,400	\$0
GCDWR W & S	**	\$192,300	\$300,250
GPC - Distribution		\$0	\$411,500
Jackson EMC		\$0	\$216,750
Charter Communications		\$10,050	\$0
Comcast CATV		\$18,750	\$0
Level 3 - Communications		\$11,400	\$0
Zayo Telecom		\$8,400	\$0
	-		
L			

TOTALS

\$931,400

\$928,500

Total Non-Reimbursable Cost

\$931,400

Total Reimbursable Cost

\$928,500

If you have any questions, please contact Robby Oliver at 770-531-5772.

RBO/jlp

cc: Lee Upkins, State Utilities Engineer Scott Frederick, Area Engineer File

^{**} If the local gov't is granted utility aid, \$192,300 will need to be added to the reimbursable cost.

WETLANDS AND OPEN WATERS MITIGATION WORKSHEETS

Gwinnett County P.I. 132986

Replacement of the SR 120 Bridge over Singleton Creek

ADVERSE IMPACT FACTORS

	AD VERSE IVII ACT TACTORS							
Factor		Options						
Dominant Effect	Fill 2.0	Dredge 1.8	Impound 1.6	Drain 1.4	Flood 1.2	Clear 1.0	Shade 0.5	
Duration of Effects	7+ years 2.0	5-7 years 1.5	3-5 years 1.0	1-3 years 0.5	< 1 year 0.1			
Existing Condition	Class 1 2.0	Class 2 1.5	Class 3 1.0	Class 4 0.5	Class 5 0.1			
Lost Kind	Kind A 2.0	Kind B 1.5	Kind C 1.0	Kind D 0.5	Kind E 0.1			
Preventability	High 2.0	Moderate 1.0	Low 0.5	None 0				
Rarity Ranking	Rare 2.0	Uncommon 0.5	Common 0.1					

[†] These factors are determined on a case-by-case basis.

REQUIRED MITIGATION CREDITS WORKSHEET

Factor	WL 4 (fill)					
Dominant Effect	2.0					
Duration of Effect	2.0					
Existing Condition	1.0					
Lost Kind	1.5					
Preventability	0.5					
Rarity Ranking	0.1					
Sum of r Factors	$R_1 = 7.1$	R ₂ =	R ₃ =	$R_4 =$	R ₅ =	R ₆ =
Impacted Area	$AA_1 = 0.20$	AA ₂ =	AA ₃ =	$AA_4 =$	AA ₅ =	AA ₆ =
$R \times AA =$	1.42					

Total Required Credits = $\sum (\mathbf{R} \times \mathbf{A}\mathbf{A}) =$	1.42
--	------

For our SR 53 project in Forsyth & Hall Counties, P.I. 0007021, the price per wetland credit was estimated at \$34,000. Using this number as the basis for estimating the cost for Section 404 mitigation for this project, the total cost for mitigation would be approximately \$48,280.

Crash Summaries

The project area is primarily comprised of two intersections, and most of the crashes occurred at those intersections. Two crashes occurred mid-block, one of which was a run-off the road crash and the other of which was a sideswipe.

Table 1 through Table 4 show the crash statistics of the project area.

Table 1: Crashes by PDO/Injury/Fatal

Year	Property Damage Only	Injury	Fatal	Grand Total
2011	3	4	0	7
2012	7	4	0	11
2013	5	2	0	7
2014	16	3	0	19
2015	12	4	0	16
Grand Total	43	17	0	60

Table 2: Crashes by Intersection

Year	Northmont Parkway	Staunton Drive	Not at an Intersection	Grand Total
2011	4	3		7
2012	10	1		11
2013	3	4		7
2014	11	8		19
2015	14		2	16
Grand Total	42	16	2	60

Table 3: Crashes by Manner of Collision

Year	Angle	Head On	Not A Collision with Motor Vehicle	Rear End	Sideswipe- Opposite Direction	Sideswipe- Same Direction	Grand Total
2011	2		1	4			7
2012	2		1	7		1	11
2013	1	2	1	3			7
2014	2	1	2	13	1		19
2015	3		1	11		1	16
Grand Total	10	3	6	38	1	2	60

Table 4: Crashes by First Harmful Event

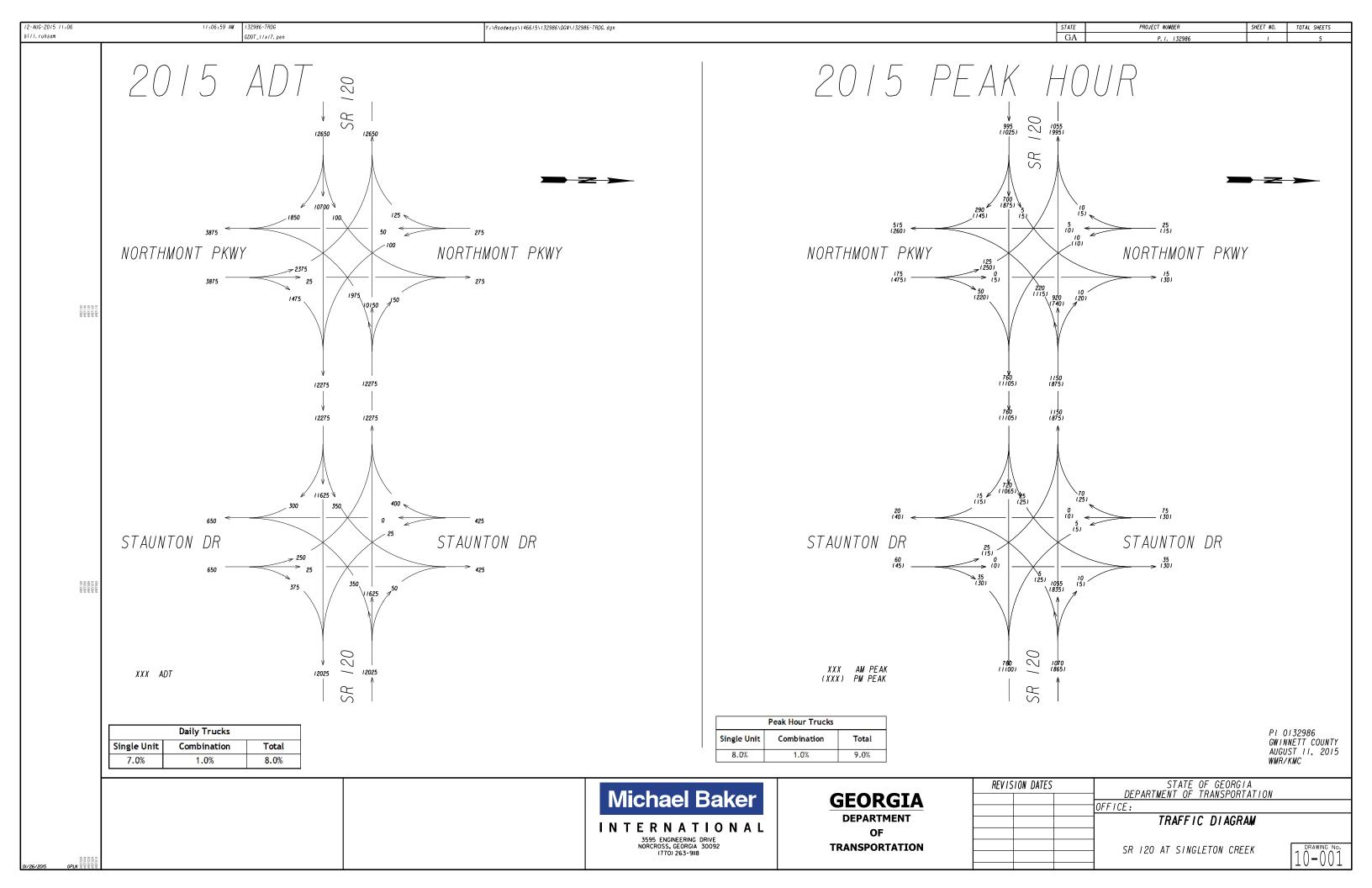
Year	Deer	Guard Rail End	Guard Rail Face	Motor Vehicle In Motion	Grand Total
2011	1			6	7
2012				11	11
2013		1	1	5	7
2014		1	1	17	19
2015	1			15	16
Grand Total	2	2	2	54	60

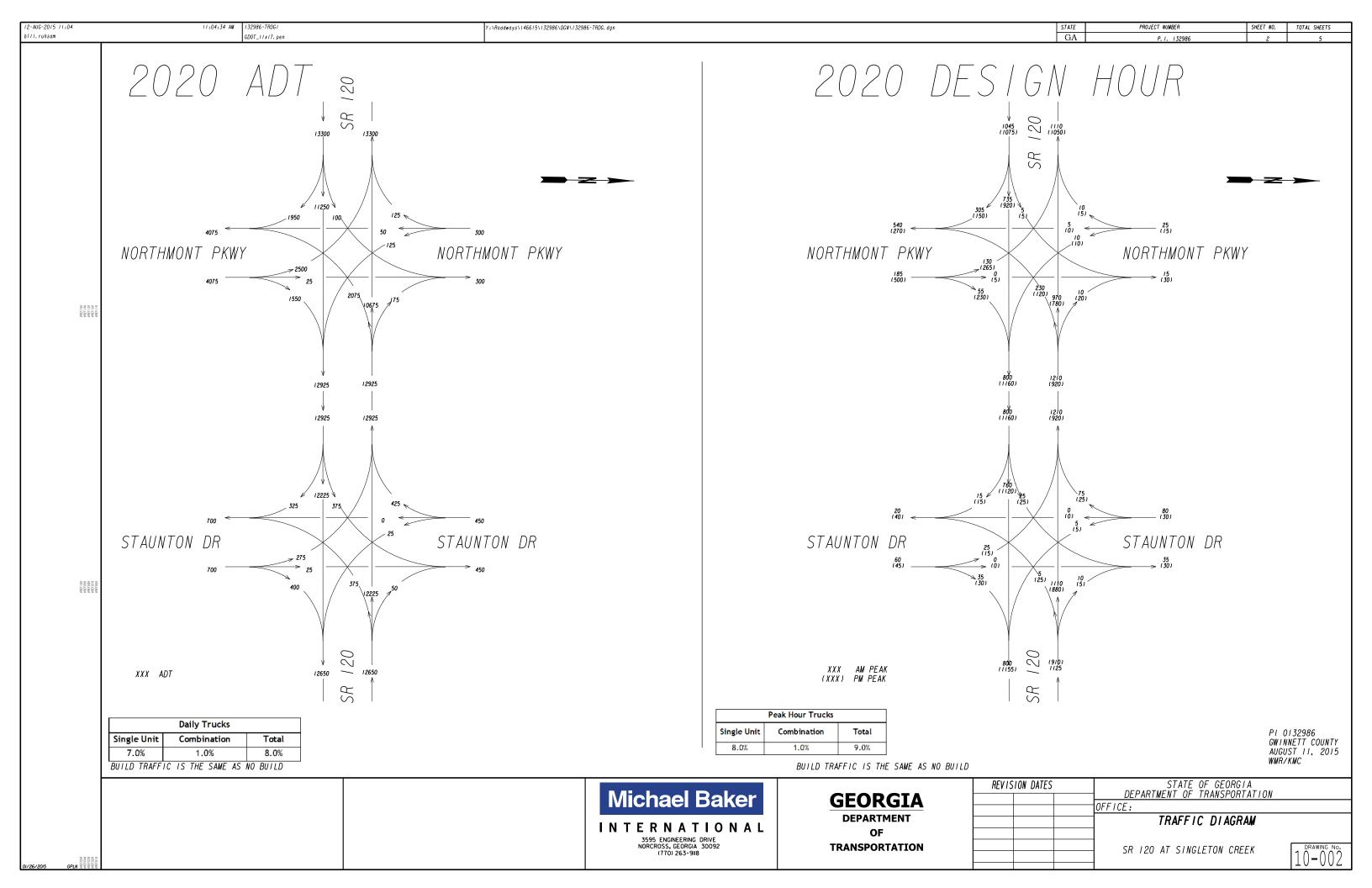
The crash history for this project does not illustrate any particular hot spot or egregious mode of collision that need to be addressed, compared to other similar locations.

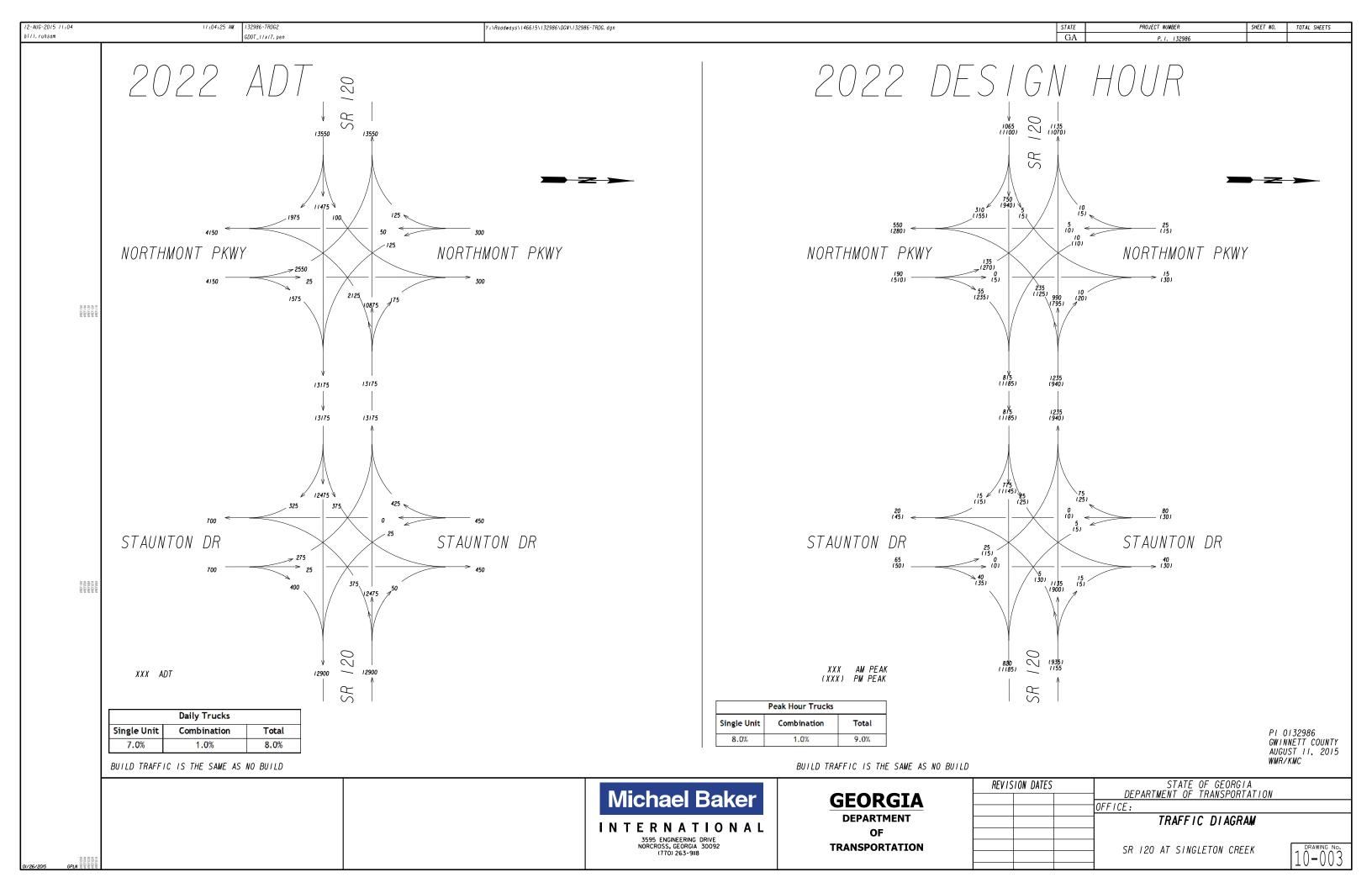
Table 5: Crashes at Staunton Drive

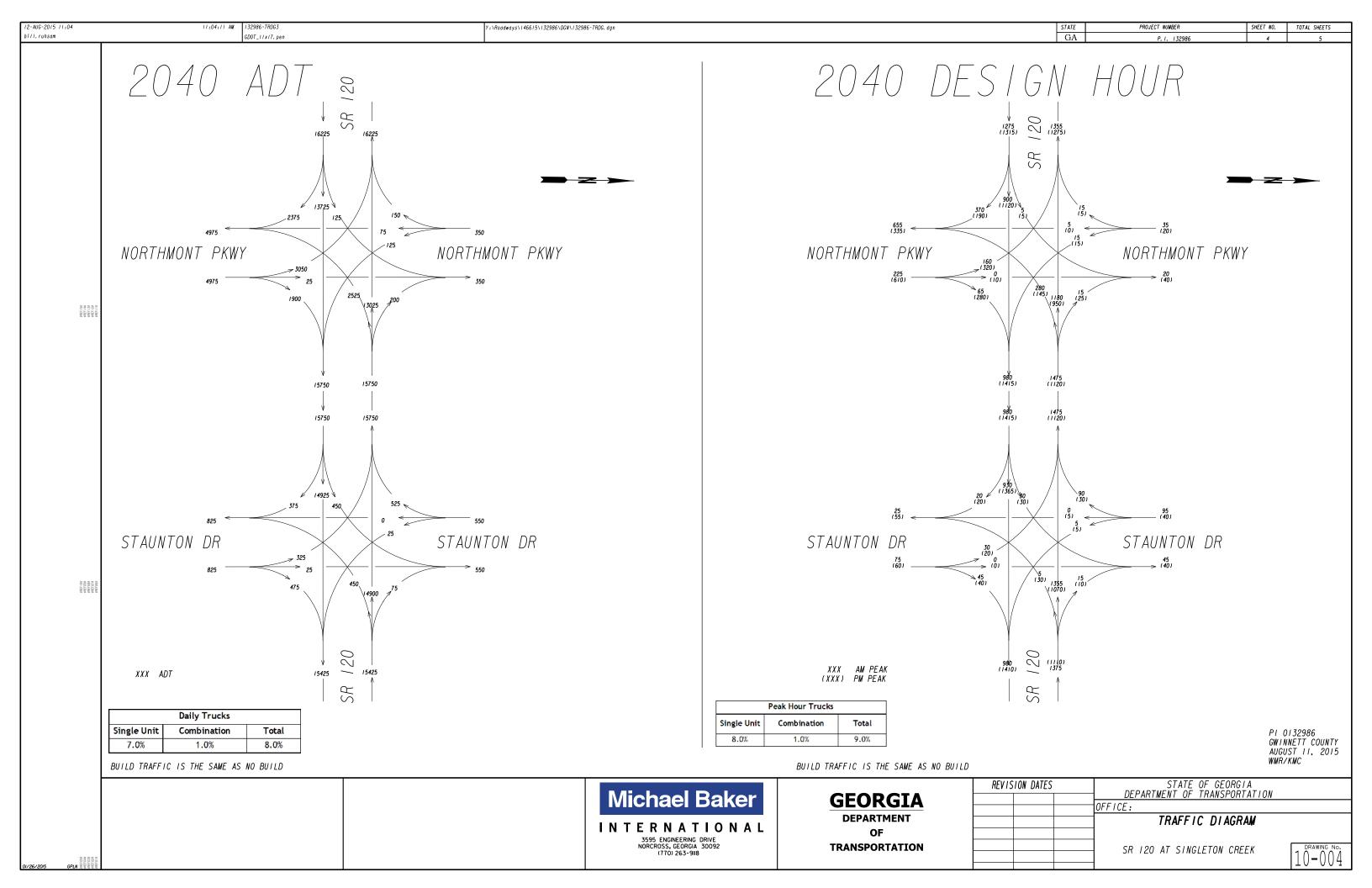
Year	Angle	Head On	Not A Collision with Motor Vehicle	Rear End	
2011	1		1	1	3
2012	1				1
2013	1	1	1	1	4
2014	2	1	1	4	8
2015					0
Grand Total	5	2	3	6	16

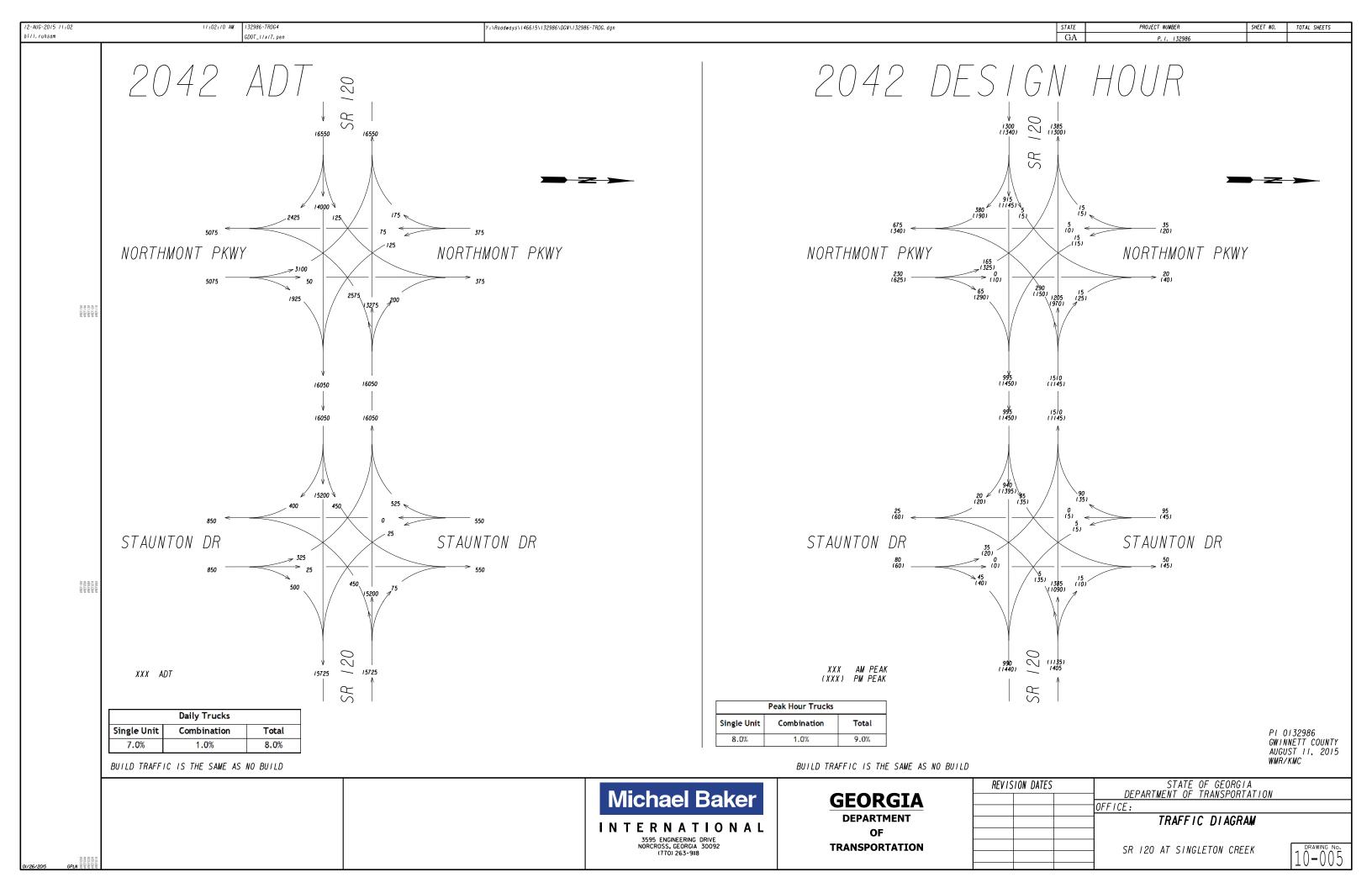
Given the short nature of this project (0.35 miles), crash rate calculations were not conducted.











Capacity Analysis

Using the existing geometry, traffic volumes and existing signal timing Existing Conditions *Synchro* models were set up for the study area. The resulting Existing Levels of Service (LOS) for each intersection, for each peak hour, are shown in Table 1. The *Synchro* reports are contained in Appendix B.

2015 Existing Level of Service

AM Peak PM Peak

Delay (Sec/Veh) LOS Delay (Sec/Veh) LOS

SR 120 at Northmont Pkwy. (Signalized)

SR 120 at Staunton Dr. (Two-Way Stop Control)

Table 1: Existing Intersection LOS

The existing operating conditions of Northmont Parkway at SR 120 are good and require no changes. Staunton Drive is showing high delays for the cross street, however a large delay for a low volume stop-controlled approach during only the peak hours does not necessarily justify improvements.

Open Year 2020 and Design Year 2040 volumes were then used to create No Build *Synchro* models with the existing roadway geometry and traffic control, with cycle lengths preserved. The resulting No Build LOS for each intersection, during each peak hour, are presented in Table 2. The *Synchro* reports are contained in Appendix B.

	No Build Level of Service (delay in sec/veh)								
		Open Year 2020				Design Year 2040			
	AM Peak PM Peak			AM F	Peak	PM Peak			
	Delay		Delay		Delay		Delay		
	(Sec/ Veh)	LOS	(Sec/ Veh)	LOS	(Sec/ Veh)	LOS	(Sec/ Veh)	LOS	
SR 120 at Northmont Pkwy. (Signalized)	20.7	С	45.1	D	44.4	D	88.7	F	
SR 120 at Staunton Dr. (Two-Way Stop Control)	*	F	*	F	*	F	*	F	

Table 2: No Build Intersection LOS

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.

In 2020, the LOS at Northmont Parkway will by C and D in the AM and PM, respectively, still acceptable Levels of Service for an urban area. In 2040, Northmont Parkway will fall to LOS F in the PM peak hour without any change to the operating conditions.

Build Conditions *Synchro* models were developed to evaluate the intersection operations with the proposed geometry. The resulting Build LOS for each intersection, during each peak hour of both the Open Year 2020 and Design Year 2040, are shown in Table 3. The Synchro reports are contained in Appendix B.

		Build Level of Service (delay in sec/veh)							
		Open Yo	ear 2020		Design Year 2040				
	AM Peak PM Peak			AM F	Peak	PM I	Peak		
	Delay (Sec/ Veh)	LOS	Delay (Sec/ Veh)	LOS	Delay (Sec/ Veh)	LOS	Delay (Sec/ Veh)	LOS	
SR 120 at Northmont Pkwy. (Signalized)	21.4	С	39.2	D	44.7	D	76.6	E	
SR 120 at Staunton Dr. (Two-Way Stop Control)	*	F	*	F	*	F	*	F	

Table 3: Build Intersection LOS

As shown above, in the Open Year 2020 there is a slight increase in delay at Northmont Parkway during the AM peak hour and a slight reduction in the PM peak hour. Neither LOS changes from the No-Build condition.

In the Design Year 2040 the AM peak hour delay is nearly identical to the No-Build, however the proposed improvements change the LOS during the PM peak hour from F to E, still considered a failing LOS in an urban area.

The *Synchro* model for 2040 PM peak hour was modified to investigate what changes would be required to achieve a LOS D. In order to achieve that acceptable level of service, both the northbound and westbound left turns would need to be expanded to dual lefts. Constructing dual lefts on either, but not both, of those turns would still have LOS E, with a delay of approximately 65 seconds per vehicle. As this project does not contain provisions for extensive widening that would be required to provide receiving lanes for dual lefts, this is not recommended.

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.



MEMORANDUM

TO: Ben Clopper, P.E.

FROM: Bill Ruhsam, P.E., PTOE

SUBJECT: SR 120 at Singleton Creek Traffic Study

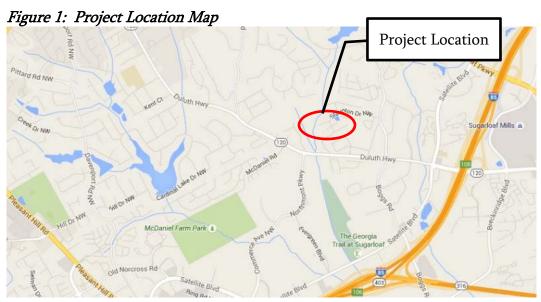
PI 132988

DATE: October 23, 2015

This memo documents the analysis conducted by Michael Baker International (Baker) regarding the SR 120 at Singleton Creek bridge replacement project. This memo summarizes the analysis of approved traffic volumes under the proposed Build conditions. For a description of how traffic volumes were derived, see the Traffic Projections Summary Memorandum included in the appendix.

Project Location and Scope

The project is located on SR 120 (Duluth Highway) between Northmont Parkway and Staunton Drive. The project location is shown in Figure 1.



The project consists of replacement of the existing SR 120 bridge over Singleton Creek. The total project length is 0.35 miles The project is located in Gwinnett County, 1.2 miles

east of the City of Duluth. The new bridge will include two 12' lanes plus a center turn lane, shoulders and a sidewalk for pedestrians.

As a part of the project, intersection improvements are proposed for SR 120 at Northmont Parkway and SR 120 at Staunton Drive. The existing condition of each intersection is shown in Figure 2 and Figure 3.

Figure 2: SR 120 at Northmont Parkway Existing Conditions



Figure 3: SR 120 at Staunton Drive Existing Conditions



The proposed conditions for these intersections are to address operational deficiencies identified by this traffic study, but within a limited scope, i.e. no additional widening. With the limitation of no additional capacity, possible improvements include changes to

turn lane storage and signal phasing. Table 1 shows the existing and proposed turn lane conditions.

Table 1: Turn Lane Storage; Existing and Proposed

		Existing/	No Build	Prop	osed
		Northmont	Staunton	Northmont	Staunton
		Parkway	Drive	Parkway	Drive
Eastbound	Left	240	175	200	220
Eastbound	Right	220	285	250	220
Westbound	Left	95	300	450	300
westbound	Right	210	205	250	205
	Left	260	Shared	260	Shared
Eastbound			Lane	200	Lane
Eastbound	Right	Lane Drop	Shared	Lane Drop	Shared
	Kigiit	Lane Drop	Lane	Lane Drop	Lane
	Left	65	Shared	65	Shared
Westbound	Leit	0.5	Lane	0.5	Lane
w estboulla	Right	Shared	Shared	Shared	Shared
	Kigiit	Lane	Lane	Lane	Lane

Crash Summaries

The project area is primarily comprised of two intersections, and most of the crashes occurred at those intersections. Two crashes occurred mid-block, one of which was a run-off the road crash and the other of which was a sideswipe.

Table 2 through Table 5 show the crash statistics of the project area.

Table 2: Crashes by PDO/Injury/Fatal

Year	Property Damage Only	Injury	Fatal	Grand Total
2011	3	4	0	7
2012	7	4	0	11
2013	5	2	0	7
2014	16	3	0	19
2015	12	4	0	16
Grand Total	43	17	0	60

Table 3: Crashes by Intersection

Year	Northmont Parkway	Staunton Drive	Not at an Intersection	Grand Total
2011	4	3		7
2012	10	1		11
2013	3	4		7
2014	11	8		19
2015	14		2	16
Grand Total	42	16	2	60

Table 4: Crashes by Manner of Collision

Year	Angle	Head On	Not A Collision with Motor Vehicle	Rear End	Sideswipe- Opposite Direction	Sideswipe- Same Direction	Grand Total
2011	2		1	4			7
2012	2		1	7		1	11
2013	1	2	1	3			7
2014	2	1	2	13	1		19
2015	3		1	11		1	16
Grand Total	10	3	6	38	1	2	60

Table 5: Crashes by First Harmful Event

Year	Deer	Guard Rail End	Guard Rail Face	Motor Vehicle In Motion	Grand Total
2011	1			6	7
2012				11	11
2013		1	1	5	7
2014		1	1	17	19
2015	1			15	16
Grand Total	2	2	2	54	60

The crash history for this project does not illustrate any particular hot spot or egregious mode of collision that need to be addressed, compared to other similar locations.

Table 6: Crashes at Staunton Drive

Year	Angle	Head On	Not A Collision with Motor Vehicle	Rear End	
2011	1		1	1	3
2012	1				1
2013	1	1	1	1	4
2014	2	1	1	4	8
2015					0
Grand Total	5	2	3	6	16

Given the short nature of this project (0.35 miles), crash rate calculations were not conducted.

Signal Warrants

The existing signalized intersection at Northmont Parkway will be maintained, with a change to signal phasing to optimize the intersection. The northbound left turn warrants protected/permitted left turn phasing in addition to the existing protected/permitted left turn for westbound lefts from SR 120.

The possibility of a signal at Staunton Drive was evaluated using the conditions set forth in the Manual on Uniform Traffic Control Devices. The 2009 edition of the Manual on Uniform Traffic Control Devices (MUTCD) states that an engineering study shall be conducted to justify the installation of a traffic control signal. The study shall investigate the need for a traffic control signal based on an analysis of the applicable traffic signal warrants, as listed below:

Warrant 1 – Eight-Hour Vehicular Volume

Warrant 2 – Four-Hour Vehicular Volume

Warrant 3 – Peak Hour

Warrant 4 – Pedestrian Volume

Warrant 5 – School Crossing

Warrant 6 – Coordinated Signal System

Warrant 7 – Crash Experience

Warrant 8 – Roadway Network

Warrant 9 - Intersection Near a Grade Crossing

The MUTCD also provides guidance that while a traffic signal should not be installed unless one or more of these warrants is met, meeting a warrant or warrants does not in itself require the installation of a traffic control signal. In all cases, engineering judgment should be used to determine if the installation of a traffic control signal will improve the overall safety and/or operation of the intersection.

Each of the applicable warrants listed above were evaluated for the intersection of Staunton Drive at SR 120.

Warrant 1 – Eight-Hour Vehicular Volume

Warrant 1 is composed of two conditions, Condition A – Minimum Vehicular Volume and Condition B – Interruption of Continuous Traffic. The MUTCD states that the need for a traffic control signal shall be considered if one of the two conditions of the warrant exists for 8 hours of an average day. The required volumes from the MUTCD, as well as the traffic volumes for the study intersection, are presented in Table 7: Warrant 1 – Eight-Hour Vehicular Volume

Table 7: Warrant 1 – Eight-Hour Vehicular Volume

		., .	Condition		Condition B	
lla	Traffic	Volume	Satisfied ?		Satisfied ?	
Hour	Major	Minor	Major	Minor	Major	Minor
	Approach	Approach	Approach	Approach	Approach	Approach
	просон	просон	(500)	(150)	(750)	(75)
12-1 AM	143	2	NO	NO	NO	NO
1-2 AM	67	0	NO	NO	NO	ОИ
2-3 AM	56	0	NO	NO	NO	NO
3-4 AM	57	1	NO	NO	NO	NO
4-5 AM	128	2	NO	NO	NO	NO
5-6 AM	402	12	NO	NO	NO	NO
6-7 AM	1164	11	YES	NO	YES	NO
7-8 AM	1675	56	YES	NO	YES	NO
8-9 AM	1716	50	YES	NO	YES	NO
9-10 AM	1364	30	YES	NO	YES	NO
10-11 AM	1189	28	YES	NO	YES	NO
11-12 Noon	1192	25	YES	NO	YES	NO
12-1 PM	1400	19	YES	NO	YES	NO
1-2 PM	1309	17	YES	NO	YES	NO
2-3 PM	1477	14	YES	NO	YES	NO
3-4 PM	1461	19	YES	NO	YES	NO
4-5 PM	1702	15	YES	NO	YES	NO
5-6 PM	1960	27	YES	NO	YES	NO
6-7 PM	1806	20	YES	NO	YES	NO
7-8 PM	1416	27	YES	NO	YES	NO
8-9 PM	996	15	YES	NO	YES	NO
9-10 PM	874	21	YES	NO	YES	NO
10-11 PM	487	4	NO	NO	NO	NO
11-12 Midnight	284	2	NO	NO	NO	NO

The necessary volumes for Condition A are met for zero hours and Condition B are met for zero hours. **Therefore, Warrant 1 is Not Satisfied.**

Warrant 2 – Four-Hour Vehicular Volume

According to the MUTCD, the conditions of Warrant 2 are to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic control signal. To satisfy Warrant 2, the hourly vehicular volume of each of four hours in an average day must fall above the applicable curve, as provided in the MUTCD. The curve for 1-or-more-lanes & 1-lane is shown in Table 8, on which points for each hour of traffic volume have been plotted.

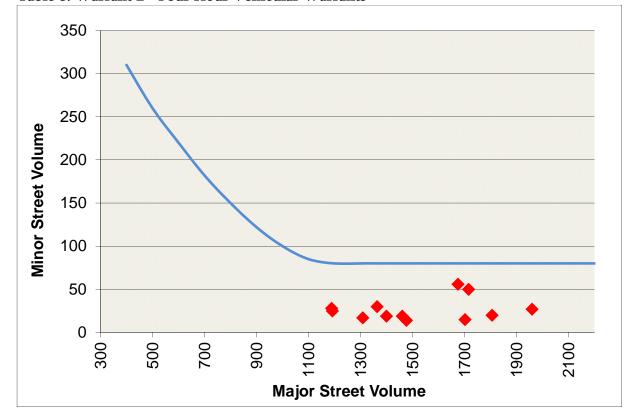


Table 8: Warrant 2 - Four Hour Vehicular Warrants

A total of zero points, each representing one hour of vehicular volume, lie above the applicable curve. **Therefore, Warrant 2 is Not Satisfied.**

Warrant 3 – Peak Hour

The study intersection is not an unusual case such as an office complex, manufacturing plant or HOV parking facility, as described in the MUTCD. Therefore, Warrant 3 in not applicable.

Warrant 4 – Pedestrian Volume

Pedestrian delay crossing the street was not observed at the time this report was written. Therefore, Warrant 4 is not applicable.

Warrant 5 – School Crossing

The presence of schoolchildren crossing the major street is not the principal reason to consider installing a traffic control signal at this intersection. Therefore, Warrant 5 is not applicable.

Warrant 6 – Coordinated Signal System

Maintaining progressive movement in a coordinated signal system is not a factor in considering the installation of a traffic control signal at this intersection. Therefore, Warrant 6 is not applicable.

Warrant 7 – Crash Experience

The MUTCD states that the need for a traffic control signal shall be considered if all three of the following criteria are met for an intersection.

- A. Adequate trial of alternatives with satisfactory observance and enforcement
- B. Five or more reported crashes, of types susceptible to correction by a traffic control signal, have occurred in a 12-month period
- C. For each of any 8 hours of an average day, the vehicles per hour (vph) given in both of the 80 percent columns of Warrant 1, Condition A, or the vph in both of the 80 percent columns of Warrant 1, Condition B exists on the major-street and the higher-volume minor-street approach

Crash statistics for the area were gathered from the GEARS website. In the period 2012-2015 (to date) only one twelve-month period had five or more crashes (2014) but only two of those would be addressable by a signal installation (angle-type crashes). **Therefore, Warrant 7 is Not Satisfied.**

Warrant 8 – Roadway Network

Encouraging concentration and organization of traffic flow is not the motive for installing a traffic control signal at this intersection. Therefore, Warrant 8 is not applicable.

Warrant 9 – Intersection Near a Grade Crossing

The study intersection is not located in close proximity to a grade crossing. Therefore, Warrant 9 is not applicable.

A summary of the nine traffic signal warrants, as presented in the MUTCD are show in Table 9.

Table 9: Signal Warrant Summary

WARRANT	SR 120 at Staunton Drive		
1. Eight-Hour Vehicular Volume	Not Satisfied		
2. Four-Hour Vehicular Volume	Not Satisfied		
3. Peak Hour	Not Applicable		
4. Pedestrian Volume	Not Applicable		
5. School Crossing	Not Applicable		
6. Coordinated Signal System	Not Applicable		
7. Crash Experience	Not Satisfied		
8. Roadway Network	Not Applicable		
9. Intersection Near a Grade	Not Applicable		
Crossing			

Capacity Analysis

Using the existing geometry, traffic volumes and existing signal timing Existing Conditions *Synchro* models were set up for the study area. The resulting Existing Levels of Service (LOS) for each intersection, for each peak hour, are shown in Table 10. The *Synchro* reports are contained in Appendix B.

Table 10: Existing Intersection LOS

	2015 Existing Level of Service						
	AM Peak PM Peak						
	Delay (Sec/Veh)	LOS	Delay (Sec/Veh)	LOS			
SR 120 at Northmont Pkwy. (Signalized)	19.1	В	17.9	В			
SR 120 at Staunton Dr. (Two-Way Stop Control)	*	F	*	F			

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.

The existing operating conditions of Northmont Parkway at SR 120 are good and require no changes. Staunton Drive is showing high delays for the cross street, however a large delay for a low volume stop-controlled approach during only the peak hours does not necessarily justify improvements.

Open Year 2020 and Design Year 2040 volumes were then used to create No Build *Synchro* models with the existing roadway geometry and traffic control, with cycle lengths preserved. The resulting No Build LOS for each intersection, during each peak hour, are presented in Table 11. The *Synchro* reports are contained in Appendix B.

Table 11: No Build Intersection LOS

		No Build Level of Service (delay in sec/veh)						
		Open Yo	ear 2020		Design Year 2040			
	AM F	Peak	PM I	Peak	AM F	Peak	PM Peak	
	Delay (Sec/		Delay (Sec/		Delay (Sec/		Delay (Sec/	
	Veh)	LOS	(Sec) Veh)	LOS	Veh)	LOS	(Sec) Veh)	LOS
SR 120 at Northmont Pkwy. (Signalized)	20.7	С	45.1	D	44.4	D	88.7	F
SR 120 at Staunton Dr. (Two-Way Stop Control)	*	F	*	F	*	F	*	F

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.

In 2020, the LOS at Northmont Parkway will by C and D in the AM and PM, respectively, still acceptable Levels of Service for an urban area. In 2040, Northmont Parkway will fall to LOS F in the PM peak hour without any change to the operating conditions.

Build Conditions *Synchro* models were developed to evaluate the intersection operations with the proposed geometry. The resulting Build LOS for each intersection, during each peak hour of both the Open Year 2020 and Design Year 2040, are shown in Table 12. The Synchro reports are contained in Appendix B.

Table 12: Build Intersection LOS

	Build Level of Service (delay in sec/veh)							
		Open Ye	ear 2020		Design Year 2040			
	AM F	Peak	PM I	Peak	AM Peak		PM Peak	
	Delay (Sec/		Delay (Sec/		Delay (Sec/		Delay (Sec/	
	Veh)	LOS	Veh)	LOS	Veh)	LOS	Veh)	LOS
SR 120 at Northmont Pkwy. (Signalized)	21.4	С	39.2	D	44.7	D	76.6	E
SR 120 at Staunton Dr. (Two-Way Stop Control)	*	F	*	F	*	F	*	F

^{*} On two-way stop controlled analysis, a delay in excess of 999 seconds is reported as unmeasurable.

As shown above, in the Open Year 2020 there is a slight increase in delay at Northmont Parkway during the AM peak hour and a slight reduction in the PM peak hour. Neither LOS changes from the No-Build condition.

In the Design Year 2040 the AM peak hour delay is nearly identical to the No-Build, however the proposed improvements change the LOS during the PM peak hour from F to E, still considered a failing LOS in an urban area.

The *Synchro* model for 2040 PM peak hour was modified to investigate what changes would be required to achieve a LOS D. In order to achieve that acceptable level of service, both the northbound and westbound left turns would need to be expanded to dual lefts. Constructing dual lefts on either, but not both, of those turns would still have LOS E, with a delay of approximately 65 seconds per vehicle. As this project does not contain provisions for extensive widening that would be required to provide receiving lanes for dual lefts, this is not recommended.

Roundabout Feasibility

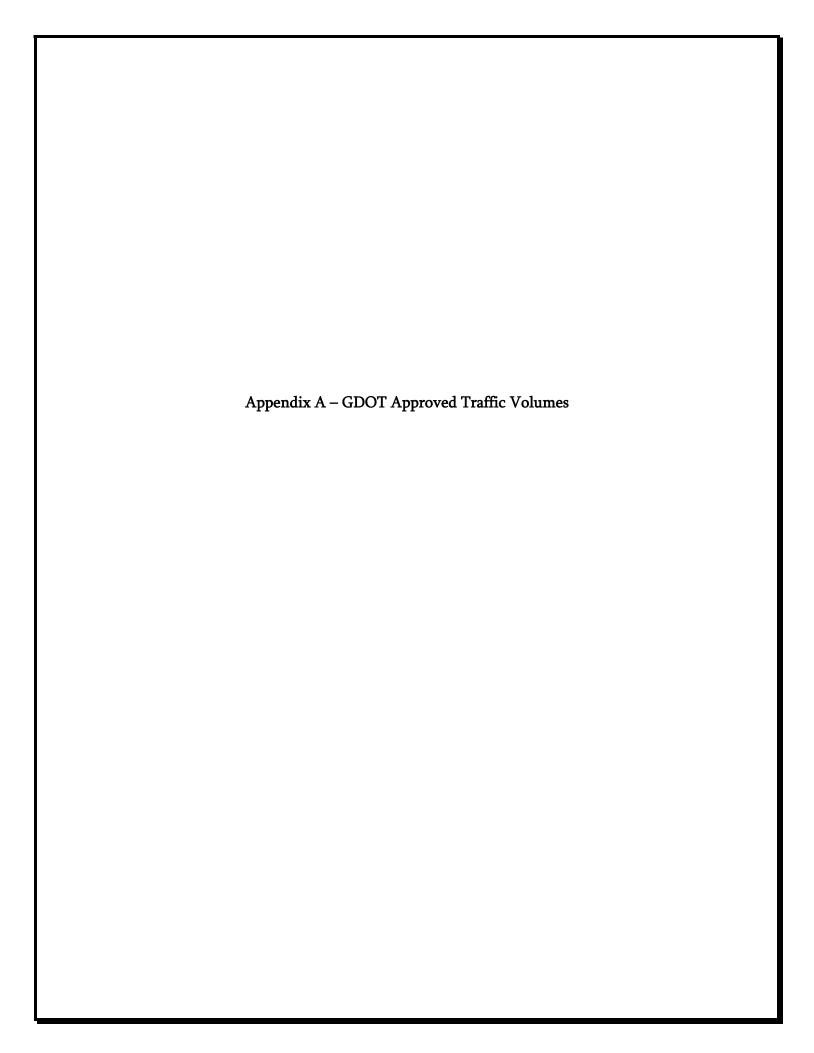
The project scope is for a bridge replacement and does not contemplate capacity improvements at either studied intersections. A roundabout was not considered at Northmont Parkway as this type of improvement is beyond the scope of this project.

A roundabout was not considered at Staunton due to the ratio of mainline (SR 120) traffic to sidestreet (Staunton Drive) traffic being greater than 90%.

Summary

In summary:

- The proposed improvements at SR 120 at Northmont Parkway maintain an acceptable level of service except in the design year (2040) PM peak hour.
- Improvements to achieve LOS D or better throughout the design year peak hours are beyond the scope of this project.
- Staunton Drive, while experiencing high delays for the side street traffic, only
 experiences this during the peak hours and does not warrant a traffic signal or
 roundabout.





MEMORANDUM

TO: Abby Ebodaghe

Georgia Department of Transportation

Office of Planning

FROM: William M. Ruhsam, Jr, P.E., PTOE

Kelly M. Cory, P.E., PTOE

SUBJECT: Summary of Design Traffic Projections

SR 120 at Singleton Creek

Gwinnett County, PI# 0132986

Michael Baker International Project # 144615

DATE: August 11, 2015

Context

Traffic projections have been produced for this project following the methods and procedures contained in the Georgia Department of Transportation (GDOT) Design Policy Manual Chapter 13.

Purpose

This memorandum is written to summarize and provide background information for the design traffic projections subject project. The SR 120 at Singleton Creek project will consist of replacing the existing bridge for SR 120 over Singleton Creek. A concept was developed about 12 years ago that showed replacing the bridge to the south side and it is expected this general layout will be retained. The total project length is 0.4 miles and includes two intersections in addition to the bridge replacement

Study Area

The study area is in the City of Duluth, Gwinnett County. The immediate study area includes SR 120 (Duluth Highway) from Northmount Parkway to Staunton Drive. See Figure 1 for a study area map which includes the relevant local GDOT count stations.

Traffic Counts in Georgia

County City Countries Stations
Country City Agency Search

Figure 1: Study Area Map

Source: Google, Inc., Georgia Department of Transportation

Annual Coverage Counts, Travel Demand Model & Growth Rates

GDOT historical annualized average daily traffic (AADT) data was obtained from three (3) traffic count stations in the vicinity of the project. The locations of the stations selected are shown in Figure 1 and the GDOT Traffic Count Database reports for each station are contained in Appendix A.

Using the historical data obtained, the historical growth rates for each station were examined using the least squares method for 5, 10, and 15 years. Discarding data from the count stations that were estimated values, the 10 year¹ annual growth rate was separately calculated. The annual counts are shown in Table 1. The growth rates are shown in Table 2.

¹ In some cases, due to the years with estimated counts, the 10-year actual growth rate is approximated by the 9-year rate. See the table for details of which years are estimated and which are actual.

Table 1: Annual Coverage Counts

Traffic Count Station	135-016	1	135-0163		135-0527	
Roadway	SR 120		SR 120		Boggs Roa	ıd
	Between		Between Kr	nox	Between S	R
Location	Buford Hv	٧y	Branch Cre	ek	120 and	
Location	and Knox	(and Satelli	te	Satellite	
	Branch Cre	ek	Blvd.		Blvd.	
1990	14,510	Α	15,012	Α	3,065	Α
1991	13,983	Α	15,775	Α	4,738	Α
1992	12,623	Α	14,263	Α	4,696	Α
1993	13,100	Α	14,200	Α	4,800	Α
1994	13,800	Α	15,600	Α	6,000	Α
1995	13,900	Α	15,700	Α	6,200	Α
1996	18,800	Α	21,500	Α	8,100	Α
1997	16,500	Α	19,200	Α	-	-
1998	19,600	Α	22,600	Α	9,600	Ε
1999	17,800	Ε	21,700	Ε	9,800	Ε
2000	20,300	Ε	25,900	Ε	11,600	Ε
2001	21,300	Ε	22,900	Α	11,900	Ε
2002	21,917	Ε	23,807	Ε	12,217	Ε
2003	20,680	Α	21,990	Α	10,820	Α
2004	24,290	Α	24,180	Α	13,160	Α
2005	21,620	Α	25,790	Α	12,870	Α
2006	21,690	Α	23,950	Α	12,120	Α
2007	20,330	Α	24,900	Ε	12,850	Ε
2008	24,060	Α	23,440	Ε	13,660	Α
2009	23,390	Ε	22,790	Ε	13,280	Ε
2010	18,110	Α	22,840	Ε	13,310	Ε
2011	18,090	Ε	20,470	Α	11,120	Α
2012	14,900	Α	20,360 E		11,060	Ε
2013	14,970	Ε	20,430	Α	11,110	Ε
2014	19,500	Α	20,400	Ε	11,100	Ε

[&]quot;A" indicates a count station that was actually counted that calendar year.

Source: Georgia Department of Transportation

[&]quot;E" indicates a count station that was estimated for that calendar year.

Table 2: Annual Growth Rates

		GDOT Count Station			
		135-0161	135-0163	135-0527	
Least Squares	15-year	-0.1%	-0.1%	0.0%	
Method	10-year	-0.1%	-0.2%	-0.2%	
Wethod	5-year	0.0%	-0.1%	-0.1%	
Using Actual Counts (As close to 10- year as possible)	Approx. 10-year	-0.5%	-0.7%	0.3%	
ARC Travel Demand Model	2015	21,092	1.2%		
Demand Model	2040	28,602	ARC G	rowth Rate	

Source: Michael Baker International

Within Table 2, all years' data were used for calculation of the Least Squares Method. As the Department prefers to only use actual traffic counts for grown predictions, the approximate ten-year rate² was calculated using a constant-rate regression calculation. Using these actual traffic counts, the rate of growth on SR 120 has been negative or zero over the last decade. The growth on Boggs Road has been positive, but low. The Atlanta Regional Commission travel demand model shows a 1.2% annual growth rate. In order to ensure that a conservative analysis is conducted and turn lanes are adequate, a 1.0% annual growth rate was selected for this project.

Traffic Counts

Michael Baker International conducted turning movement counts (TMCs), classification counts, and bi-directional volume counts on all roadways and intersections within the study area of the project. The traffic count location map is shown in Appendix B. All counts were taken while school was in session.

An evaluation of the count data shows that the morning peak hour occurs from 7:30 to 8:30 AM and the afternoon peak hour occurs from 5:00 to 6:00 PM. The count data was further analyzed to determine the K & D factors for the project area roadways, as discussed in the next section.

K & D Analysis

K-values and D-factors for the project area roadways were calculated using the most recent GDOT actual traffic counts and the volume counts collected for this project. A summary of the weighted K-values during each peak hour for the project area is shown below in Table 3.

² In only one instance could a 10-year growth evaluation be calculated (TC 135-0163) due to holes in the annual county data. In the other two calculations an 11-year (TC 135-0161) and an 8-year (TC 135-0527) were used.

Table 3: K-Values

	K-Value				
	AM Peak	PM Peak			
Project Area	0.07	0.07			
Weighted Average	0.07	0.07			
Mainline	0.08	0.08			
Weighted Average	0.00	0.08			
Sidestreet	0.06	0.05			
Weighted Average	0.00	0.03			

Source: Michael Baker International

The sidestreet Ks show weighted values at 0.06 and 0.05 for AM and PM respectively, however the K value is heavily adjusted by volumes on Boggs Road. An excerpt from the K & D worksheet is shown in Table 4. The actual measured K values for the side streets vary from 0.06 to 0.13, and reflect the volatility of low volume roadways. The K values for the sidestreets are reflected in the volume diagrams shown in the Appendix E.

Table 4: Excerpt from K & D Worksheet

					AM	PM	AM	PM
Count #	Year	Daily Traffic	Location Description	Mainline or Sidestreet		Hourly ffic	K Va	alue
2	2015	532	Northmont Pkwy north of SR 120	S	39	42	0.07	0.08
3	2015	7,744	Northmont Pkwy south of SR 120	S	694	746	0.09	0.10
5	2015	845	Staunton Dr. north of SR 120	S	112	56	0.13	0.07
6	2015	1,302	Staunton Dr. south of SR 120	S	79	87	0.06	0.07
135-0527	2015	24,320	Boggs Rd Between SR 120 and Satellite Blvd.	S	1038	860	0.04	0.04

Source: Michael Baker International

The full K & D worksheet is shown in Appendix C.

Truck Percentages

The truck classification percentages were measured on SR 120 at the east and west ends of the project area. The 24-hour, AM, and PM peak hour truck percentages were averaged across the two days of data gathered for this count. These raw truck percentages are shown along with the selected truck percentages, rounded to a half-percent, in Table 5.

Table 5: Truck Percentages

	SR 120 west of Northmont Pkwy						
	Single Unit	Combinatio	Total				
	Sirigic Offic	n	Total				
24-Hour	6.6%	0.5%	7.1%				
AM Peak	7.9%	0.5%	8.4%				
PM Peak	4.1%	0.4%	4.4%				
	SR 120	east of Staur	nton Dr				
24-Hour	6.9%	0.8%	7.8%				
AM Peak	7.7%	0.6%	8.3%				
PM Peak	5.3%	0.5%	5.7%				
Selected Truck Percentages							
24-Hour	7.0%	1.0%	8.0%				
Peak	8.0%	1.0%	9.0%				

Source: Michael Baker International, Inc.

Build vs. No Build

Based on the concept plan, there is no anticipated difference in traffic volume between the build and no-build concepts. The capacity of the roadway will not be increased.

Development of Design Traffic

Using the turning movement counts, the bi-directional volume counts, and the K and D values from the K & D worksheet, the 2015 traffic volumes were smoothed and balanced. The smoothed and balanced Peak Hour and Average Daily Traffic were projected to 2020 and 2040 using a 1.0% annual growth rate.

Per direction from the GDOT Office of Planning, two additional sets of traffic diagrams were prepared for years 2022 and 2040.

The design traffic volumes are shown in Appendix E.

List of Appendices

Appendix A: GDOT Count Station Reports

Appendix B: Traffic Count Data Appendix C: K&D Worksheet

Appendix D: Design Traffic Worksheets

Appendix E: Design Traffic

Appendix A: GDOT Count Station Reports





Short Term Station 1350161 In Gwinnett County Located on 012000 LRS ID: 1351012000

Abo	ut Station 1350161	
Station ID	1350161	
County	Gwinnett	
City		
Road		
Road functional class	urban - Minor Arterial	
Description		
	Route Number	012000
Routes	Concurrent Route Number	
Routes	Concurrent Route 2	
	Concurrent Route 3	
LRS Section ID	1351012000 @ 0.000 Miles	
Traffic Segment	2.460 to 4.440 Miles	
Coordinate (Lat/Lon)	33.989000, -84.132000	
Map Reference		



-6.27

0.32

-10.99



Short Term Station 1350161 In Gwinnett County Located on 012000 LRS ID: 1351012000



Short Term Station 1350161 In Gwinnett County Located on 012000 LRS ID: 1351012000

Year	Month	Status	Summary	Volume By Hour Class By Hour Speed Turning Movements	
2010	May	Count accepted	Summary By Day	/ All North South	1
2012	Mar	Count accepted	Summary By Day	γ All North South	
2014	Jan	Count accepted	Summary By Day	∠ All North South	
					_





Short Term Station 1350161 In Gwinnett County Located on 012000 LRS ID: 1351012000

Referencing Annual Statistics Surveys

Year	Month	Status	Summary	Volume By Hour	Class By Hour Speed	Turning Movements
2010	May	Count accepted	Summary By Day	All North South	=	
2012	Mar	Count accepted	Summary By Day	All North South	_	
2014	Jan	Count accepted	Summary By Day	All North South	_	

Volume By Hour Direction: All Directions

Time	Tue Feb 18	Wed Feb 19	Thu Feb 20	Total	Avg	Pct	Graphic
12:00 am		64	74	138	69	0.35	
1:00 am		32	46	78	39	0.20	•
2:00 am		44	48	92	46	0.23	•
3:00 am		36	40	76	38	0.19	•
4:00 am		98	70	168	84	0.42	•
5:00 am		260	304	564	282	1.41	
6:00 am		1016	954	1970	985	4.93	
7:00 am		1576	1540	3116	1558	7.79	
8:00 am		1676	1630	3306	1653	8.27	
9:00 am		1236	1240	2476	1238	6.19	
10:00 am		960	858	1818	909	4.55	
11:00 am		918	942	1860	930	4.65	
12:00 pm	1028	1012		2040	1020	5.10	
1:00 pm	1110	1142		2252	1126	5.63	
2:00 pm	1268	1228		2496	1248	6.24	
3:00 pm	1442	1380		2822	1411	7,06	
4:00 pm	1584	1544		3128	1564	7.82	
5:00 pm	1712	1712		3424	1712	8.56	
6:00 pm	1494	1424		2918	1459	7.30	
7:00 pm	1070	1024		2094	1047	5.24	
8:00 pm	638	636		1274	637	3.19	
9:00 pm	428	554		982	491	2.46	
10:00 pm	302	250		552	276	1.38	
11:00 pm	164	188		352	176	0.88	
Total	12240	20010	7746	39996	19998		
SF	1.047	1.047	1.047				
DF	0.931	0.935	0.929				
AADT		19596			19535		





Short Term Station 1350163 In Gwinnett County Located on 012000 LRS ID: 1351012000

About Station 1350163						
Station ID	1350163					
County	Gwinnett					
City						
Road						
Road functional class	urban - Minor Arterial					
Description						
	Route Number	012000				
Routes	Concurrent Route Number					
Routes	Concurrent Route 2					
	Concurrent Route 3					
LRS Section ID	1351012000 @ 0.000 Miles					
Traffic Segment	4.440 to 5.680 Miles					
Coordinate (Lat/Lon)	33.978500, -84.104700					
Map Reference						



2004

24180



Short Term Station 1350163 In Gwinnett County Located on 012000 LRS ID: 1351012000

	Aimaars	ш	Surveys		1	T -	
		Volume				т	rucks
-	20430						
	20430						
	20360 20470						
	22840						
	22790						
	23440						
	24900						
	23950						
2005	25790		-				
2004	24180						
2003	21990						
2002	23807						
	22900						
	25900		-				
	21700						
	22600						
	19200						
	21500						
	L5700 						
	15600						
	14200						
	14263						
	15775 15012						
1550	15012		1				
		Key	Annual	Trends	1		
		_	Annual				
	Annual		Average				
	Average		Daily				85th
	Daily	% APR	Truck	%	K	D	Pctl
Year	Traffic	Change	Traffic	Trucks	Factor	Factor	Speed
201	4 20430	0.00					
201	20430	0.34			9.00		
201	20360	-0.54					
201	1 20470	-10.38					
201							
200							
200							
200							
200							
200							
	23,30	0.00					



Short Term Station 1350163 In Gwinnett County Located on 012000 LRS ID: 1351012000

Year	Month	Status	Summary	Volume By Hour	Class By Hour Spe	ed Turning Movements
2011	Mar	Count accepted	Summary By Day	All North South	4	
2013	Mar	Count accepted	Summary By Day	All North South		
2015	Feb	Count accepted	Summary By Day	All North South	📥	





Short Term Station 1350163 In Gwinnett County Located on 012000 LRS ID: 1351012000

Referencing Annual Statistics Surveys

Year	Month	Status	Summary	Volume By Hour	Class By Hour Speed	Turning Movements
2011	Mar	Count accepted	Summary By Day	All North South	4	
2013	Mar	Count accepted	Summary By Day	All North South	.	
2015	Feb	Count accepted	Summary By Day	All North South	₫	

Volume By Hour Direction: All Directions

Time	Tue Mar 17	Wed Mar 18	Thu Mar 19	Total	Avg	Pct	Graphic
12:00 am		140	126	266	133	0.57	
1:00 am		70	68	138	69	0.30	
2:00 am		60	66	126	63	0.27	
3:00 am		70	86	156	78	0.33	
4:00 am		128	132	260	130	0.56	
5:00 am		394	344	738	369	1.58	
6:00 am		1158	1052	2210	1105	4.74	
7:00 am		1646	1554	3200	1600	6.86	
8:00 am		1794	1682	3476	1738	7.45	
9:00 am		1480	1386	2866	1433	6.14	
10:00 am		1080	1002	2082	1041	4.46	
11:00 am		1164	1058	2222	1111	4.76	
12:00 pm	1358	1288		2646	1323	5.67	
1:00 pm	1308	1388		2696	1348	5.78	
2:00 pm	1460	1410		2870	1435	6.15	
3:00 pm	1448	1486		2934	1467	6,29	
4:00 pm	1634	1726		3360	1680	7.20	
5:00 pm	1988	1868		3856	1928	8.27	
6:00 pm	1702	1690		3392	1696	7,27	
7:00 pm	1242	1410		2652	1326	5.69	
8:00 pm	894	964		1858	929	3.98	
9:00 pm	636	714		1350	675	2.89	
10:00 pm	406	414		820	410	1.76	
11:00 pm	244	222		466	233	1.00	
Total	14320		8556	46640	23320		
SF	0.000		0.000				
DF	0.000		0.000				
AADT		0			0		





Short Term Station 1350527 In Gwinnett County Located on 055200 LRS ID: 1352055200

About Station 1350527						
Station ID	1350527					
County	Gwinnett					
City						
Road						
Road functional class	urban - Minor Arterial					
Description						
	Route Number	055200				
Routes	Concurrent Route Number					
Routes	Concurrent Route 2					
	Concurrent Route 3					
LRS Section ID	1352055200 @ 0.000 Miles					
Traffic Segment	1.300 to 2.220 Miles					
Coordinate (Lat/Lon)	33.971800, -84.098900					
Map Reference						





Short Term Station 1350527 In Gwinnett County Located on 055200 LRS ID: 1352055200

		Volume	Trucks
2014	11100		
2013	11110		
2012	11060		
2011	11120		
2010	13310		
2009	13280		
2008	13660		
2007	12850		
2006	12120		
2005	12870		
2004	13160		
2003	10820		
2002	12217		
2001	11900		
2000	11600		
1999	9800		
1998	9600		
1997	-		
1996	8100		
1995	6200		
1994	6000		
1993	4800		
1992	1000		
1991	4738		
1990	3065	-	
		Key Annual Trends	
	Annu	Annual	

	Annual Average Daily	% APR	Annual Average Daily Truck	%	к	D	85th Pctl
Year	Traffic	Change	Traffic	Trucks	Factor	Factor	Speed
2014	11100	-0.09					
2013	11110	0.45					
2012	11060	-0.54					
2011	11120	-16.45					
2010	13310	0.23					
2009	13280	-2.78					
2008	13660	6.30					
2007	12850	6.02					
2006	12120	-5.83					
2005	12870	-2.20					
2004	13160						





Short Term Station 1350527 In Gwinnett County Located on 055200 LRS ID: 1352055200

2011 Mar Count accepted Summary By Day All East West 2015 Feb Count accepted Summary By Day All East West \$\frac{1}{2}\$	Year	Month	Status	Summary	Volume By Hour	Class By Hour Speed	Turning Movements
2015 Feb Count accepted Summary By Day All East West	2011	Mar	Count accepted	Summary By Day	All East West	.	
	2015	Feb	Count accepted	Summary By Day	All East West		

Appendix B: Traffic Count Data

CLASSIFICATION

SR 120/Duluth Hwy E/O Staunton Dr

Day: Wednesday Date: 5/13/2015

City: Duluth Project #: GA15_9189_007

Summary															
Time	# 1	# 2	# 3	# 4	# 5	# 6	# 7	# 8	# 9	# 10	# 11	# 12	# 13	Total	
00:00 AM	0	112	11	1	7	1	0	5	0	0	0	0	0	137	
01:00	0	59	3	0	2	0	0	3	0	0	0	0	0	67	
02:00	0	42	1	1	2	0	0	2	1	0	0	0	0	49	
03:00	0	43	3	1	5	0	0	2	1	0	0	0	0	55	
04:00	0	106	13	0	6	0	0	1	1	0	0	0	0	127	
05:00	1	332	38	3	30	1	0	3	0	0	0	0	0	408	
06:00	5	926	140	5	82	2	0	4	5	0	0	0	0	1169	
07:00	3	1354	204	10	121	3	0	4	5	0	0	0	0	1704	
08:00	0	1403	159	8	117	3	0	6	6	0	0	0	0	1702	
09:00	3	1077	162	2	101	4	0	5	6	0	0	0	0	1360	
10:00	0	923	168	8	89	8	0	7	4	0	0	0	0	1207	
11:00	4	941	160	7	76	6	1	6	8	0	0	0	0	1209	
12:00 PM	7	1072	174	5	108	3	0	7	9	0	0	0	0	1385	
13:00	2	1020	170	8	92	3	0	8	8	0	0	0	0	1311	
14:00	5	1151	155	7	97	4	0	10	8	0	0	0	0	1437	
15:00	2	1131	166	12	114	1	0	7	9	0	0	0	0	1442	
16:00	2	1380	185	7	107	1	0	8	5	0	0	0	0	1695	
17:00	3	1667	168	4	99	2	0	4	5	0	0	0	0	1952	
18:00	4	1476	197	3	85	0	0	4	2	0	0	0	0	1771	
19:00	2	1160	131	0	78	1	0	1	0	0	0	0	0	1373	
20:00	2	802	86	2	52	0	0	0	1	0	0	0	0	945	
21:00	0	727	81	0	39	0	0	1	2	0	0	0	0	850	
22:00	0	422	35	0	18	0	0	4	2	0	0	0	0	481	
23:00	1	240	20	1	9	0	0	3	1	0	0	0	0	275	
Totals	46	19566	2630	95	1536	43	1	105	89					24111	
% of Totals	0%	81%	11%	0%	6%	0%	0%	0%	0%					100%	
AM Volumes	16	7318	1062	46	638	28	1	48	37	0	0	0	0	9194	
% AM	0%	30%	4%	0%	3%	0%	0%	0%	0%					38%	
AM Peak Hour	06:00	08:00	07:00	07:00	07:00	10:00	11:00	10:00	11:00					07:00	
Volume	5	1403	204	10	121	8	1	7	8					1704	
PM Volumes	30	12248	1568	49	898	15	0	57	52	0	0	0	0	14917	
% PM	0%	51%	7%	0%	4%	0%		0%	0%					62%	
PM Peak Hour	12:00	17:00	18:00	15:00	15:00	14:00		14:00	12:00					17:00	
Volume	7	1667	197	12	114	4		10	9					1952	
Dir	ectional Pe	ak Periods		AM 7-9			NOON 12-2			PM 4-6		Off	Peak Volun	nes	
		All Classes	Volume		%	Volume		%	Volume		%	Volume		%	
			3406	\longleftrightarrow	14%	2696	\longleftrightarrow	11%	3647	\longleftrightarrow	15%	14362	\longleftrightarrow	60%	

1 Motorcycles

3 2-Axle, 4-Tire Single Units

- 2 Passenger Cars
- 4 Buses
- 5 2-Axle, 6-Tire Single Units

6 3-Axle Single Units

7 > =4-Axle Single Units

Classification Definitions

- 8 <=4-Axle Single Trailers
- **9** 5-Axle Single Trailers
- 10 >=6-Axle Single Trailers
- 11 <=5-Axle Multi-Trailers
- 12 6-Axle Multi-Trailers
- 13 >=7-Axle Multi-Trailers

VOLUME

Staunton Dr S/O SR 120/Duluth Hwy

Day: Wednesday Date: 5/13/2015

DAILY TOTALS					NB	SB		EB		WB						То	tal	
	U#	AILY I	UIA	(L)		650	652		0		0						1,3	302
AM Period	NB		SB		EB	WB	TO	TAL	PM Period	NB		SB		EB	WE	3	TO	TAL
00:00	3		6				9		12:00	9		12					21	
00:15	1		1				2		12:15	8		10					18	
00:30 00:45	1 2	7	3 2	12			4	19	12:30 12:45	8 6	31	9 12	43				17 18	74
01:00	0		2	12			2	15	13:00	15	31	8	43				23	74
01:15	Ö		2				2		13:15	11		11					22	
01:30	1		1				2		13:30	4		6					10	
01:45	0	1	1	6			1	7	13:45	3	33	11	36				14	69
02:00 02:15	0 0		3 0				3		14:00 14:15	7 6		7 10					14 16	
02:30	1		0				1		14:30	7		10					17	
02:45	0	1	0	3			0	4	14:45	10	30	15	42				25	72
03:00	0		1				1		15:00	8		9					17	
03:15	0		0				0		15:15	16		13					29	
03:30 03:45	0 1	1	0 1	2			0	3	15:30 15:45	13 15	52	13 13	48				26 28	100
04:00	0		1				1	<u> </u>	16:00	9	32	9	40				18	100
04:15	0		0				Ō		16:15	8		16					24	
04:30	0		0				0		16:30	8		18					26	
04:45	0		0	1			0	11	16:45	14	39	6	49				20	88
05:00	3		2				5		17:00	11		9					20	
05:15 05:30	6 1		0 0				6 1		17:15 17:30	11 13		7 9					18 22	
05:45	3	13	0	2			3	15	17:45	9	44	18	43				27	87
06:00	4		4				8		18:00	13		18					31	
06:15	2		2				4		18:15	9		17					26	
06:30	8		2	_			10		18:30	11		10					21	
06:45 07:00	<u>4</u> 12	18	<u>1</u>	9			5 18	27	18:45 19:00	<u>5</u> 8	38	8 12	53				13 20	91
07:00 07:15	12		5				17		19:15	7		11					18	
07:30	14		2				16		19:30	6		13					19	
07:45	14	52	3	16			17	68	19:45	12	33	8	44				20	77
08:00	16		7				23		20:00	7		14					21	
08:15 08:30	14		9				23 19		20:15	6		14					20 14	
08:45	15 16	61	4 2	22			18	83	20:30 20:45	4 4	21	10 10	48				14	69
09:00	15	- 01	9				24		21:00	4		6	-10				10	- 05
09:15	16		8				24		21:15	4		7					11	
09:30	15		10				25		21:30	9		13					22	
09:45	21	67	7	34			28	101	21:45	4	21	13	39				17	60
10:00 10:15	7 11		15 9				22 20		22:00 22:15	6 2		9 5					15 7	
10:30	7		5				12		22:30	2		5					7	
10:45	8	33	6	35			14	68	22:45	0	10	10	29				10	39
11:00	6		5				11		23:00	4		5					9	
11:15	12		7				19		23:15	2		2					4	
11:30 11:45	9 11	38	4 5	21			13 16	59	23:30 23:45	0 0	6	3 5	15				3 5	21
TOTALS	11	292	<u> </u>	163			10	455	TOTALS	U	358	<u> </u>	489				3	847
SPLIT %		64.2%		35.8%				34.9%	SPLIT %		42.3%		57.7%					65.1%
	D/	AILY T	ΌΤΔ	us		NB	SB		EB		WB							tal
		TIET I	017			650	652		0		0						1,3	302
AM Peak Hour		09:00		09:30				09:00	PM Peak Hour		15:15		17:45					17:30
AM Pk Volume		67		41				101	PM Pk Volume		53		63					106
Pk Hr Factor		0.798		0.683				0.902	Pk Hr Factor		0.828		0.875					0.855
7 - 9 Volume		113		38	0	0		151	4 - 6 Volume		83		92	C		0		175
7 - 9 Peak Hour		08:00		07:45				08:00	4 - 6 Peak Hour		16:45		16:00					16:15
7 - 9 Pk Volume		61		23				83	4 - 6 Pk Volume		49		49					90
Pk Hr Factor		0.953		0.639	0.000	0.000		0.902	Pk Hr Factor		0.875		0.681	0.0	00	0.000		0.865

VOLUME

Staunton Dr N/O SR 120/Duluth Hwy

Day: Wednesday Date: 5/13/2015

	DΛ	ILY T	OT A	110		NB		SB		EB		WB						To	otal
	DA	ILY I	UIA	NL3		428		417		0		0						8	45
AM Period	NB		SB		ЕВ	WB		TO	TAL	PM Period	NB		SB		EB	W	3	TO	TAL
00:00	2		0			***		2		12:00	4		0				,	4	.,,,_
00:15	2		1					3		12:15	3		11					14	
00:30	0	_	0	•				0	_	12:30	4		3	4.0				7	2.5
00:45 01:00	0	5	0	2				0	7	12:45 13:00	<u>6</u> 3	17	<u>5</u> 2	19				11 5	36
01:15	0		0					0		13:15	10		3					13	
01:30	1		0					1		13:30	5		6					11	
01:45	1	2	0					1	2	13:45	5	23	6	17				11	40
02:00 02:15	0 1		0 0					0 1		14:00 14:15	4 7		2 3					6 10	
02:30	Ō		Ö					0		14:30	7		4					11	
02:45	4	5	0					4	5	14:45	8	26	5	14				13	40
03:00	0		1					1		15:00	15		4					19	
03:15 03:30	0 0		0 0					0		15:15 15:30	4 3		5 10					9 13	
03:45	0		0	1				0	1	15:45	4	26	0	19				4	45
04:00	0		0					0		16:00	4		4					8	
04:15	1		1					2		16:15	5		4					9	
04:30 04:45	0 0	1	0 1	2				0 1	3	16:30 16:45	5 7	21	3 4	15				8 11	36
05:00	0		0					0	<u> </u>	17:00	7	21	4	13				11	30
05:15	0		4					4		17:15	9		5					14	
05:30	1	_	6	4.0				7		17:30	8	•	8					16	
05:45 06:00	1	2	3	12				3	14	17:45 18:00	5 10	29	10 6	27				15 16	56
06:00	1		4					5		18:15	11		2					13	
06:30	Ō		1					1		18:30	13		8					21	
06:45	0	2	3	11				3	13	18:45	13	47	4	20				17	67
07:00 07:15	1 1		2 7					3 8		19:00 19:15	9 11		2 8					11 19	
07:30	4		14					0 18		19:30	10		0 11					21	
07:45	6	12	33	56				39	68	19:45	8	38	6	27				14	65
08:00	13		25					38		20:00	5		6					11	
08:15 08:30	10 4		7 8					17 12		20:15 20:30	9 6		2 4					11 10	
08:45	2	29	10	50				12	79	20:45	8	28	3	15				11	43
09:00	6		5					11		21:00	17		2					19	
09:15	5		9					14		21:15	5		5					10	
09:30	4 4	10	11	20				15 9	49	21:30 21:45	7 6	25	13	21				20 7	F.6
09:45 10:00	8	19	5 10	30				18	49	22:00	3	35	1	21				4	56
10:15	4		9					13		22:15	3		1					4	
10:30	3		4					7		22:30	1		0					1	
10:45	3 10	18	5 4	28				8 14	46	22:45 23:00	3	10	2	4				5 5	14
11:00 11:15	10 3		4 7					14 10		23:00 23:15	2		2 0					2	
11:30	4		7					11		23:30	2		0					2	
11:45	7	24	7	25				14	49	23:45	2	9	0	2				2	11
TOTALS		119		217					336	TOTALS		309		200					509
SPLIT %	3	35.4%		64.6%					39.8%	SPLIT %		60.7%		39.3%					60.2%
,.																			
	DA	ILY T	OTA	\LS		NB		SB		EB		WB							tal
						428		417		0		0						8	45
AM Peak Hour		07:30		07:15					07:30	PM Peak Hour		18:00		19:15					18:30
AM Pk Volume		33		79					112	PM Pk Volume		47		31					68
Pk Hr Factor		0.635		0.598					0.718	Pk Hr Factor		0.904		0.705					0.810
7 - 9 Volume		41		106	0		0		147	4 - 6 Volume		50		42	0		0		92
7 - 9 Peak Hour		07:30		07:15					07:30	4 - 6 Peak Hour		16:45		17:00					17:00
7 - 9 Pk Volume		33		79					112	4 - 6 Pk Volume		31		27					56
Pk Hr Factor		0.635		0.598	0.000		0.000		0.718	Pk Hr Factor		0.861		0.675	0.0	JU	0.000		0.875

VOLUME

SR 120/Duluth Hwy E/O Northmont Pkwy

Day: Wednesday Date: 5/13/2015

	DAILY TOTALS			NB		SB		EB		WB						To	otal
	DAILT TOTALS			0		0		12,114	:	12,367						24,	,481
AM Period	NB SB	EB		WB		TO	TAL	PM Period	NB		SB	EB		WB		TO	TAL
00:00		23		16		39		12:00				223		168		391	
00:15		19		24		43		12:15				177		173		350	
00:30 00:45		17 12	71	20 13	72	37	144	12:30 12:45				173 161	724	157 175	672	330	1407
01:00		8	/1	5	73	25 13	144	13:00				171	734	177	673	336 348	1407
01:15		10		6		16		13:15				168		144		312	
01:30		12		10		22		13:30				145		160		305	
01:45		9	39	5	26	14	65	13:45				171	655	168	649	339	1304
02:00		7		3		10		14:00				178		169		347	
02:15 02:30		4 6		8 9		12 15		14:15 14:30				200 202		169 174		369 376	
02:45		8	25	9	29	17	54	14:45				207	787	175	687	382	1474
03:00		4		4		8		15:00				230		138		368	
03:15		15		9		24		15:15				190		163		353	
03:30		6	22	8	25	14		15:30				219	026	176	620	395	4.47.4
03:45 04:00		7 11	32	<u>4</u> 6	25	11 17	57	15:45 16:00				197 222	836	161 182	638	358 404	1474
04:00		14		12		26		16:15				253		177		430	
04:30		17		27		44		16:30				243		188		431	
04:45		16	58	27	72	43	130	16:45				263	981	174	721	437	1702
05:00		27		44		71		17:00				288		195		483	
05:15		26		71		97		17:15				280		239		519	
05:30 05:45		41 37	131	74 92	281	115 129	412	17:30 17:45				266 266	1100	226 207	867	492 473	1967
06:00		74	131	125	201	199	412	18:00				246	1100	224	807	470	1507
06:15		79		179		258		18:15				278		210		488	
06:30		109		223		332		18:30				234		188		422	
06:45		117	379	260	787	377	1166	18:45				243	1001	179	801	422	1802
07:00		144		249		393		19:00				233		157		390	
07:15 07:30		121 139		275 300		396 439		19:15 19:30				200 189		158 148		358 337	
07:45		212	616	290	1114	502	1730	19:45				182	804	145	608	327	1412
08:00		210		283		493		20:00				161		113		274	
08:15		204		267		471		20:15				142		120		262	
08:30		164		248		412		20:30				124		109		233	
08:45		150	728	244	1042	394	1770	20:45				128 136	555	85 97	427	213	982
09:00 09:15		147 143		206		386 349		21:00 21:15				155		94		233 249	
09:30		151		209		360		21:30				111		86		197	
09:45		121	562	187	841	308	1403	21:45				84	486	97	374	181	860
10:00		168		195		363		22:00				94		83		177	
10:15		112		160		272		22:15				48		53		101	
10:30		113	E 42	161	CEO	274	1202	22:30				43	227	47	220	90	466
10:45 11:00		150 135	543	143 148	659	293 283	1202	22:45 23:00				42 61	227	<u>56</u> 39	239	98 100	466
11:15		150		131		281		23:15				44		32		76	
11:30		160		160		320		23:30				25		28		53	
11:45		164	609	167	606	331	1215	23:45				25	155	29	128	54	283
TOTALS			3793		5555		9348	TOTALS					8321		6812		15133
SPLIT %			40.6%		59.4%		38.2%	SPLIT %					55.0%		45.0%		61.8%
				NB		SB		EB		WB						To	otal
	DAILY TOTALS			0		0		12,114		12,367							,481
AM Peak Hour			07:45		07:15		07:30	PM Peak Hour					17:00		17:15		17:00
AM Pk Volume			790		1148		1905	PM Pk Volume					1100		896		1967
Pk Hr Factor			0.932		0.957		0.949	Pk Hr Factor					0.955		0.937		0.947
7 - 9 Volume	0 0		1344		2156		3500	4 - 6 Volume		0	0		2081		1588		3669
7 - 9 Peak Hour			07:45		07:15		07:30	4 - 6 Peak Hour					17:00		17:00		17:00
7 - 9 Pk Volume			790		1148		1905	4 - 6 Pk Volume					1100		867		1967
Pk Hr Factor	0.000 0.000		0.932		0.957		0.949	Pk Hr Factor		0.000	0.0	00	0.955		0.907		0.947
			·		·		·	·									·

VOLUME

Northmont Pkwy S/O SR 120/Duluth Hwy

Day: Wednesday Date: 5/13/2015

	D	AILY 1	TOT A	VI C		NB		SB		EB		WB						To	otal
	וט	AILI I	1014	(L)		3,594	4	4,150)	0		0						7,	744
AM Period	NB		SB		ЕВ	WB		то	TAL	PM Period	NB		SB		ЕВ	W	В	TO	TAL
00:00	13		7					20		12:00	77		57					134	
00:15	10		6					16		12:15	64		61					125	
00:30 00:45	4 5	32	4 3	20				8 8	52	12:30 12:45	68 53	262	74 72	264				142 125	526
01:00	5	32	1	20				6	32	13:00	72	202	78	204				150	320
01:15	6		4					10		13:15	58		76					134	
01:30	1		3					4		13:30	61		44					105	
01:45 02:00	3	14	<u>5</u> 3	13				<u>7</u>	27	13:45 14:00	53 52	244	66 64	264				119 116	508
02:00	0		2					2		14:15	52 47		63					110	
02:30	4		2					6		14:30	52		52					104	
02:45	3	10	1	8				4	18	14:45	61	212	55	234				116	446
03:00	2		2					4		15:00	62		33					95	
03:15 03:30	0 5		1 3					1 8		15:15 15:30	51 60		65 56					116 116	
03:45	10	17	4	10				14	27	15:45	54	227	51	205				105	432
04:00	4		2					6		16:00	70		51					121	
04:15	2		4					6		16:15	70		46					116	
04:30	2	12	6	22				8	26	16:30	95	220	37	101				132	F10
04:45 05:00	5 14	13	11 8	23				16 22	36	16:45 17:00	94 149	329	47 66	181				141 215	510
05:15	16		4					20		17:15	113		63					176	
05:30	5		5					10		17:30	115		75					190	
05:45	12	47	17	34				29	81	17:45	100	477	65	269				165	746
06:00	9		15					24		18:00	82		73					155	
06:15 06:30	12 25		29 52					41 77		18:15 18:30	88 72		58 52					146 124	
06:45	31	77	78	174				109	251	18:45	53	295	42	225				95	520
07:00	31		108					139		19:00	63	233	44					107	320
07:15	20		113					133		19:15	54		49					103	
07:30	44		124					168		19:30	51		48					99	
07:45 08:00	44	139	124 122	469				168 162	608	19:45 20:00	51 58	219	49 28	190				100 86	409
08:15	46		150					196		20:15	43		19					62	
08:30	31		125					156		20:30	32		22					54	
08:45	31	148	136	533				167	681	20:45	32	165	19	88				51	253
09:00	30		96					126		21:00	38		29					67	
09:15 09:30	29 36		82 74					111 110		21:15 21:30	34 34		35 18					69 52	
09:45	27	122	74 76	328				103	450	21:45	18	124	28	110				46	234
10:00	24		63	320				87	130	22:00	23	121	17	110				40	
10:15	41		68					109		22:15	22		7					29	
10:30	30	425	32	227				62	252	22:30	8	F0	6					14	400
10:45 11:00	30 36	125	64 45	227				94 81	352	22:45 23:00	<u>6</u> 20	59	<u>14</u> 6	44				20 26	103
11:15	40		53					93		23:15	14		7					21	
11:30	50		49					99		23:30	6		5					11	
11:45	56	182	61	208				117	390	23:45	15	55	11	29				26	84
TOTALS		926		2047					2973	TOTALS		2668		2103					4771
SPLIT %		31.1%		68.9%					38.4%	SPLIT %		55.9%		44.1%					61.6%
	_	0 11 24-	-0=-			NB		SB		ЕВ		WB						To	otal
	D	AILY 1	OTA	ILS		3,594	4	4,150)	0		0							744
ANA De-latte		11.45		00:00						PM Peak Hour		17:00		12,20					
AM Peak Hour AM Pk Volume		11:45 265		08:00 533					07:30 694	PM Pk Volume		17:00 477		12:30 300					17:00 746
Pk Hr Factor		0.860		0.888					0.885	Pk Hr Factor		0.800		0.962					0.867
7 - 9 Volume		287		1002	0		0		1289	4 - 6 Volume		806		450)	0		1256
7 - 9 Peak Hour		07:30		08:00					07:30	4 - 6 Peak Hour		17:00		17:00					17:00
7 - 9 Pk Volume		174		533					694	4 - 6 Pk Volume		477		269					746
Pk Hr Factor		0.946		0.888	0.00	0 0	.000		0.885	Pk Hr Factor		0.800		0.897	0.0	000	0.00	0	0.867

VOLUME

Northmont Pkwy N/O SR 120/Duluth Hwy

Day: Wednesday Date: 5/13/2015

	D/	AILY T	OT/	VI C		NB	SB		EB		WB						To	otal
	יט	AILI I	UIF	AL3		263	269		0		0						5	32
AM Period	NB		SB		EB	WB	TC	OTAL	PM Period	NB		SB		ЕВ	WB		TO	TAL
00:00	2		1			VVD	3	, IAL	12:00	3		4	•	-0	VVD		7	177.2
00:15	0		0				ő		12:15	4		5					9	
00:30	0		0				0		12:30	8		8					16	
00:45	0	2	0	1			0	3	12:45	7	22	5	22				12	44
01:00	0		0				0		13:00	1		4					5	
01:15	0		0				0		13:15	2		4					6	
01:30	0		0				0		13:30	3 2	0	1 0	0				4	17
01:45 02:00	0		0				0		13:45 14:00	6	8	2	9			-	2 8	17
02:15	1		0				1		14:15	5		3					8	
02:30	0		Ō				0		14:30	3		4					7	
02:45	0	1	0				0	1	14:45	2	16	5	14				7	30
03:00	0		0				0		15:00	8		7					15	
03:15	0		0				0		15:15	3		3					6	
03:30	0		0				0		15:30	7	22	4	4.5				11	27
03:45 04:00	<u>0</u> 1		<u>0</u>				2		15:45 16:00	2	22	1 1	15				5 3	37
04:00	0		1				1		16:15	4		6					10	
04:30	0		0				0		16:30	4		4					8	
04:45	0	1	Ō	2			Ō	3	16:45	5	15	3	14				8	29
05:00	0		0				0		17:00	2		2			-		4	
05:15	0		1				1		17:15	8		4					12	
05:30	0		1	_			1		17:30	7		3					10	
05:45	0		1	3			1	3	17:45	11	28	5	14				16	42
06:00	1		3				4		18:00 18:15	7		3					10	
06:15 06:30	1 2		5 7				6 9		18:30	5 7		11 5					16 12	
06:45	1	5	5	20			6	25	18:45	7	26	5	24				12	50
07:00	0		2				2		19:00	6		2					8	
07:15	1		6				7		19:15	5		5					10	
07:30	2		6				8		19:30	2		2					4	
07:45	3	6	4	18			7	24	19:45	4	17	3	12				7	29
08:00	2		9				11		20:00	5		3					8	
08:15 08:30	7 3		6 7				13 10		20:15 20:30	1 5		1 0					2 5	
08:45	3	15	9	31			12	46	20:30	5 5	16	2	6				7	22
09:00	1	13	5	<u> </u>			6		21:00	7	10	2					9	
09:15	2		5				7		21:15	7		1					8	
09:30	3		9				12		21:30	7		1					8	
09:45	5	11	5	24			10	35	21:45	2	23	2	6				4	29
10:00	1		6				7		22:00	2		3					5	
10:15	0		5				5		22:15	1		0					1	
10:30 10:45	1 1	3	3 2	16			4	19	22:30 22:45	3 5	11	0 1	4				3 6	15
11:00	4	э	4	10			8	19	23:00	1	11	0	4			+	1	13
11:15	2		5				7		23:15	0		0					0	
11:30	5		2				7		23:30	0		Ö					0	
11:45	3	14	2	13			5	27	23:45	0	1	1	1				1	2
TOTALS		58		128				186	TOTALS		205		141					346
SPLIT %		31.2%		68.8%				35.0%	SPLIT %		59.2%		10.8%					65.0%
	D/	AILY T	OT/	AIS		NB	SB		EB		WB							otal
		-U-U-U	- 01/	TLO		263	269		0		0						5	32
AM Peak Hour		11:45		08:00				08:00	PM Peak Hour		17:15		17:45					17:45
AM Pk Volume		18		31				46	PM Pk Volume		33		24					54
Pk Hr Factor		0.563		0.861				0.885	Pk Hr Factor		0.750		0.545					0.844
7 - 9 Volume		21		49	0	0		70	4 - 6 Volume		43		28	0		n		71
7 - 9 Peak Hour		07:45		08:00				08:00	4 - 6 Peak Hour		17:00		16:15					17:00
7 - 9 Pk Volume		15		31				46	4 - 6 Pk Volume		28		15					42
Pk Hr Factor		0.536		0.861				0.885	Pk Hr Factor		0.636		0.625					0.656
		2.330		0.001	0.000	0.000					2.330			0.00				2.500

CLASSIFICATION

SR 120/Duluth Hwy W/O Northmont Pkwy

Day: Wednesday Date: 5/13/2015

City: Duluth

Project #: GA15_9189_001

Summary

Summary														
Time	# 1	# 2	# 3	# 4	# 5	# 6	#7	# 8	# 9	# 10	# 11	# 12	# 13	Total
00:00 AM	1	120	10	1	5	1	0	0	0	0	0	0	0	138
01:00	0	65	3	0	2	0	0	1	0	0	0	0	0	71
02:00	0	50	2	0	1	0	0	1	1	0	0	0	0	55
03:00	0	47	3	0	1	0	0	1	0	0	0	0	0	52
04:00	0	112	10	0	5	0	0	1	1	0	0	0	0	129
05:00	2	357	31	2	26	1	0	2	0	0	0	0	0	421
06:00	2	979	140	8	94	1	0	3	4	0	0	0	0	1231
07:00	2	1454	207	15	128	2	0	5	5	0	0	0	0	1818
08:00	0	1593	184	10	117	2	0	3	5	0	0	0	0	1914
09:00	2	1139	166	3	101	7	0	7	11	0	0	0	0	1436
10:00	0	950	156	11	96	9	0	2	3	0	0	0	0	1227
11:00	2	856	153	8	83	5	1	4	4	0	0	0	0	1116
12:00 PM	2	1028	172	6	91	4	0	4	4	0	0	0	0	1311
13:00	2	1022	163	8	79	3	0	4	3	0	0	0	0	1284
14:00	5	1144	175	9	117	4	0	6	10	0	0	0	0	1470
15:00	1	1303	163	13	103	4	1	4	5	0	0	0	0	1597
16:00	5	1491	167	4	105	1	0	6	4	0	0	0	0	1783
17:00	2	1719	177	5	75	0	1	4	3	0	0	0	0	1986
18:00	2	1574	182	2	100	0	0	3	1	0	0	0	0	1864
19:00	2	1326	147	2	66	1	0	2	0	0	0	0	0	1546
20:00	0	882	90	1	59	0	0	0	1	0	0	0	0	1033
21:00	1	793	89	0	34	0	0	0	2	0	0	0	0	919
22:00	0	444	36	0	14	0	0	0	2	0	0	0	0	496
23:00	0	273	28	0	6	0	0	0	0	0	0	0	0	307
Totals	33	20721	2654	108	1508	45	3	63	69					25204
% of Totals	0%	82%	11%	0%	6%	0%	0%	0%	0%					100%
AM Volumes	11	7722	1065	58	659	28	1	30	34	0	0	0	0	9608
% AM	0%	31%	4%	0%	3%	0%	0%	0%	0%	-				38%
AM Peak Hour	05:00	08:00	07:00	07:00	07:00	10:00	11:00	09:00	09:00					08:00
Volume	2	1593	207	15	128	9	1	7	11					1914
PM Volumes	22	12999	1589	50	849	17	2	33	35	0	0	0	0	15596
% PM	0%	52%	6%	0%	3%	0%	0%	0%	0%					62%
PM Peak Hour	14:00	17:00	18:00	15:00	14:00	12:00	15:00	14:00	14:00					17:00
Volume	5	1719	182	13	117	4	1	6	10					1986
Dir	ectional Pe	ak Periods		AM 7-9			NOON 12-2			PM 4-6		Off	Peak Volun	nes
	All Classes				%	Volume		%	Volume		%	Volume		%
				\longleftrightarrow	15%	2595	\longleftrightarrow	10%	3769	\longleftrightarrow	15%	15108	\longleftrightarrow	60%

1 Motorcycles

- 2 Passenger Cars **3** 2-Axle, 4-Tire Single Units
- 4 Buses
 - 5 2-Axle, 6-Tire Single Units
 - 6 3-Axle Single Units
- 7 > =4-Axle Single Units

Classification Definitions

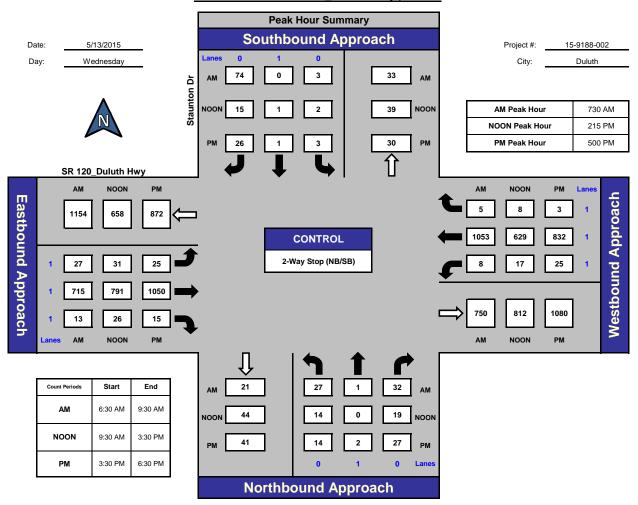
- 8 <=4-Axle Single Trailers
- **9** 5-Axle Single Trailers
- 10 >=6-Axle Single Trailers
- 11 <=5-Axle Multi-Trailers
- 12 6-Axle Multi-Trailers
- 13 >=7-Axle Multi-Trailers

ITM Peak Hour Summary

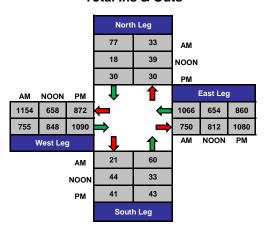


National Data & Surveying Services

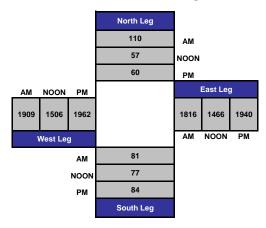
Staunton Dr and SR 120_Duluth Hwy, Duluth



Total Ins & Outs

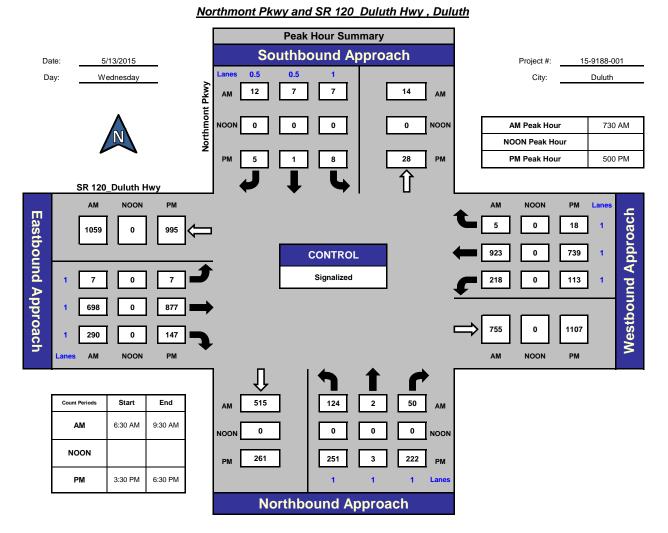


Total Volume Per Leg

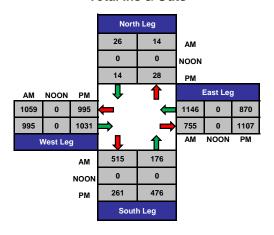


ITM Peak Hour Summary

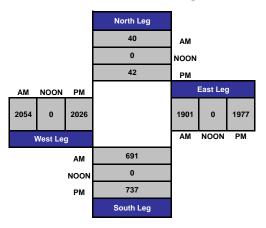








Total Volume Per Leg



Appendix C: K&D Worksheet

Peak Hour Factor and Directional Distribution Worksheet

AM Peak End Time PM Peak End Time 8:30 18:00 Shaded Cells are manually entered

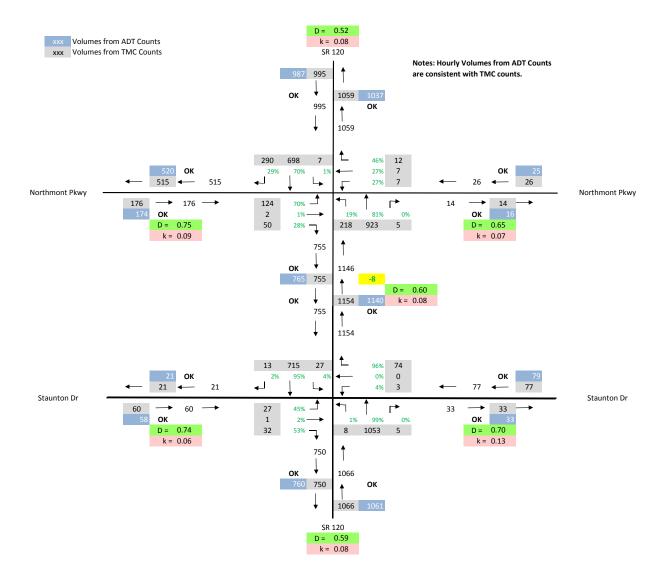
Blank Cells are calculated

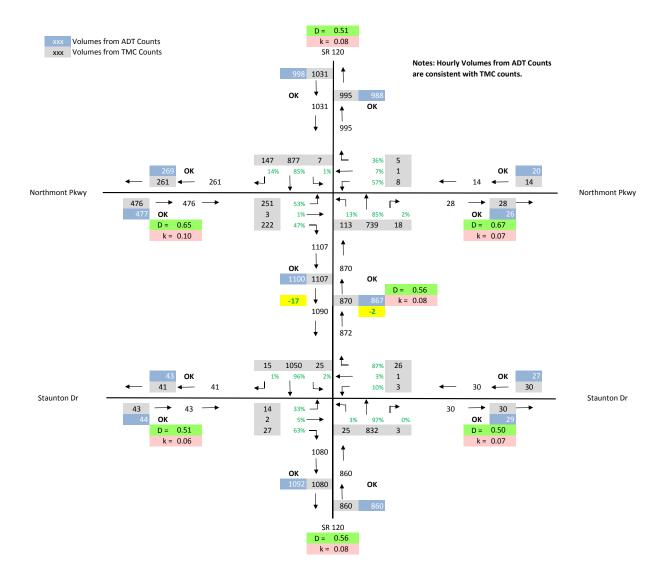
			Distribution works		v Counts and Inf	formation		18.00					Calculat	ions	
						А	M	F	PM	AM	PM	AM	PM	AM	PM
Count #	Year	Daily Traffic	Location Description	Type of Count*	Mainline or Sidestreet	East/North Bound	West/South Bound	East/North Bound	West/South Bound	Total Hou	rly Traffic	ΚV	alue	D Fa	ctor†
1	2015	25,204	SR 120 west of Northmont Pkwy	Class	М	987	1,037	998	988	2024	1986	0.08	0.08	0.51 ←	0.5 →
2	2015	532	Northmont Pkwy north of SR 120	Volume	S	14	25	28	14	39	42	0.07	0.08	0.64 ↓	0.67 ↑
3	2015	7,744	Northmont Pkwy south of SR 120	Volume	S	174	520	477	269	694	746	0.09	0.10	0.75↓	0.64 ↑
4	2015	24,481	SR 120 between Northmont Pkwy and Staunton Dr.	Volume	M	765	1,140	1,100	867	1905	1967	0.08	0.08	0.6 ←	0.56 →
5	2015	845	Staunton Dr. north of SR 120	Volume	S	33	79	29	27	112	56	0.13	0.07	0.71↓	0.52 ↑
6	2015	1,302	Staunton Dr. south of SR 120	Volume	S	58	21	44	43	79	87	0.06	0.07	0.73 ↑	0.51 ↑
7	2015	24,111	SR 120 east of Staunton Drive	Volume	М	760	1,061	1,092	860	1821	1952	0.08	0.08	0.58 ←	0.56 →
135-0161	2014	19,500	SR 120 Between Buford Hwy and Knox Branch Creek	AADT	M	not available	not available	not available	not available	1676	1494	0.09	0.08	not available	not available
135-0163	2015	23,320	SR 120 Between Knox Branch Creek and Satellite Blvd.	AADT	M	not available	not available	not available	not available	1646	1690	0.07	0.07	not available	not available
135-0527	2015	24,320	Boggs Rd Between SR 120 and Satellite Blvd.	AADT	S	not available	not available	not available	not available	1038	860	0.04	0.04	not available	not available

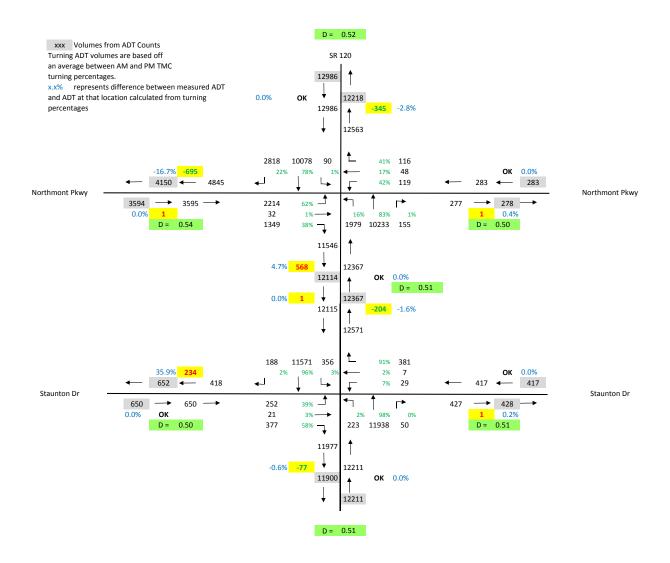
^{*} AADT counts from GDOT Count Stations, Volume and Class counts by tubes
† D values are measured by the largest direction movement and are thus never less than 0.50
NOTE: Where GDOT Count Stations are used, the Daily Traffic and Peak Hour volumes reported are those of the raw count, not the AADT.

Weighted Average0.070.07Mainline Weighted Average0.080.08Sidestreet Weighted Average0.060.05

Appendix D: Design Traffic Worksheets

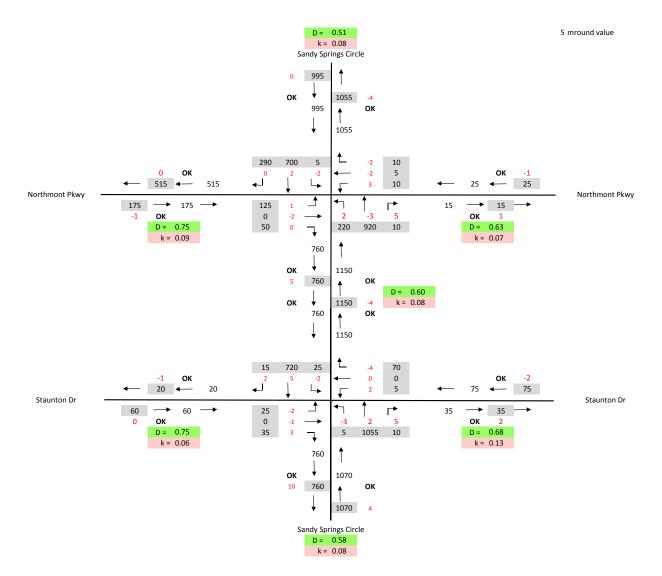


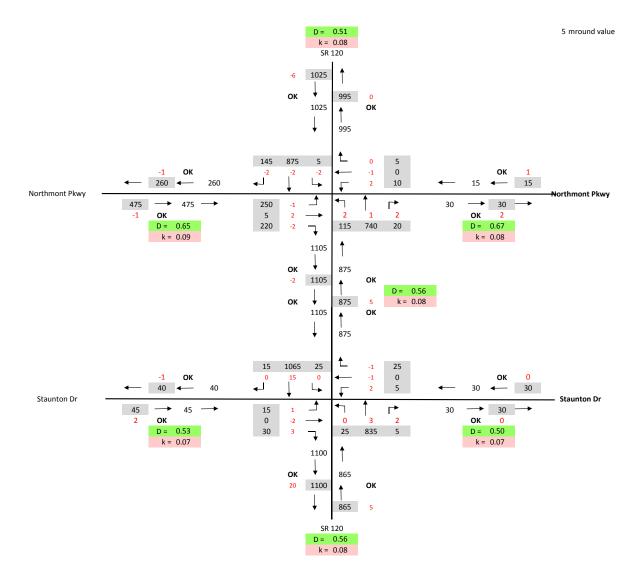


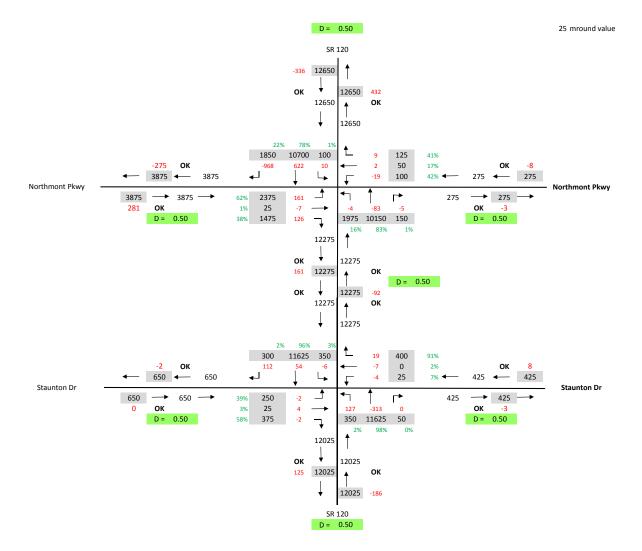


SR 120 at Singleton Creek Traffic Volumes.xlsx

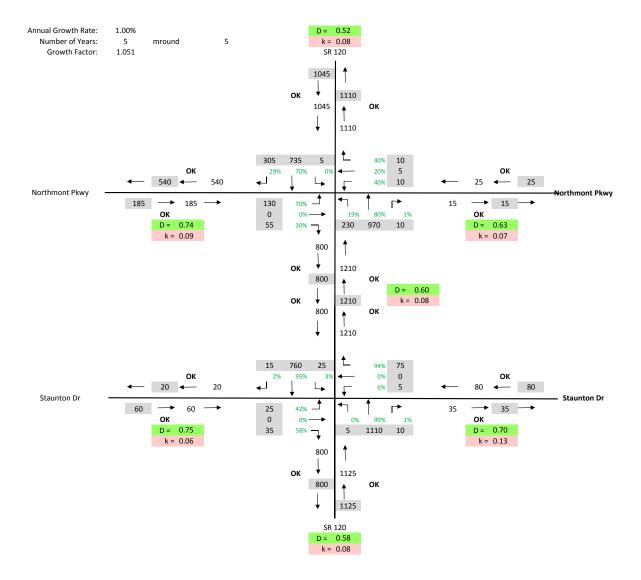
ADT_RAW

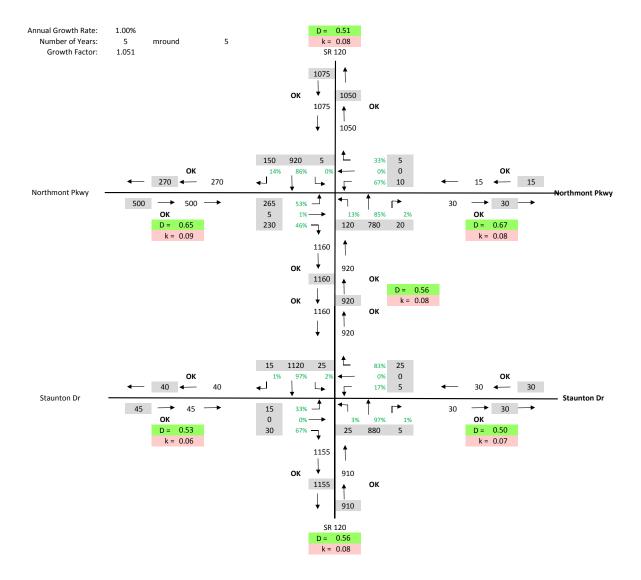


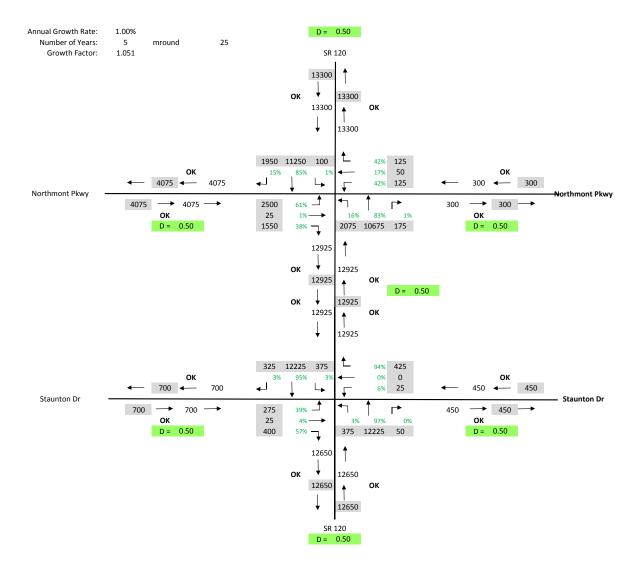


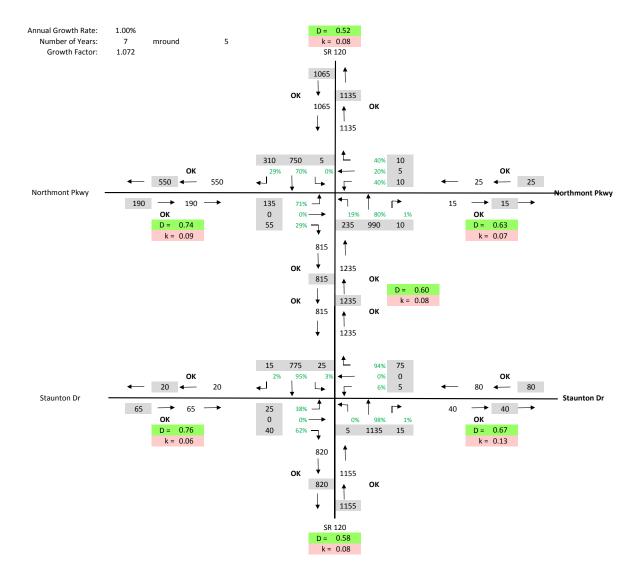


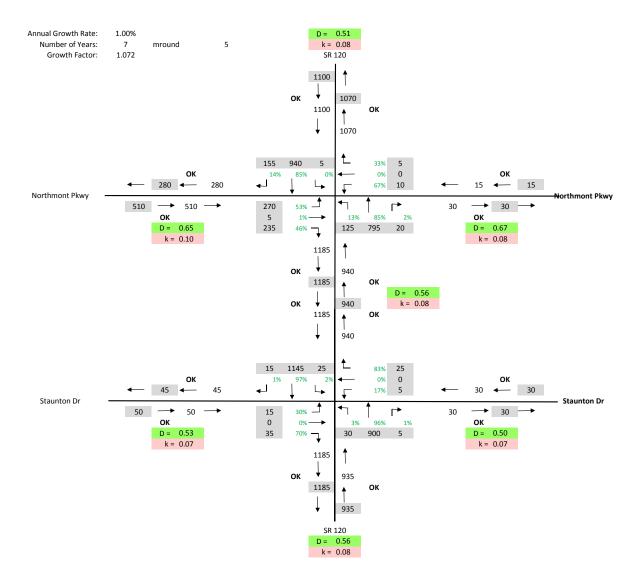
SR 120 at Singleton Creek Traffic Volumes.xlsx ADT_2015

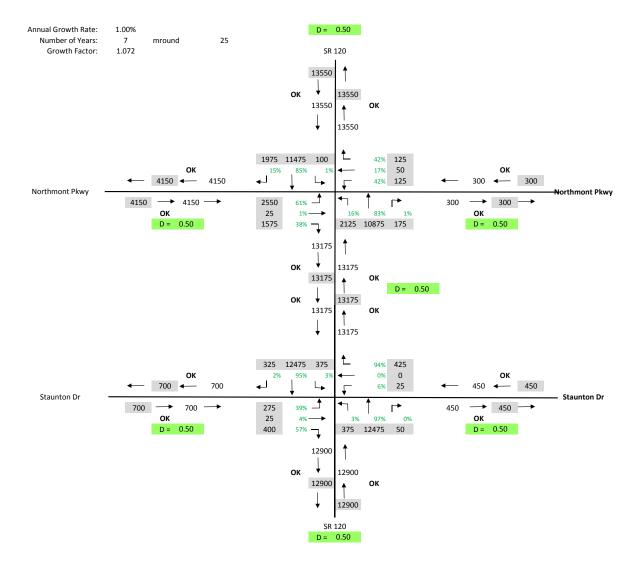


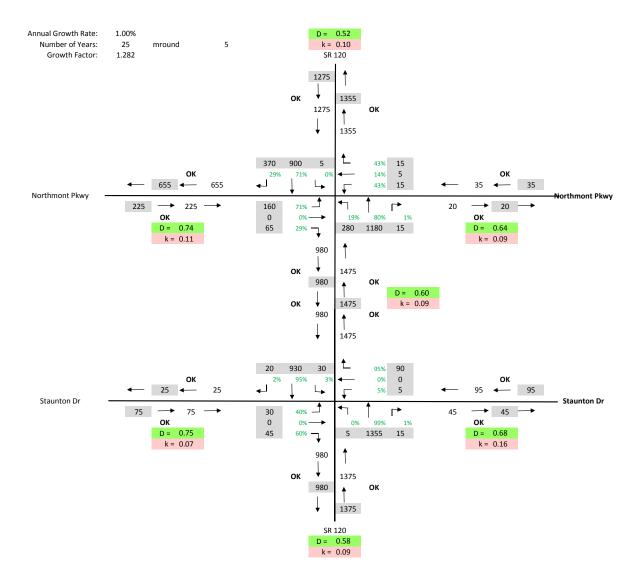


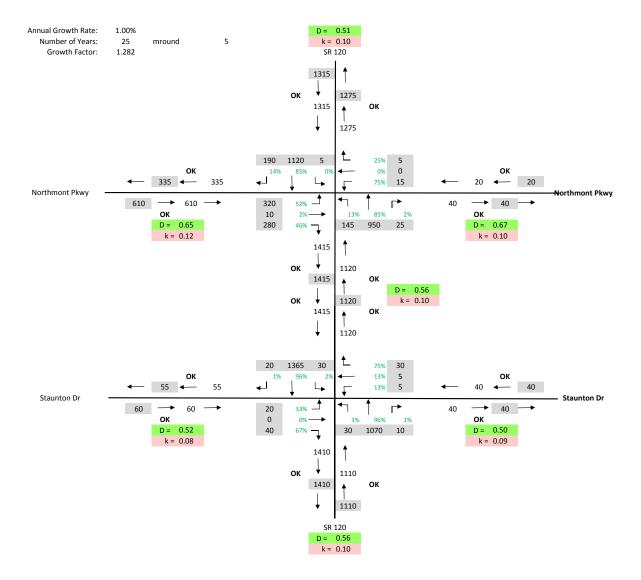


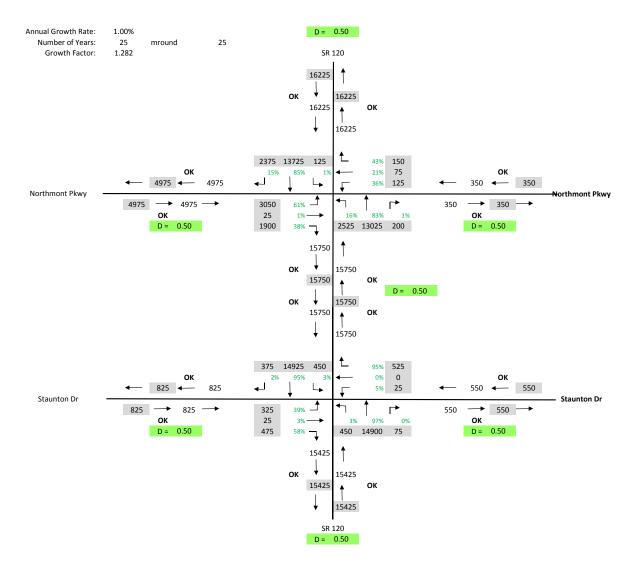




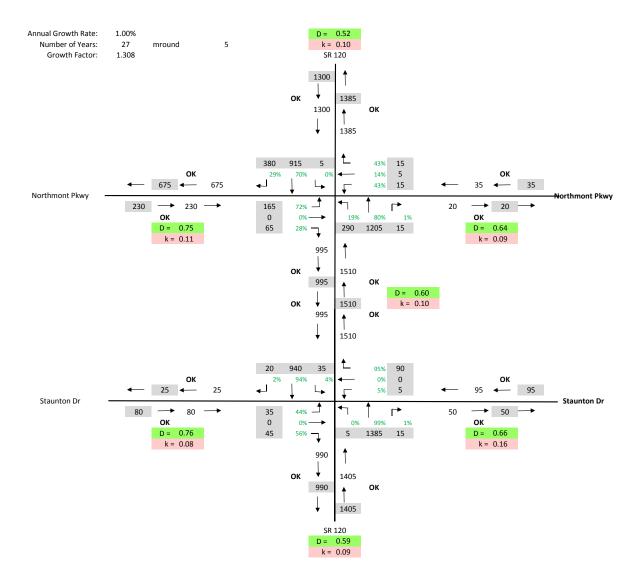


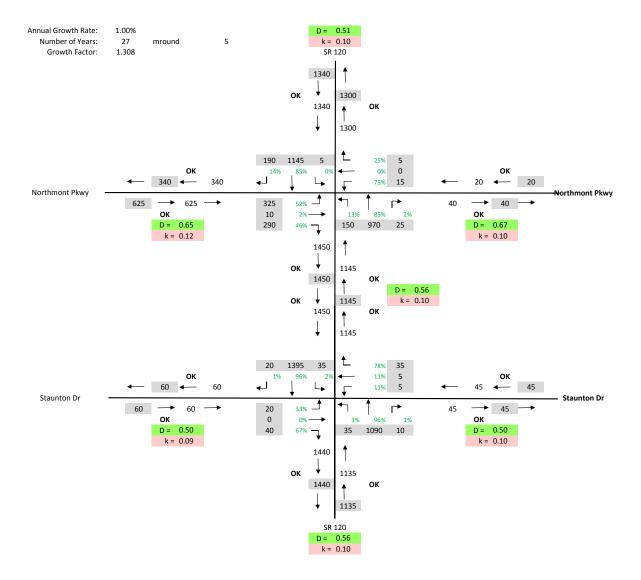


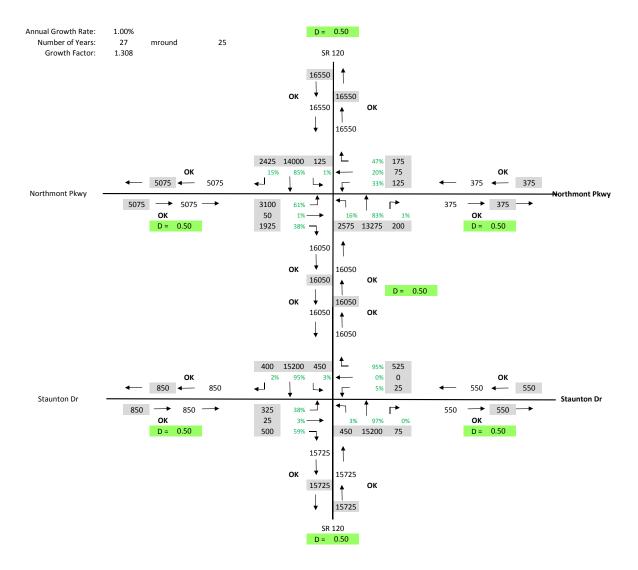




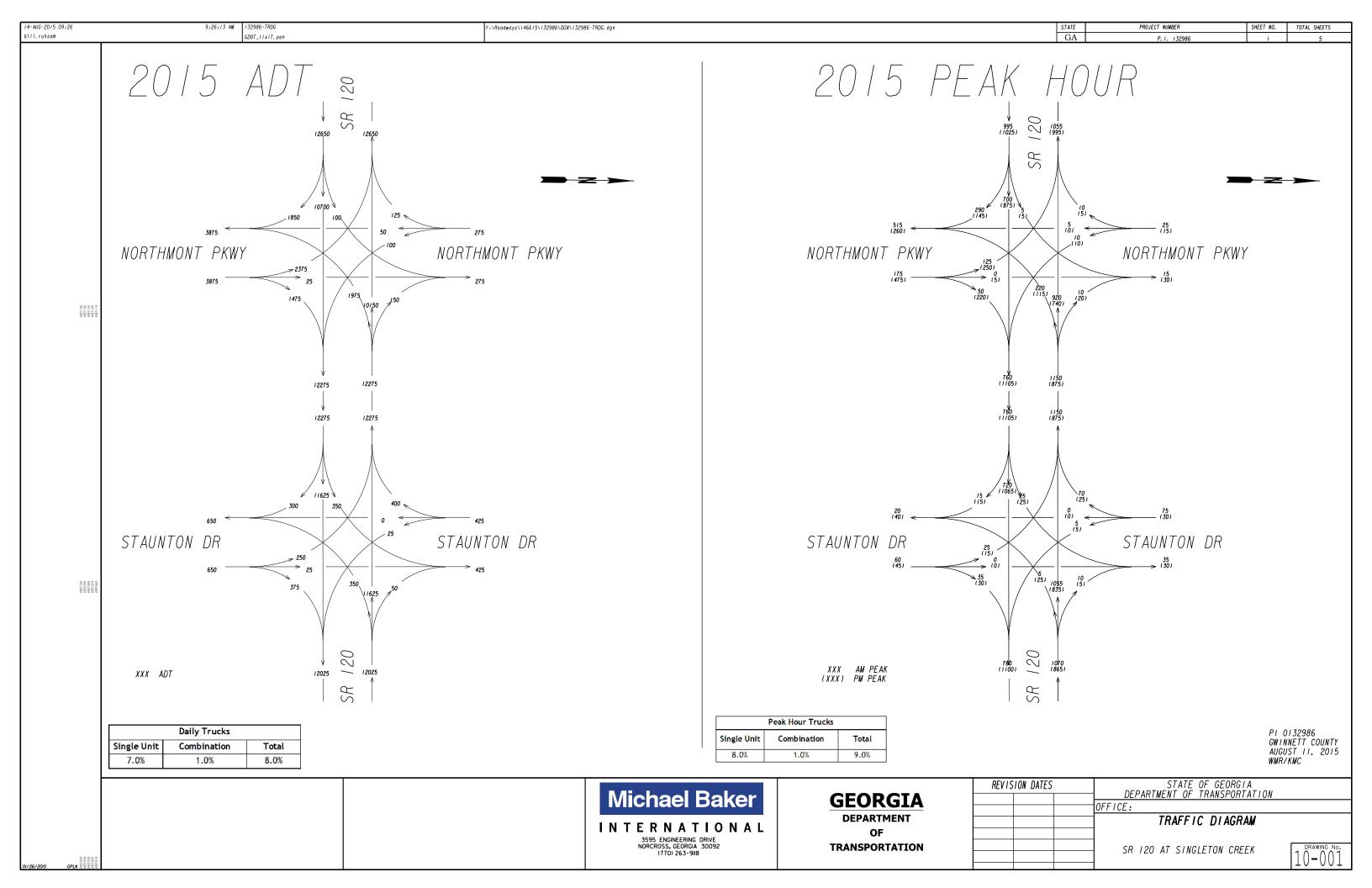
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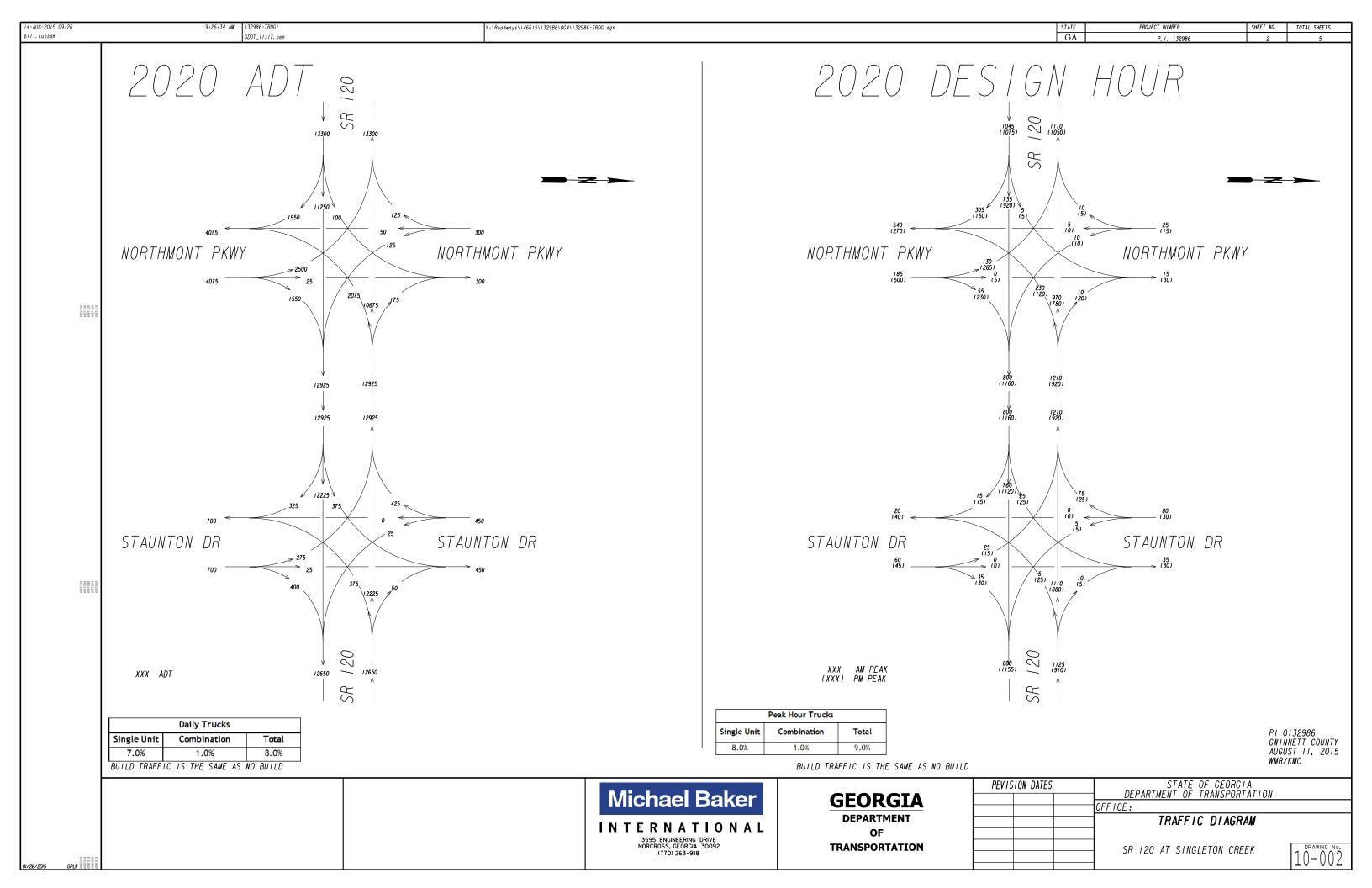


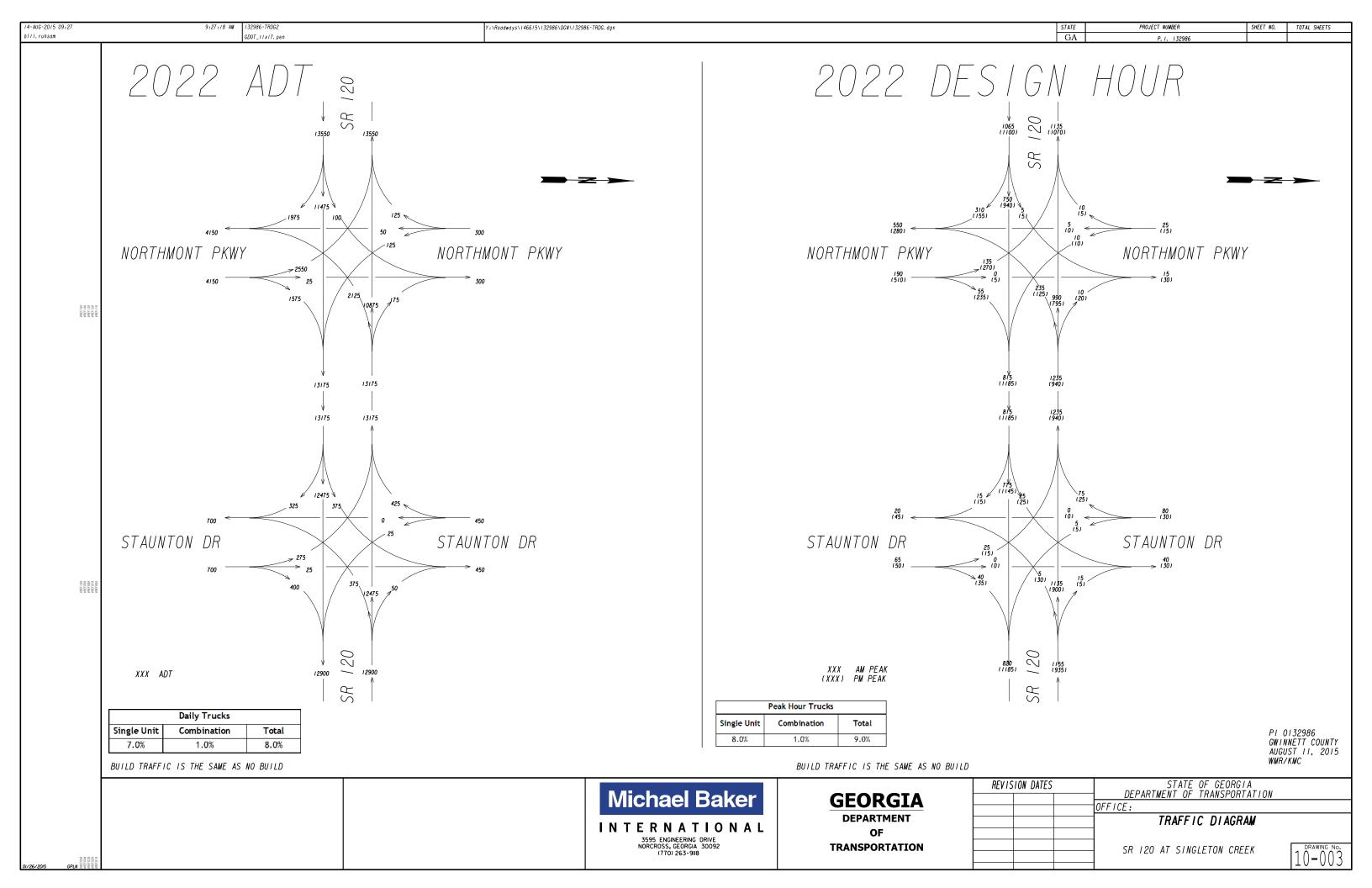


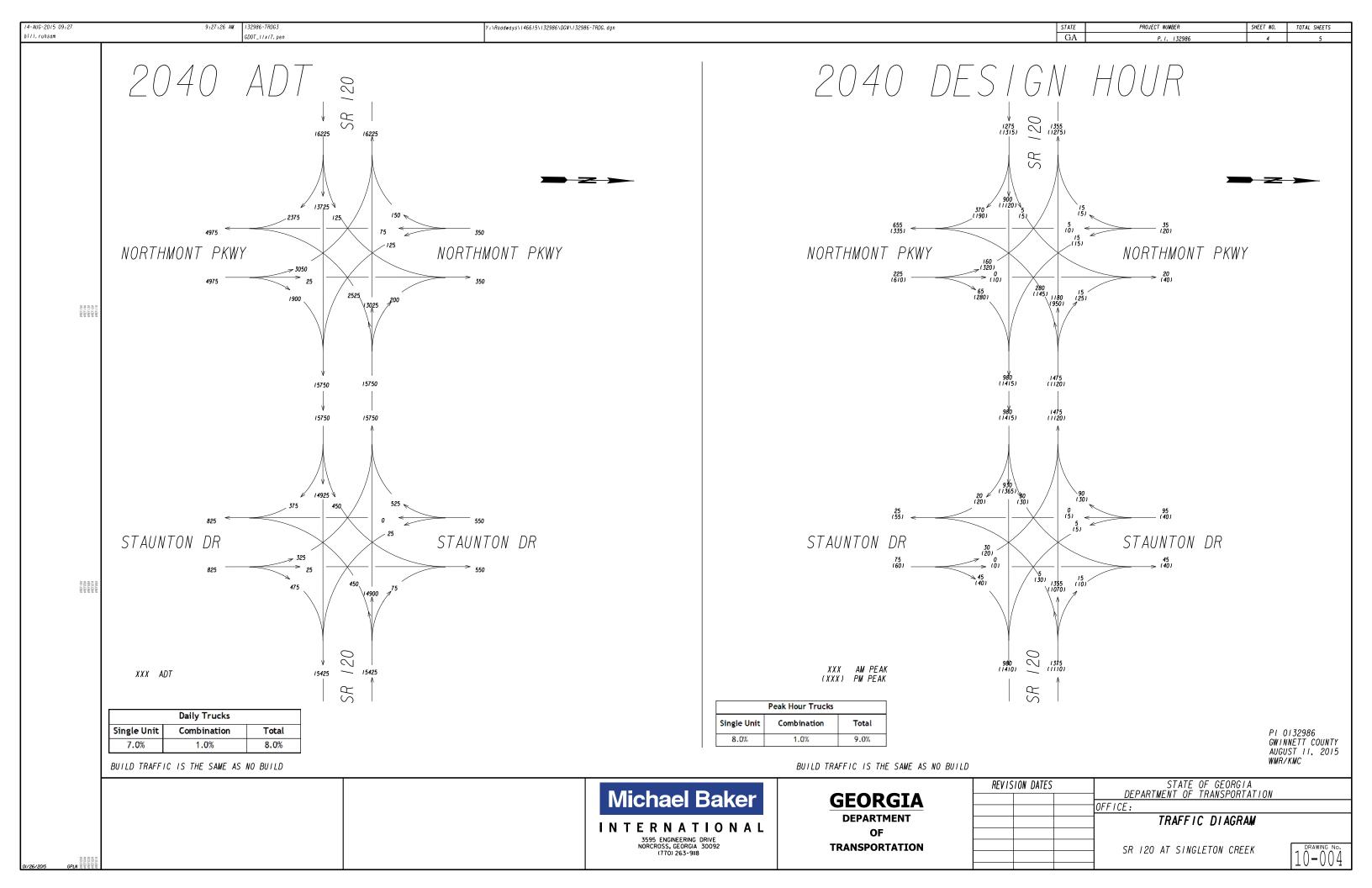


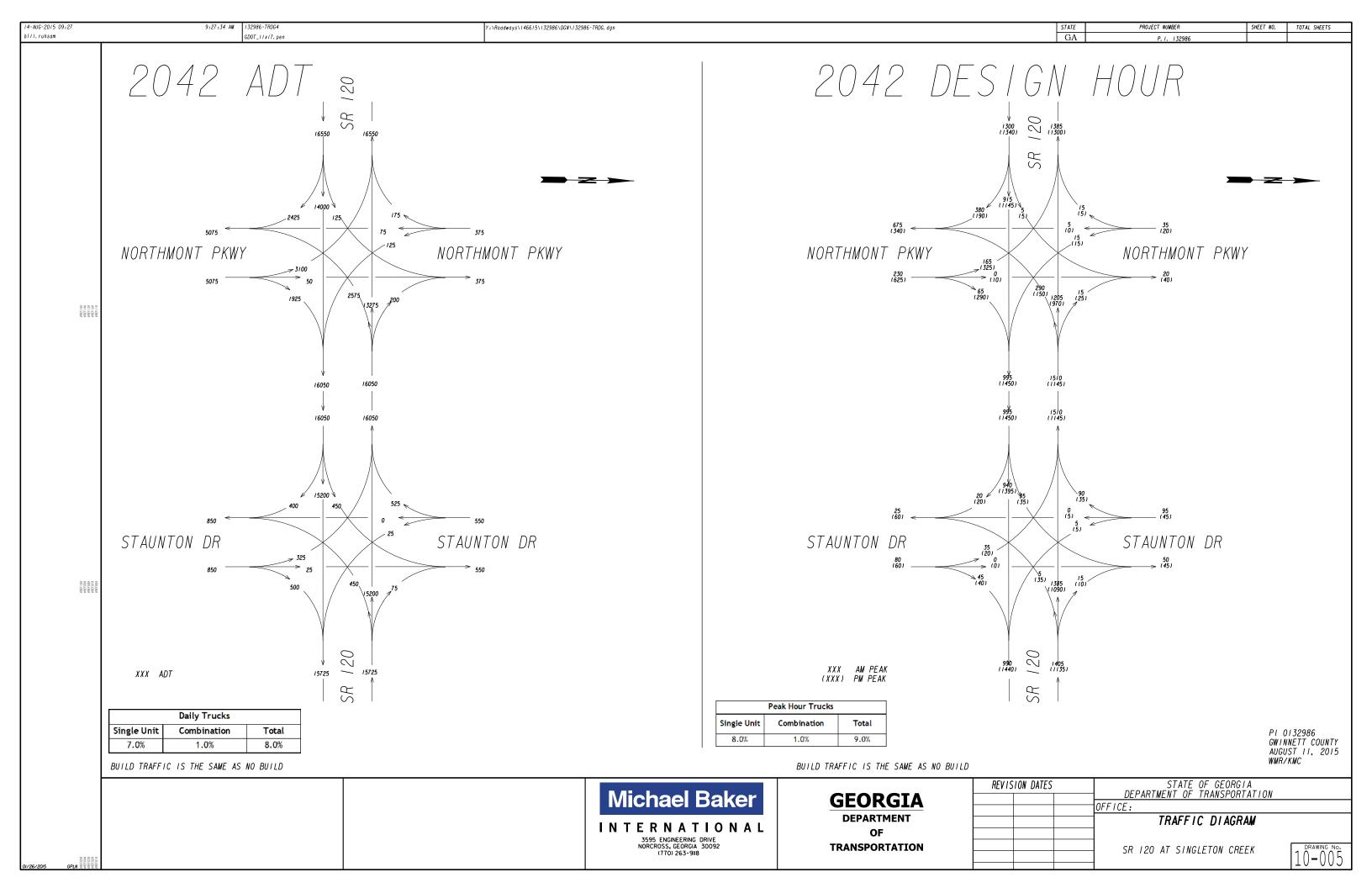
Appendix E: Design Traffic

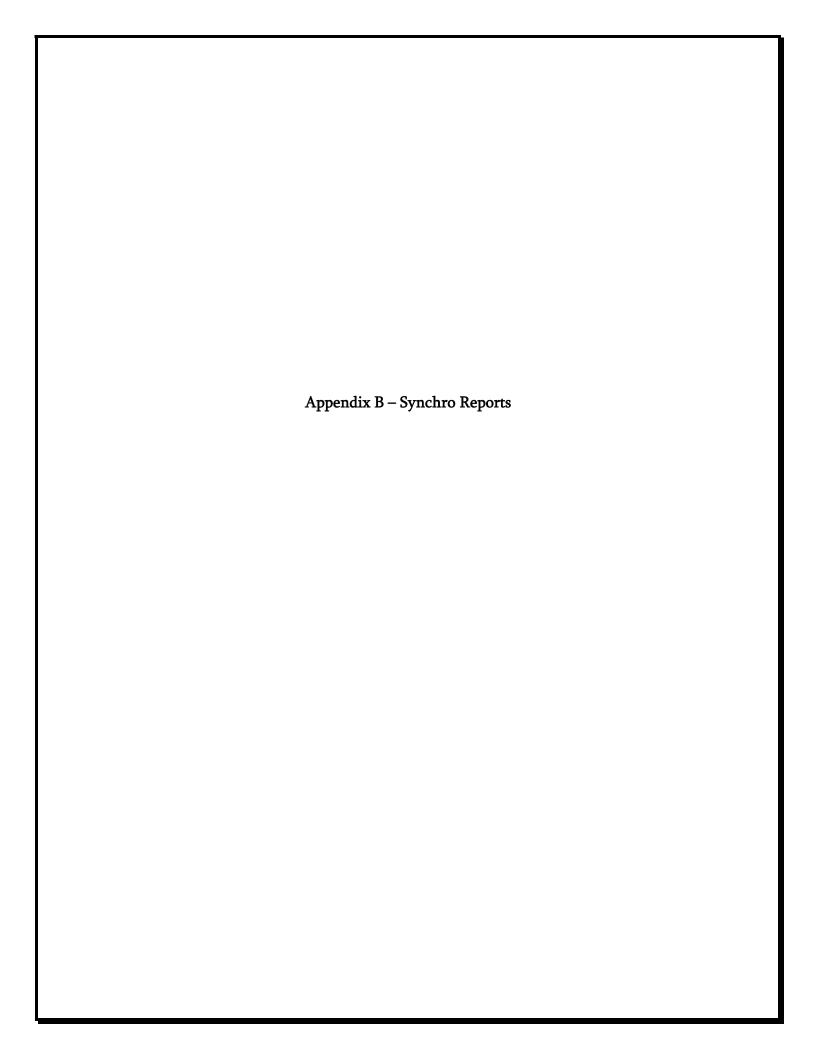












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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ň	ĵ»	
Volume (vph)	5	700	290	220	920	10	125	0	50	10	5	10
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00		0.85	1.00	0.90	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95		1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689		1511	1770	1671	
Flt Permitted	0.24	1.00	1.00	0.17	1.00	1.00	0.75		1.00	0.76	1.00	
Satd. Flow (perm)	412	1719	1461	283	1660	1411	1328		1511	1410	1671	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	761	315	239	1000	11	136	0	54	11	5	11
RTOR Reduction (vph)	0	0	120	0	0	3	0	0	46	0	9	0
Lane Group Flow (vph)	5	761	195	239	1000	8	136	0	8	11	7	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm		Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	47.6	47.6	47.6	63.2	63.2	63.2	12.7		12.7	12.7	12.7	
Effective Green, g (s)	47.6	47.6	47.6	63.2	63.2	63.2	12.7		12.7	12.7	12.7	
Actuated g/C Ratio	0.54	0.54	0.54	0.71	0.71	0.71	0.14		0.14	0.14	0.14	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2		0.2	0.2	0.2	
Lane Grp Cap (vph)	221	924	785	352	1185	1007	190		216	202	239	
v/s Ratio Prot		0.44		0.08	c0.60						0.00	
v/s Ratio Perm	0.01		0.13	0.40		0.01	c0.10		0.01	0.01		
v/c Ratio	0.02	0.82	0.25	0.68	0.84	0.01	0.72		0.04	0.05	0.03	
Uniform Delay, d1	9.6	17.0	10.9	11.9	9.1	3.6	36.2		32.6	32.7	32.6	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	0.0	6.0	0.2	4.1	5.7	0.0	10.2		0.0	0.0	0.0	
Delay (s)	9.6	23.0	11.1	16.0	14.8	3.6	46.3		32.7	32.8	32.6	
Level of Service	А	C	В	В	В	А	D	40.5	С	С	C	
Approach Delay (s)		19.5			14.9			42.5			32.7	
Approach LOS		В			В			D			С	
Intersection Summary												
HCM 2000 Control Delay			19.1	Н	CM 2000	Level of	Service		В			
HCM 2000 Volume to Capa	acity ratio		0.88									
Actuated Cycle Length (s)			88.5	Sum of lost time (s) 17.9								
Intersection Capacity Utiliza	ation		92.8%	IC	CU Level	of Service	! 		F			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ		7	ሻ		7		4			4	
Volume (veh/h)	25	720	15	5	1055	10	25	0	35	5	0	70
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	783	16	5	1147	11	27	0	38	5	0	76
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.62			0.62	0.62	0.62	0.62	0.62	
vC, conflicting volume	1158			799			2071	2005	783	2033	2011	1147
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1158			369			2421	2315	343	2359	2324	1147
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	95			99			0	100	91	59	100	69
cM capacity (veh/h)	579			714			9	22	434	13	22	242
Direction, Lane #	EB 1	EB 2	EB3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	783	16	5	1147	11	65	82				
Volume Left	27	0	0	5	0	0	27	5				
Volume Right	0	0	16	0	0	11	38	76				
cSH	579	1700	1700	714	1700	1700	21	113				
Volume to Capacity	0.05	0.46	0.01	0.01	0.67	0.01	3.08	0.72				
Queue Length 95th (ft)	4	0	0	1	0	0	Err	97				
Control Delay (s)	11.5	0.0	0.0	10.1	0.0	0.0	Err	93.4				
Lane LOS	В			В			F	F				
Approach Delay (s)	0.4			0.0			Err	93.4				
Approach LOS							F	F				
Intersection Summary												
Average Delay			309.0									
Intersection Capacity Utilizat	tion		72.4%	IC	CU Level	of Service			С			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ሻ	₽	
Volume (vph)	5	875	145	115	740	20	250	5	220	10	0	5
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.85	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689	1778	1511	1770	1583	
Flt Permitted	0.32	1.00	1.00	0.07	1.00	1.00	0.75	1.00	1.00	0.75	1.00	
Satd. Flow (perm)	545	1719	1461	119	1660	1411	1341	1778	1511	1405	1583	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	951	158	125	804	22	272	5	239	11	0	5
RTOR Reduction (vph)	0	0	45	0	0	7	0	0	191	0	4	0
Lane Group Flow (vph)	5	951	113	125	804	15	272	5	48	11	1	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	69.1	69.1	69.1	84.2	84.2	84.2	24.5	24.5	24.5	24.5	24.5	
Effective Green, g (s)	69.1	69.1	69.1	84.2	84.2	84.2	24.5	24.5	24.5	24.5	24.5	
Actuated g/C Ratio	0.57	0.57	0.57	0.69	0.69	0.69	0.20	0.20	0.20	0.20	0.20	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2	0.2	0.2	0.2	0.2	
Lane Grp Cap (vph)	310	979	832	200	1152	979	270	359	305	283	319	
v/s Ratio Prot		c0.55		0.05	c0.48			0.00			0.00	
v/s Ratio Perm	0.01		0.08	0.38		0.01	c0.20		0.03	0.01		
v/c Ratio	0.02	0.97	0.14	0.62	0.70	0.02	1.01	0.01	0.16	0.04	0.00	
Uniform Delay, d1	11.3	25.1	12.2	25.2	11.0	5.7	48.4	38.7	39.9	38.9	38.6	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Incremental Delay, d2	0.0	22.0	0.1	4.3	1.9	0.0	56.7	0.0	0.1	0.0	0.0	
Delay (s)	11.4	47.1	12.3	29.5	12.9	5.7	105.1	38.7	40.0	39.0	38.7	
Level of Service	В	D	В	С	В	Α	F	D	D	D	D	
Approach Delay (s)		42.0			14.9			74.3			38.9	
Approach LOS		D			В			E			D	
Intersection Summary												
HCM 2000 Control Delay			38.5	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capac	city ratio		0.97									
Actuated Cycle Length (s)			121.3	Sum of lost time (s) 17.9								
Intersection Capacity Utilization			90.2%	IC	CU Level	of Service)		Е			
Analysis Period (min)			15									
c Critical Lane Group												

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	↑	7	7	↑	7		4			4	
Volume (veh/h)	25	1065	15	25	835	5	15	0	30	5	0	25
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	1158	16	27	908	5	16	0	33	5	0	27
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.46			0.46	0.46	0.46	0.46	0.46	
vC, conflicting volume	913			1174			2201	2179	1158	2207	2190	908
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	913			792			3023	2975	756	3034	2999	908
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	96			93			0	100	83	0	100	92
cM capacity (veh/h)	718			368			3	6	188	3	6	334
Direction, Lane #	EB 1	EB 2	EB3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	1158	16	27	908	5	49	33				
Volume Left	27	0	0	27	0	0	16	5				
Volume Right	0	0	16	0	0	5	33	27				
cSH	718	1700	1700	368	1700	1700	9	16				
Volume to Capacity	0.04	0.68	0.01	0.07	0.53	0.00	5.38	2.05				
Queue Length 95th (ft)	3	0	0	6	0	0	Err	117				
Control Delay (s)	10.2	0.0	0.0	15.6	0.0	0.0	Err	981.2				
Lane LOS	В			С			F	F				
Approach Delay (s)	0.2			0.4			Err	981.2				
Approach LOS							F	F				
Intersection Summary												
Average Delay			234.7									
Intersection Capacity Utilization	on		67.6%	IC	CU Level	of Service			С			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ሻ	1>	•
Volume (vph)	5	735	305	230	970	10	130	0	55	10	5	10
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00		0.85	1.00	0.90	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95		1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689		1511	1770	1671	
Flt Permitted	0.21	1.00	1.00	0.17	1.00	1.00	0.75		1.00	0.76	1.00	
Satd. Flow (perm)	357	1719	1461	282	1660	1411	1328		1511	1410	1671	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	799	332	250	1054	11	141	0	60	11	5	11
RTOR Reduction (vph)	0	0	112	0	0	3	0	0	51	0	9	0
Lane Group Flow (vph)	5	799	220	250	1054	8	141	0	9	11	7	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm		Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	57.3	57.3	57.3	73.4	73.4	73.4	14.4		14.4	14.4	14.4	
Effective Green, g (s)	57.3	57.3	57.3	73.4	73.4	73.4	14.4		14.4	14.4	14.4	
Actuated g/C Ratio	0.57	0.57	0.57	0.73	0.73	0.73	0.14		0.14	0.14	0.14	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2		0.2	0.2	0.2	
Lane Grp Cap (vph)	203	981	833	345	1213	1031	190		216	202	239	
v/s Ratio Prot		0.46		0.08	c0.64						0.00	
v/s Ratio Perm	0.01		0.15	0.45		0.01	c0.11		0.01	0.01		
v/c Ratio	0.02	0.81	0.26	0.72	0.87	0.01	0.74		0.04	0.05	0.03	
Uniform Delay, d1	9.4	17.3	10.9	13.8	10.0	3.7	41.2		37.0	37.1	37.0	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	0.0	5.3	0.2	6.3	6.8	0.0	12.8		0.0	0.0	0.0	
Delay (s)	9.4	22.6	11.1	20.1	16.8	3.7	54.0		37.1	37.2	37.0	
Level of Service	А	С	В	С	В	А	D		D	D	D	
Approach Delay (s)		19.1			17.3			48.9			37.1	
Approach LOS		В			В			D			D	
Intersection Summary	Intersection Summary											
HCM 2000 Control Delay					CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.90									
Actuated Cycle Length (s)					um of lost				17.9			
Intersection Capacity Utiliza	ation		95.7%	IC	CU Level	of Service	!		F			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	↑	7	7	↑	7		4			4	
Volume (veh/h)	25	760	15	5	1110	10	25	0	35	5	0	75
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	826	16	5	1207	11	27	0	38	5	0	82
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.61			0.61	0.61	0.61	0.61	0.61	
vC, conflicting volume	1217			842			2179	2109	826	2136	2114	1207
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1217			422			2613	2497	396	2542	2506	1207
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	95			99			0	100	90	43	100	64
cM capacity (veh/h)	549			671			6	17	399	10	16	224
Direction, Lane #	EB 1	EB 2	EB3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	826	16	5	1207	11	65	87				
Volume Left	27	0	0	5	0	0	27	5				
Volume Right	0	0	16	0	0	11	38	82				
cSH	549	1700	1700	671	1700	1700	14	93				
Volume to Capacity	0.05	0.49	0.01	0.01	0.71	0.01	4.64	0.93				
Queue Length 95th (ft)	4	0	0	1	0	0	Err	133				
Control Delay (s)	11.9	0.0	0.0	10.4	0.0	0.0	Err	156.0				
Lane LOS	В			В			F	F				
Approach Delay (s)	0.4			0.0			Err	156.0				
Approach LOS							F	F				
Intersection Summary												
Average Delay			296.7									
Intersection Capacity Utilizati	on		75.3%	IC	CU Level	of Service			D			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	*	1	7	ሻ	†	7	ሻ	†	7	ሻ	ĵ»	
Volume (vph)	5	920	150	120	780	20	265	5	230	10	0	5
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.85	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689	1778	1511	1770	1583	
Flt Permitted	0.30	1.00	1.00	0.07	1.00	1.00	0.75	1.00	1.00	0.75	1.00	
Satd. Flow (perm)	514	1719	1461	111	1660	1411	1341	1778	1511	1405	1583	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	1000	163	130	848	22	288	5	250	11	0	5
RTOR Reduction (vph)	0	0	41	0	0	6	0	0	203	0	4	0
Lane Group Flow (vph)	5	1000	122	130	848	16	288	5	47	11	1	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	77.9	77.9	77.9	93.6	93.6	93.6	24.3	24.3	24.3	24.3	24.3	
Effective Green, g (s)	77.9	77.9	77.9	93.6	93.6	93.6	24.3	24.3	24.3	24.3	24.3	
Actuated g/C Ratio	0.60	0.60	0.60	0.72	0.72	0.72	0.19	0.19	0.19	0.19	0.19	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2	0.2	0.2	0.2	0.2	
Lane Grp Cap (vph)	306	1026	872	196	1190	1012	249	331	281	261	294	
v/s Ratio Prot		c0.58		0.05	c0.51			0.00			0.00	
v/s Ratio Perm	0.01		0.08	0.42		0.01	c0.21		0.03	0.01		
v/c Ratio	0.02	0.97	0.14	0.66	0.71	0.02	1.16	0.02	0.17	0.04	0.00	
Uniform Delay, d1	10.7	25.3	11.6	31.0	10.7	5.3	53.1	43.3	44.6	43.6	43.2	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Incremental Delay, d2	0.0	22.0	0.1	6.4	2.0	0.0	106.0	0.0	0.1	0.0	0.0	
Delay (s)	10.7	47.3	11.6	37.4	12.7	5.3	159.1	43.3	44.7	43.6	43.2	
Level of Service	В	D	В	D	В	Α	F	D	D	D	D	
Approach Delay (s)		42.2			15.8			105.3			43.5	
Approach LOS		D			В			F			D	
Intersection Summary												
HCM 2000 Control Delay			45.1	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capac	city ratio		1.01									
Actuated Cycle Length (s)			130.5		um of los				17.9			
Intersection Capacity Utiliza	tion		93.2%	IC	CU Level	of Service)		F			
Analysis Period (min)			15									
c Critical Lane Group												

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	†	7	7	↑	7		4			4	
Volume (veh/h)	25	1120	15	25	880	5	15	0	30	5	0	25
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	1217	16	27	957	5	16	0	33	5	0	27
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.43			0.43	0.43	0.43	0.43	0.43	
vC, conflicting volume	962			1234			2310	2288	1217	2315	2299	957
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	962			882			3381	3330	844	3393	3355	957
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	96			91			0	100	79	0	100	91
cM capacity (veh/h)	688			318			2	3	156	1	3	313
Direction, Lane #	EB 1	EB 2	EB 3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	1217	16	27	957	5	49	33				
Volume Left	27	0	0	27	0	0	16	5				
Volume Right	0	0	16	0	0	5	33	27				
cSH	688	1700	1700	318	1700	1700	5	8				
Volume to Capacity	0.04	0.72	0.01	0.09	0.56	0.00	10.65	4.19				
Queue Length 95th (ft)	3	0	0	7	0	0	Err	Err				
Control Delay (s)	10.4	0.0	0.0	17.4	0.0	0.0	Err	Err				
Lane LOS	В			С			F	F				
Approach Delay (s)	0.2			0.5			Err	Err				
Approach LOS							F	F				
Intersection Summary												
Average Delay			349.9									
Intersection Capacity Utilization	on		70.5%	IC	CU Level	of Service			С			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	^	7	ሻ	†	7	ሻ	†	7	ሻ	1>	•
Volume (vph)	5	900	370	280	1180	15	160	0	65	15	5	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00		0.85	1.00	0.89	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95		1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689		1511	1770	1650	
Flt Permitted	0.09	1.00	1.00	0.11	1.00	1.00	0.74		1.00	0.76	1.00	
Satd. Flow (perm)	156	1719	1461	188	1660	1411	1322		1511	1410	1650	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	978	402	304	1283	16	174	0	71	16	5	16
RTOR Reduction (vph)	0	0	94	0	0	4	0	0	61	0	14	0
Lane Group Flow (vph)	5	978	308	304	1283	12	174	0	10	16	7	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm		Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	93.8	93.8	93.8	113.8	113.8	113.8	20.9		20.9	20.9	20.9	
Effective Green, g (s)	93.8	93.8	93.8	113.8	113.8	113.8	20.9		20.9	20.9	20.9	
Actuated g/C Ratio	0.64	0.64	0.64	0.77	0.77	0.77	0.14		0.14	0.14	0.14	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3		6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2		0.2	0.2	0.2	
Lane Grp Cap (vph)	99	1094	930	283	1282	1090	187		214	200	234	
v/s Ratio Prot		0.57		0.11	c0.77						0.00	
v/s Ratio Perm	0.03		0.21	c0.72		0.01	c0.13		0.01	0.01		
v/c Ratio	0.05	0.89	0.33	1.07	1.00	0.01	0.93		0.05	0.08	0.03	
Uniform Delay, d1	10.0	22.6	12.3	39.9	16.8	3.8	62.5		54.6	54.9	54.5	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	0.2	9.5	0.2	74.6	25.3	0.0	45.7		0.0	0.1	0.0	
Delay (s)	10.3	32.1	12.5	114.5	42.1	3.8	108.2		54.6	54.9	54.5	
Level of Service	В	C	В	F	D	Α	F	00.7	D	D	D	
Approach Delay (s)		26.3			55.4			92.7			54.7	
Approach LOS		С			E			F			D	
Intersection Summary												
HCM 2000 Control Delay			45.9	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capa	icity ratio		1.08									
Actuated Cycle Length (s)			147.3		um of los				17.9			
Intersection Capacity Utiliza	ation		108.4%	IC	CU Level	of Service	:		G			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7		4			4	
Volume (veh/h)	30	930	20	5	1365	15	30	0	45	5	0	90
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	33	1011	22	5	1484	16	33	0	49	5	0	98
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.48			0.48	0.48	0.48	0.48	0.48	
vC, conflicting volume	1500			1033			2668	2587	1011	2620	2592	1484
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1500			517			3959	3787	471	3856	3799	1484
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	92			99			0	100	83	0	100	36
cM capacity (veh/h)	427			482			0	2	282	1	2	153
Direction, Lane #	EB 1	EB 2	EB3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	33	1011	22	5	1484	16	82	103				
Volume Left	33	0	0	5	0	0	33	5				
Volume Right	0	0	22	0	0	16	49	98				
cSH	427	1700	1700	482	1700	1700	1	12				
Volume to Capacity	0.08	0.59	0.01	0.01	0.87	0.01	126.34	8.34				
Queue Length 95th (ft)	6	0	0	1	0	0	Err	Err				
Control Delay (s)	14.1	0.0	0.0	12.6	0.0	0.0	Err	Err				
Lane LOS	В			В			F	F				
Approach Delay (s)	0.4			0.0			Err	Err				
Approach LOS							F	F				
Intersection Summary												
Average Delay			670.7									
Intersection Capacity Utilization	n		89.6%	IC	CU Level	of Service	е		E			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ሻ	1>	•
Volume (vph)	5	1120	190	145	950	25	320	10	280	15	0	5
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.85	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689	1778	1511	1770	1583	
Flt Permitted	0.22	1.00	1.00	0.04	1.00	1.00	0.75	1.00	1.00	0.75	1.00	
Satd. Flow (perm)	373	1719	1461	67	1660	1411	1341	1778	1511	1398	1583	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	1217	207	158	1033	27	348	11	304	16	0	5
RTOR Reduction (vph)	0	0	40	0	0	6	0	0	183	0	4	0
Lane Group Flow (vph)	5	1217	167	158	1033	21	348	11	121	16	1	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	Perm	NA	Perm	Perm	NA	
Protected Phases		6		5	2			8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	93.8	93.8	93.8	112.4	112.4	112.4	23.7	23.7	23.7	23.7	23.7	
Effective Green, g (s)	93.8	93.8	93.8	112.4	112.4	112.4	23.7	23.7	23.7	23.7	23.7	
Actuated g/C Ratio	0.63	0.63	0.63	0.76	0.76	0.76	0.16	0.16	0.16	0.16	0.16	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	0.2	0.2	0.2	0.2	0.2	
Lane Grp Cap (vph)	235	1084	921	185	1254	1066	213	283	240	222	252	
v/s Ratio Prot		c0.71		0.08	c0.62			0.01			0.00	
v/s Ratio Perm	0.01		0.11	0.57		0.01	c0.26		0.08	0.01		
v/c Ratio	0.02	1.12	0.18	0.85	0.82	0.02	1.63	0.04	0.50	0.07	0.00	
Uniform Delay, d1	10.3	27.4	11.4	54.1	11.7	4.5	62.5	52.9	57.1	53.1	52.6	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Incremental Delay, d2	0.0	67.6	0.1	28.9	4.5	0.0	305.5	0.0	0.6	0.1	0.0	
Delay (s)	10.3	95.1	11.5	83.0	16.3	4.5	368.0	52.9	57.7	53.2	52.6	
Level of Service	В	F	В	F	В	Α	F	D	Е	D	D	
Approach Delay (s)		82.7			24.7			220.5			53.0	
Approach LOS		F			С			F			D	
Intersection Summary												
HCM 2000 Control Delay			88.7	Н	CM 2000	Level of	Service		F			
HCM 2000 Volume to Capa	icity ratio		1.20									
Actuated Cycle Length (s)			148.7		um of los				17.9			
Intersection Capacity Utiliza	ation		106.3%	IC	CU Level	of Service	<u> </u>		G			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	↑	7	7	↑	7		4			4	
Volume (veh/h)	30	1365	20	30	1070	10	20	0	40	5	5	30
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	33	1484	22	33	1163	11	22	0	43	5	5	33
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.38			0.38	0.38	0.38	0.38	0.38	
vC, conflicting volume	1174			1505			2812	2788	1484	2821	2799	1163
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1174			1514			4950	4886	1457	4972	4914	1163
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	94			80			0	100	28	0	0	86
cM capacity (veh/h)	571			160			0	0	61	0	0	237
Direction, Lane #	EB 1	EB 2	EB 3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	33	1484	22	33	1163	11	65	43				
Volume Left	33	0	0	33	0	0	22	5				
Volume Right	0	0	22	0	0	11	43	33				
cSH	571	1700	1700	160	1700	1700	0	0				
Volume to Capacity	0.06	0.87	0.01	0.20	0.68	0.01	Err	262.15				
Queue Length 95th (ft)	5	0	0	18	0	0	Err	Err				
Control Delay (s)	11.7	0.0	0.0	33.1	0.0	0.0	Err	Err				
Lane LOS	В			D			F	F				
Approach Delay (s)	0.2			0.9			Err	Err				
Approach LOS							F	F				
Intersection Summary												
Average Delay			Err									
Intersection Capacity Utilizat	tion		86.0%	IC	CU Level	of Service			Е			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ň	ĵ»	
Volume (vph)	5	735	305	230	970	10	130	0	55	10	5	10
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0		6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00		0.85	1.00	0.90	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95		1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689		1511	1770	1671	
Flt Permitted	0.19	1.00	1.00	0.16	1.00	1.00	0.63		1.00	1.00	1.00	
Satd. Flow (perm)	333	1719	1461	267	1660	1411	1129		1511	1863	1671	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	799	332	250	1054	11	141	0	60	11	5	11
RTOR Reduction (vph)	0	0	147	0	0	3	0	0	51	0	11	0
Lane Group Flow (vph)	5	799	185	250	1054	8	141	0	9	11	5	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt		Perm	Perm	NA	
Protected Phases		6		5	2		3	8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	49.5	49.5	49.5	63.4	63.4	63.4	13.0		13.0	2.3	2.3	
Effective Green, g (s)	49.5	49.5	49.5	63.4	63.4	63.4	13.0		13.0	2.3	2.3	
Actuated g/C Ratio	0.56	0.56	0.56	0.71	0.71	0.71	0.15		0.15	0.03	0.03	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0		6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	3.0		0.2	0.2	0.2	
Lane Grp Cap (vph)	185	956	812	316	1182	1005	207		220	48	43	
v/s Ratio Prot		0.46		0.08	c0.64		c0.05				0.00	
v/s Ratio Perm	0.02		0.13	0.49		0.01	c0.05		0.01	0.01		
v/c Ratio	0.03	0.84	0.23	0.79	0.89	0.01	0.68		0.04	0.23	0.12	
Uniform Delay, d1	8.9	16.4	10.0	13.3	10.1	3.7	35.5		32.6	42.5	42.4	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	0.1	6.4	0.1	11.9	8.8	0.0	8.9		0.0	0.9	0.5	
Delay (s)	9.0	22.8	10.2	25.2	18.9	3.7	44.4		32.7	43.4	42.8	
Level of Service	А	C	В	С	B	А	D	40.0	С	D	D	
Approach Delay (s)		19.0			19.9			40.9			43.1	
Approach LOS		В			В			D			D	
Intersection Summary												
HCM 2000 Control Delay			21.4	Н	CM 2000	Level of	Service		С			
HCM 2000 Volume to Capa	acity ratio		0.97	_					0.1.0			
Actuated Cycle Length (s)			89.0		um of lost				21.9			
Intersection Capacity Utiliza	ation		95.7%	IC	CU Level	of Service	;		F			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	†	7	7	†	7		4			4	
Volume (veh/h)	25	760	15	5	1110	10	25	0	35	5	0	75
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	826	16	5	1207	11	27	0	38	5	0	82
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.60			0.60	0.60	0.60	0.60	0.60	
vC, conflicting volume	1217			842			2179	2109	826	2136	2114	1207
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1217			396			2641	2522	368	2568	2531	1207
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	95			99			0	100	91	39	100	64
cM capacity (veh/h)	549			670			6	16	403	9	15	224
Direction, Lane #	EB 1	EB 2	EB 3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	826	16	5	1207	11	65	87				
Volume Left	27	020	0	5	0	0	27	5				
Volume Right	0	0	16	0	0	11	38	82				
cSH	549	1700	1700	670	1700	1700	13	90				
Volume to Capacity	0.05	0.49	0.01	0.01	0.71	0.01	4.97	0.97				
Queue Length 95th (ft)	4	0.49	0.01	1	0.71	0.01	Err	139				
Control Delay (s)	11.9	0.0	0.0	10.4	0.0	0.0	Err	170.9				
Lane LOS	В	0.0	0.0	В	0.0	0.0	F	F				
Approach Delay (s)	0.4			0.0			Err	170.9				
Approach LOS	0.4			0.0			F	F				
Intersection Summary												
Average Delay			297.3									
Intersection Capacity Utiliza	tion		75.3%	IC	CU Level	of Service			D			
Analysis Period (min)			15									
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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	, J	†	7	*	†	7	¥	†	7	¥	f)	
Volume (vph)	5	920	150	120	780	20	265	5	230	10	0	5
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0	6.3	6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.85	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689	1778	1511	1770	1583	
Flt Permitted	0.30	1.00	1.00	0.09	1.00	1.00	0.65	1.00	1.00	1.00	1.00	
Satd. Flow (perm)	512	1719	1461	151	1660	1411	1147	1778	1511	1863	1583	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	1000	163	130	848	22	288	5	250	11	0	5
RTOR Reduction (vph)	0	0	55	0	0	6	0	0	163	0	5	0
Lane Group Flow (vph)	5	1000	108	130	848	16	288	5	87	11	0	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	Perm	NA	
Protected Phases		6		5	2		3	8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	65.9	65.9	65.9	76.7	76.7	76.7	17.2	17.2	17.2	2.2	2.2	
Effective Green, g (s)	65.9	65.9	65.9	76.7	76.7	76.7	17.2	17.2	17.2	2.2	2.2	
Actuated g/C Ratio	0.62	0.62	0.62	0.72	0.72	0.72	0.16	0.16	0.16	0.02	0.02	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0	6.3	6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	3.0	0.2	0.2	0.2	0.2	
Lane Grp Cap (vph)	316	1063	904	182	1195	1016	241	287	244	38	32	
v/s Ratio Prot		c0.58		0.04	c0.51		c0.12	0.00			0.00	
v/s Ratio Perm	0.01		0.07	0.48		0.01	c0.07		0.06	0.01		
v/c Ratio	0.02	0.94	0.12	0.71	0.71	0.02	1.20	0.02	0.36	0.29	0.00	
Uniform Delay, d1	7.8	18.5	8.4	20.2	8.5	4.2	44.2	37.5	39.7	51.4	51.1	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Incremental Delay, d2	0.0	15.4	0.1	10.5	2.0	0.0	121.0	0.0	0.3	1.5	0.0	
Delay (s)	7.8	33.9	8.4	30.8	10.5	4.2	165.2	37.6	40.1	52.9	51.1	
Level of Service	А	C	А	С	В	Α	F	10/ 4	D	D	D	
Approach Delay (s)		30.2			13.0			106.4			52.3	
Approach LOS		С			В			F			D	
Intersection Summary												
HCM 2000 Control Delay					CM 2000	Level of	Service		D			
	2000 Volume to Capacity ratio 1.04											
j 0 1, 7	ted Cycle Length (s) 106.5				um of lost				21.9			
Intersection Capacity Utilizat	tion		93.2%	IC	CU Level	of Service	9		F			
			15									
HCM 2000 Control Delay HCM 2000 Volume to Capac Actuated Cycle Length (s)	j		1.04 106.5	S		t time (s)			21.9			

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	†	7	7	↑	7		4			4	
Volume (veh/h)	25	1120	15	25	880	5	15	0	30	5	0	25
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	27	1217	16	27	957	5	16	0	33	5	0	27
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.42			0.42	0.42	0.42	0.42	0.42	
vC, conflicting volume	962			1234			2310	2288	1217	2315	2299	957
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	962			869			3420	3369	830	3433	3394	957
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	96			91			0	100	79	0	100	91
cM capacity (veh/h)	688			315			1	3	156	1	3	313
Direction, Lane #	EB 1	EB 2	EB3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	27	1217	16	27	957	5	49	33				
Volume Left	27	0	0	27	0	0	16	5				
Volume Right	0	0	16	0	0	5	33	27				
cSH	688	1700	1700	315	1700	1700	4	7				
Volume to Capacity	0.04	0.72	0.01	0.09	0.56	0.00	11.63	4.58				
Queue Length 95th (ft)	3	0	0	7	0	0	Err	Err				
Control Delay (s)	10.4	0.0	0.0	17.5	0.0	0.0	Err	Err				
Lane LOS	В			С			F	F				
Approach Delay (s)	0.2			0.5			Err	Err				
Approach LOS							F	F				
Intersection Summary												
Average Delay			349.9									
Intersection Capacity Utilization	on		70.5%	IC	CU Level	of Service			С			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ሻ	1>	
Volume (vph)	5	900	370	280	1180	15	160	0	65	15	5	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0		6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00		0.85	1.00	0.89	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95		1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689		1511	1770	1650	
Flt Permitted	0.11	1.00	1.00	0.09	1.00	1.00	0.53		1.00	1.00	1.00	
Satd. Flow (perm)	193	1719	1461	154	1660	1411	948		1511	1863	1650	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	978	402	304	1283	16	174	0	71	16	5	16
RTOR Reduction (vph)	0	0	122	0	0	3	0	0	63	0	16	0
Lane Group Flow (vph)	5	978	280	304	1283	13	174	0	8	16	5	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt		Perm	Perm	NA	
Protected Phases		6		5	2		3	8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	78.4	78.4	78.4	100.6	100.6	100.6	15.1		15.1	3.5	3.5	
Effective Green, g (s)	78.4	78.4	78.4	100.6	100.6	100.6	15.1		15.1	3.5	3.5	
Actuated g/C Ratio	0.61	0.61	0.61	0.78	0.78	0.78	0.12		0.12	0.03	0.03	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0		6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	3.0		0.2	0.2	0.2	
Lane Grp Cap (vph)	117	1050	892	308	1301	1106	155		177	50	45	
v/s Ratio Prot		0.57		0.13	c0.77		c0.07				0.00	
v/s Ratio Perm	0.03		0.19	c0.64		0.01	c0.07		0.01	0.01		
v/c Ratio	0.04	0.93	0.31	0.99	0.99	0.01	1.12		0.05	0.32	0.12	
Uniform Delay, d1	10.0	22.5	12.0	39.4	13.2	3.0	56.1		50.2	61.2	60.9	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	0.2	14.2	0.2	47.2	21.5	0.0	109.0		0.0	1.3	0.4	
Delay (s)	10.1	36.7	12.2	86.6	34.7	3.0	165.1		50.3	62.6	61.3	
Level of Service	В	D	В	F	C	А	F	101.0	D	E	(1.0	
Approach Delay (s)		29.5			44.2			131.8			61.9	
Approach LOS		С			D			F			E	
Intersection Summary												
HCM 2000 Control Delay			44.7	Н	CM 2000	Level of	Service		D			
HCM 2000 Volume to Capa	acity ratio		1.08	_					0.1.0			
Actuated Cycle Length (s)			128.3		um of los				21.9			
Intersection Capacity Utiliza	ation		108.4%	IC	CU Level	of Service	9		G			
Analysis Period (min)			15									

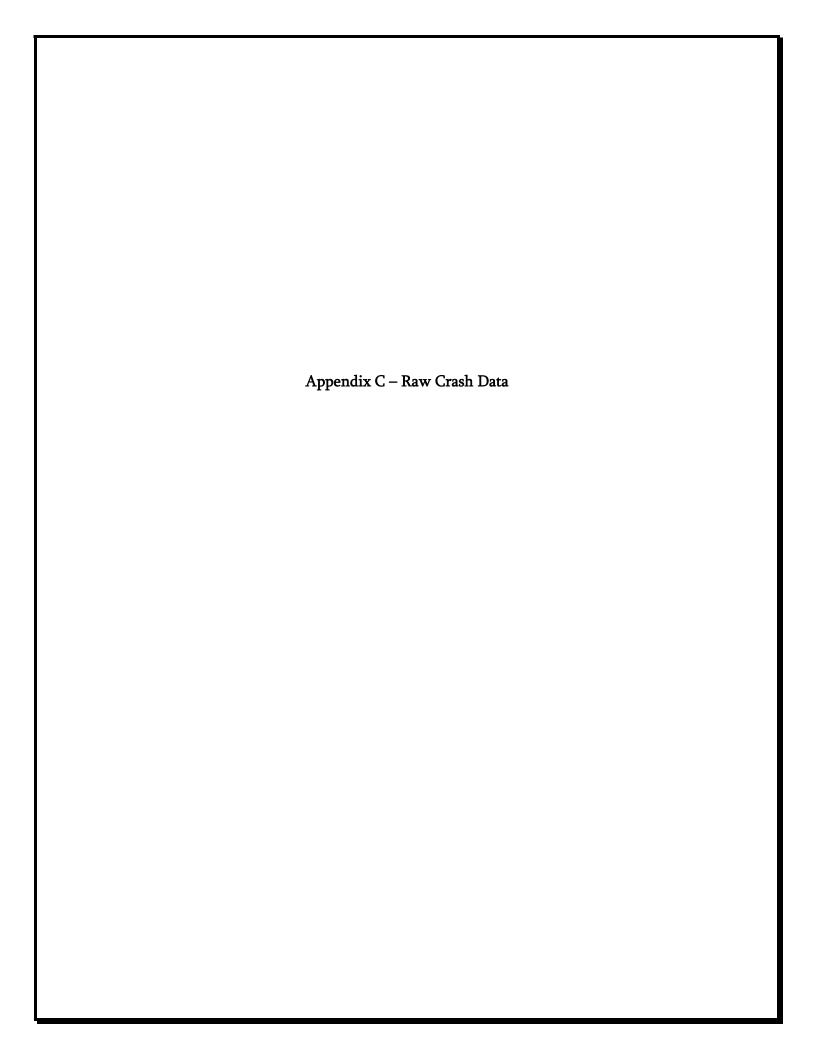
c Critical Lane Group

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	Ť	†	7	7	†	7		4			4	
Volume (veh/h)	30	930	20	5	1365	15	30	0	45	5	0	90
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	33	1011	22	5	1484	16	33	0	49	5	0	98
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.43			0.43	0.43	0.43	0.43	0.43	
vC, conflicting volume	1500			1033			2668	2587	1011	2620	2592	1484
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1500			424			4189	4001	374	4076	4014	1484
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	92			99			0	100	83	0	100	36
cM capacity (veh/h)	427			477			0	1	292	0	1	153
Direction, Lane #	EB 1	EB 2	EB 3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	33	1011	22	5	1484	16	82	103				
Volume Left	33	0	0	5	0	0	33	5				
Volume Right	0	0	22	0	0	16	49	98				
cSH	427	1700	1700	477	1700	1700	0	8				
Volume to Capacity	0.08	0.59	0.01	0.01	0.87	0.01	206.64	12.93				
Queue Length 95th (ft)	6	0	0	1	0	0	Err	Err				
Control Delay (s)	14.1	0.0	0.0	12.6	0.0	0.0	Err	Err				
Lane LOS	В			В			F	F				
Approach Delay (s)	0.4			0.0			Err	Err				
Approach LOS							F	F				
Intersection Summary												
Average Delay			670.7									
Intersection Capacity Utiliz	zation		89.6%	IC	CU Level	of Servic	е		Е			
Analysis Period (min)			15									

	٠	→	\rightarrow	•	•	•	4	†	/	\	ļ	4
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	ሻ	†	7	ሻ	†	7	ሻ	1>	•
Volume (vph)	5	1120	190	145	950	25	320	10	280	15	0	5
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	11	11	11	11	11	11	12	12	12	12	12	12
Grade (%)		-4%			3%			-4%			0%	
Total Lost time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0	6.3	6.3	6.3	6.3	
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Frt	1.00	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.85	
Flt Protected	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	1.00	0.95	1.00	
Satd. Flow (prot)	1633	1719	1461	1577	1660	1411	1689	1778	1511	1770	1583	
Flt Permitted	0.19	1.00	1.00	0.04	1.00	1.00	0.53	1.00	1.00	1.00	1.00	
Satd. Flow (perm)	327	1719	1461	66	1660	1411	948	1778	1511	1863	1583	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	5	1217	207	158	1033	27	348	11	304	16	0	5
RTOR Reduction (vph)	0	0	43	0	0	7	0	0	132	0	5	0
Lane Group Flow (vph)	5	1217	164	158	1033	20	348	11	172	16	0	0
Heavy Vehicles (%)	9%	9%	9%	9%	9%	9%	9%	9%	9%	2%	2%	2%
Turn Type	Perm	NA	Perm	pm+pt	NA	Perm	pm+pt	NA	Perm	Perm	NA	
Protected Phases		6		5	2		3	8			4	
Permitted Phases	6		6	2		2	8		8	4		
Actuated Green, G (s)	95.6	95.6	95.6	108.6	108.6	108.6	26.5	26.5	26.5	3.5	3.5	
Effective Green, g (s)	95.6	95.6	95.6	108.6	108.6	108.6	26.5	26.5	26.5	3.5	3.5	
Actuated g/C Ratio	0.65	0.65	0.65	0.74	0.74	0.74	0.18	0.18	0.18	0.02	0.02	
Clearance Time (s)	6.3	6.3	6.3	5.3	6.3	6.3	4.0	6.3	6.3	6.3	6.3	
Vehicle Extension (s)	3.0	3.0	3.0	0.2	3.0	3.0	3.0	0.2	0.2	0.2	0.2	
Lane Grp Cap (vph)	211	1112	945	127	1220	1037	265	319	271	44	37	
v/s Ratio Prot		0.71		c0.06	0.62		c0.17	0.01			0.00	
v/s Ratio Perm	0.02		0.11	c0.85		0.01	c0.07		0.11	0.01		
v/c Ratio	0.02	1.09	0.17	1.24	0.85	0.02	1.31	0.03	0.63	0.36	0.00	
Uniform Delay, d1	9.3	26.0	10.3	54.1	13.7	5.2	59.5	50.0	56.1	71.0	70.4	
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Incremental Delay, d2	0.0	56.6	0.1	159.6	5.6	0.0	165.2	0.0	3.5	1.9	0.0	
Delay (s)	9.4	82.6	10.4	213.7	19.3	5.3	224.8	50.1	59.7	72.9	70.4	
Level of Service	А	F	В	F	В	Α	F	D	Е	Е	Е	
Approach Delay (s)		71.9			44.2			146.2			72.3	
Approach LOS		E			D			F			Е	
Intersection Summary												
HCM 2000 Control Delay 76.6				Н	Level of	Service		Е				
	ICM 2000 Volume to Capacity ratio 1.31											
Actuated Cycle Length (s)					um of los				21.9			
Intersection Capacity Utiliza	ation		106.3% 15	IC	of Service	9		G				
Analysis Period (min)												

c Critical Lane Group

	۶	→	•	•	+	•	1	†	/	/	↓	-√
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ሻ	†	7	7	↑	7		4			4	
Volume (veh/h)	30	1365	20	30	1070	10	20	0	40	5	5	30
Sign Control		Free			Free			Stop			Stop	
Grade		3%			-4%			0%			0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	33	1484	22	33	1163	11	22	0	43	5	5	33
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)		1058										
pX, platoon unblocked				0.36			0.36	0.36	0.36	0.36	0.36	
vC, conflicting volume	1174			1505			2812	2788	1484	2821	2799	1163
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1174			1515			5105	5038	1455	5128	5068	1163
tC, single (s)	4.2			4.2			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.3			2.3			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	94			79			0	100	25	0	0	86
cM capacity (veh/h)	571			153			0	0	58	0	0	237
Direction, Lane #	EB 1	EB 2	EB 3	WB 1	WB 2	WB 3	NB 1	SB 1				
Volume Total	33	1484	22	33	1163	11	65	43				
Volume Left	33	0	0	33	0	0	22	4 3				
Volume Right	0	0	22	0	0	11	43	33				
cSH	571	1700	1700	153	1700	1700	0	0				
Volume to Capacity	0.06	0.87	0.01	0.21	0.68	0.01	Err	403.52				
Queue Length 95th (ft)	5	0.67	0.01	19	0.00	0.01	Err	403.32 Err				
Control Delay (s)	11.7	0.0	0.0	34.7	0.0	0.0	Err	Err				
Lane LOS	11.7 B	0.0	0.0	34.7 D	0.0	0.0	F	F				
Approach Delay (s)	0.2			0.9			Err	Err				
Approach LOS	0.2			0.9			F	F				
							'	'				
Intersection Summary			Frr									
3			Err 86.0%	10	NII ovel	of Convice						
Intersection Capacity Utilizat	IUH			IC	o Level (of Service			E			
Analysis Period (min)			15									



Date Time Milelog Route Crash Fatalities Collision Impact UlEvent Light Surface DirVeh1 MnvrVeh1 U1Factors DULUTH HWY SR NORTHMO 1/30/2012 8:23:00 120 0 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry South Straight too Close DULUTH SR NORTHMO 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR NORTHMO 0 NORTHMO 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR NORTHMO 0 Rear End Roadway Motion Daylight Dry East Straight too Close	South	MnvrVeh2 Straight	No Contributin
DULUTH HHWY SR NORTHMO 0 Rear End Roadway Motion Daylight Dry South Straight too Close DULUTH SR NORTHMO NORT	South		No Contributin
HWY SR NORTHMO 1/30/2012 8:23:00 120 0 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry South Straight Following too Close NORTHMO 1/30/2012 12:08:00 120 HWY 0 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR NORTHMO 0 NT PKWY 0 OR Rear End Roadway Motion Daylight Dry East Straight Following Too Close North	South	Straight	Contributin
1/30/2012 8:23:00 120 0 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry South Straight too Close NORTHMO NORTHMO NORTHMO NT PKWY NORTHMO NORTH	South	Straight	
DULUTH SR NORTHMO 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR NORTHMO 0 O Rear End Roadway Motion Daylight Dry Following Too Close On Vehicle In Dark-Not Following F		Straight	a Eactors
DULUTH SR NORTHMO 1/30/2012 12:08:00 120 HWY 0 NT PKWY 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR NORTHMO			g Factors
1/30/2012 12:08:00 120 HWY 0 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry East Straight too Close DULUTH SR			No
DULUTH SR NORTHMO On Vehicle In Dark-Not Following			Contributin
DULUTH SR NORTHMO On Vehicle In Dark-Not Following	East	Stopped	g Factors
DULUTH SR NORTHMO On Vehicle In Dark-Not Following			No
2/8/2012 21:41:00 120 HWY 0 NT PKWY 1 0 Rear End Roadway Motion Lighted Dry East Straight too Close			Contributin
	East	Stopped	g Factors
DULUTH Motor			No
DULUTH Motor HWY SR NORTHMO On Vehicle In Following			Contributin
7/16/2015 16:38:00 120 5.02 NT PKWY 1 0 Rear End Roadway Motion Daylight Dry East Straight too Close	East	Stopped	g Factors
2434			
DULUTH Sideswipe- Motor No No HWY SR Same On Vehicle In Contributi	in		No Contributin
2/22/2015 13:33:00 120 5.02 0 0 Direction Roadway Motion Daylight Wet West Straight g Factors	West	Straight	g Factors
2400			
DULUTH SR Motor 120 HWY NORTHMO On Vehicle In Dark- Turning Failed to			No Contributin
3/14/2013 22:13:00 NW 5.02 NT PKWY 1 0 Head On Roadway Motion Lighted Dry South Left Yield	East	Straight	g Factors
DULUTH Motor HWY SR NORTHMO On Vehicle In Following			No
HWY SR NORTHMO On Vehicle In Following 7/2/2014 17:02:00 120 5.02 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry South Straight too Close		Stopped	Contributin g Factors
Motor			No
DULUTH SR NORTHMO On Vehicle In Following 9/21/2014 13:51:00 120 HWY 5.02 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry East Straight too Close	East	Stopped	Contributin g Factors
SIZINI SI	2001	оторрец	g · uctors
DULUTH Motor			No
HWY SR NORTHMO On Vehicle In Following 10/7/2014 7:31:00 120 5.02 NT PKWY 1 0 Rear End Roadway Motion Daylight Dry West Straight too Close	West	Stopped	Contributin g Factors
10/7/2014 7.51.00 120 3.02 NT PKWT 1 OREAL ETIU ROBUWAY MOLION DAYINGTIL DIY WEST Straight Loo close		эторрец	g ractors
Motor too			No
DULUTH SR NORTHMO On Vehicle In Close, Dist		Chamand	Contributin
######### 17:48:00 120 HWY 5.02 NT PKWY 0 0 Rear End Roadway Motion Dusk Dry East Straight acted	East	Stopped	g Factors
Following Following			
too			
	at		No Contributin
######################################	s East	Straight	g Factors
DULUTH			No Contributin
HWY NORTHMO On Vehicle In Turning Following ########## 13:08:00 SR120 5.02 NT PKWY 0 0 Rear End Roadway Motion Daylight Dry East Right too Close		Stopped	g Factors

D-4-	- :		Battala	Intersectin	Injury	For Batter	MannerOf	LocationOf		I Solat	Conferen	District 1	B. 8	III Farebaue	IntersectR	District 2	84	1125
Date	Time		Milelog	gRoute	Crash	Fatalities	Collision	Impact	ulEvent	Light	Surface	DirVeh1	MnvrVeh1	U1Factors	outeType	DirVeh2	MnvrVeh2	U2Factors
									Motor									No
		DULUTH		NORTHMO				On	Vehicle In					Following				Contributin
12/9/2014	9:59:00	HWY	5.02	NT PKWY	1	0	Rear End	Roadway	Motion	Daylight	Dry	South	Straight	too Close		South	Stopped	g Factors
														Following				
														too				
									Motor					Close,Weat				No
1/15/2015	17.20.00	DULUTH SR 120 HWY	E 02	NORTHMO NT PKWY		0	Rear End	On Roadway	Vehicle In Motion	Dusk	Wet	East	Ctraight	her Conditions		East	Stannad	Contributin
1/13/2013	17.26.00	120 HW1	3.02	INTPRVVI		U	Real Ellu	Noduway	WIOLIOII	Dusk	wet	EdSt	Straight	Conditions		EdSt	Stopped	g Factors
									Motor									No
		DULUTH SR		NORTHMO				On	Vehicle In					Following				Contributin
1/23/2015	8:05:00	120 HWY	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Wet	West	Straight	too Close		West	Straight	g Factors
									Motor									No
		DULUTH SR		NORTHMO				On	Vehicle In	Dark-				Following				Contributin
2/5/2015	18:39:00	120 HWY	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Lighted	Dry	North	Straight	too Close		North	Stopped	g Factors
		DULUTH SR												Object Or				
		120 HWY		NORTHMO				On		Dark-Not				Object Or Animal,Dist				
4/13/2015	3:00:00		5.02	NT PKWY	0	0	Angle	Roadway	Deer	Lighted	Dry	East	Straight	racted				
									Motor									
4/26/2015	11:13:00	SP 120	5.02	NORTHMO NT PKWY	1	0	Angle	On Roadway	Vehicle In Motion	Daylight	Dry	West	Straight	Driver Lost Control				
4/20/2013	11.13.00	3N 120	3.02	INTERVO	1	U	Aligie	Noauway	WIOTION	Daylight	ыу	West	Juaignu	Control				
									Motor									No
c /2 /2 c =	40.45.00	DULUTH SR		NORTHMO				On	Vehicle In					Following				Contributin
6/2/2015	19:15:00	120 HWY	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	too Close		West	Stopped	g Factors
		DULUTH							Motor									No
		HWY		NORTHMO				On	Vehicle In					Following				Contributin
6/17/2015	21:10:00	SR120	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	East	Straight	too Close		East	Stopped	g Factors
									Motor									No
				NORTHMO				On	Vehicle In					Following				Contributin
7/16/2015	9:11:00	SR 120	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	too Close		West	Straight	g Factors
									Motor									No
		DULUTH SR		NORTHMO				On	Motor Vehicle In					Following				No Contributin
5/8/2015	17:38:00	120 HWY	5.02	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	North	Straight	too Close		North	Straight	g Factors
		DULUTH SR		NORTHMO			Sideswipe- Same	On	Motor Vehicle In				Making U-	Failed to				No Contributin
2/28/2010	12:19:00	120 HWY	5.02	NT PKWY	0		Same Direction	Roadway	Motion	Daylight	Dry	North	turn	Yield		North	Straight	g Factors
, = 0, = 310			5.02					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		.,	1					7		0 2222.0
									Motor] .				l				No
3/10/2010	20.06.00	DULUTH SR 120 HWY	5.02	NORTHMO NT PKWY	0	_	Rear End	On Roadway	Vehicle In Motion	Dark-Not	Wet	East	Straight	Following too Close		Fact	Stopped	Contributin
3/10/2010	20:00:00	TZO HAA I	5.02	INITAVVI		1 0	near Ellu	inuauway	IVIULIUII	Lighted	wei	EdSt	Straight	too close	l	East	Stopped	g Factors

				Intersectin	Injury		MannerOf	LocationOf	FirstHarmf						IntersectR			
Date	Time		Milelog	gRoute	Crash	Fatalities	Collision	Impact	ulEvent	Light	Surface	DirVeh1	MnvrVeh1	U1Factors	outeType	DirVeh2	MnvrVeh2	U2Fa
																		NI-
		DULUTH SR		NORTHMO				On	Motor Vehicle In					Fallouring				No Cont
5/7/2011	15:14:00	120 HWY	5.02	NT PKWY	1	0	Rear End	Roadway	Motion	Daylight	Dry	East	Straight	Following too Close		East	Straight	g Fac
3/1/2011	13.14.00	DULUTH	3.02	IVIIIVVI		0	itear Ena	Nodaway	WIGHOU	Dayligit	ыу	Lust	Straight	too close		Lust	Juaigne	g i u
		HIGHWAY							Motor									No
		SR120		NORTHMO				On	Vehicle In	Dark-				Following				Cont
6/8/2012	21:17:00	2400	5.03	NT PKWY	1	0	Rear End	Roadway	Motion	Lighted	Dry	East	Straight	too Close		East	Stopped	g Fa
														Following				
														too				
		DI II I I I I I I I I I I I I I I I I I		NODTUNA				_	Motor					Close,Misju				No
C /4.2 /204.2	F-20-00	DULUTH SR	F 02	NORTHMO			D	On	Vehicle In	Dark-	\A/-+	\A/+	C+:	dged		\A/+	Ctural alata	Cont
6/12/2012	5:30:00	120, HWY	5.03	NT PKWY	0	0	Rear End	Roadway	Motion	Lighted	Wet	West	Straight	Clearance		West	Straight	g Fac
														Changed				
		DULUTH					Sideswipe-		Motor					Lanes				No
		HWY S R		NORTHMO			Same	On	Vehicle In				Changing	Improperly,				Cont
6/16/2012	19:53:00	120 NW	5.03	NT PKWY	0	0	Direction	Roadway	Motion	Daylight	Dry	East	Lanes	Inattentive		East	Straight	g Fa
									Motor									No
c /a = /a a . a		DULUTH SR		NORTHMO				On	Vehicle In	Dark-			Turning	Failed to				Cont
6/25/2012	15:19:00	120 HWY	5.03	NT PKWY	0	0	Angle	Roadway	Motion	Lighted	Dry	East	Left	Yield		West	Straight	g Fa
									Motor									No
		DULUTH SR		NORTHMO				On	Vehicle In					Following				Cont
7/27/2012	18:24:00	120 HWY	5.03	NT PKWY	1	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	too Close		West	Stopped	g Fa
							Not A											
		DULUTH					Collision	255	Motor									
4/25/2012	15:59:00	HWY SR	0	NORTHMO NT PKWY	0		with Motor Vehicle	Off Roadway	Vehicle In	Davlight	Dest	West	Ctroight	Driver Lost				
4/25/2012	15.59.00	120	U	NIPKWY	U	U	venicie	Roadway	Motion	Daylight	Dry	west	Straight	Control				
									Motor									No
				NORTHMO				On	Vehicle In					Following				Cont
4/28/2012	15:47:00	SR 120	0	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	too Close		West	Straight	g Fa
		DULUTH							Motor									No
E /4 /2014	10.10.00	HWY SR	F 00	NORTHMO	_	_	D	On	Vehicle In	Davidiale	D	Name	Chun i mh b	Following		NI	C+	Cont
5/1/2014	19:19:00	120	5.03	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Dry	North	Straight	too Close		North	Stopped	g Fa
							Sideswipe-		Motor									
		DULUTH SR		NORTHMO			Opposite	On	Vehicle In									
5/29/2014	8:46:00	120 HWY	5.03	NT PKWY	0		Direction	Roadway	Motion	Daylight	Dry	West	Straight	Other		East	Straight	Othe
			_			_	_											
							Not A											
							Collision		Motor									
- 4		DULUTH SR		NORTHMO			with Motor		Vehicle In									
5/13/2014	17:09:00	120 HWY	5.03	NT PKWY	0	0	Vehicle	Roadway	Motion	Daylight	Dry	East	Straight	Other				

Date	Time		Milelog	Intersectin gRoute	Injury Crash	Fatalities	MannerOf Collision	LocationOf Impact	FirstHarmf ulEvent	Light	Surface	DirVeh1	MnvrVeh1	U1Factors	IntersectR outeType	DirVeh2	MnvrVeh2	U2Factors
5/21/2014	16:01:00	DULUTH HWY	5.03	NORTHMO NT PKWY	0	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	East	Straight	Following too Close		East	Stopped	No Contributin g Factors
9/17/2010		2444 DULUTH HWY SR 120		NORTHMO NT PKWY	1	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	East	Straight	Following too Close,Mec hanical Or Vehicle Failure		East	Straight	No Contributin g Factors
4/21/2010	12:46:00	DULUTH HWY SR 120	5.03	NORTHMO NT PKWY	0	0	Rear End	On Roadway	Motor Vehicle In Motion Motor	Daylight	Dry	East	Straight	Following too Close		East	Stopped	No Contributin g Factors
8/19/2010	6:15:00	DULUTH HWY	5.03	NORTHMO NT PKWY	1	. 0	Angle	Off Roadway	Vehicle In Motion	Dark- Lighted	Dry	West	Straight	Distracted				
10/5/2010	8:52:00	DULUTH SR 120 HWY		NORTHMO NT PKWY	0	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	West	Stopped	No Contributin g Factors		West	Straight	Following too Close
#########	7:30:00	DULUTH HIGHWAY SR 120	5.03	NORTHMO NT PKWY	0	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Wet	East	Straight	Following too Close		East	Straight	No Contributin g Factors
3/15/2011	7:22:00	DULUTH SR 120 HWY		NORTHMO NT PKWY	1	0	Angle	On Roadway	Motor Vehicle In Motion	Dawn	Wet	South	Turning Left	Failed to Yield		East	Straight	No Contributin g Factors
#########	8:02:00	SR 120 NORTHMO	0	NORTHMO NT PKWY	1	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Wet	East	Straight	Following too Close		East	Straight	No Contributin g Factors
9/6/2015	7:57:00	NT PKWY AND DULUTH	0		0	0	Not A Collision with Motor Vehicle	On Roadway	Motor Vehicle In Motion	Daylight	Dry	North	Straight					
8/29/2013	8:45:00	DULUTH SR 120 HWY	5.02	NORTHMO NT PKWY	0	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	East	Straight	Following too Close		East	Straight	No Contributin g Factors
7/21/2013	11:04:00	HWY 120 DULUTH HWY		STAUNTON DR	0		Not A Collision with Motor Vehicle	On Roadway	Guard Rail Face	Daylight	Dry	East	Straight	Driver Lost Control				
6/3/2010				STAUNTON DR	1		Angle	On Roadway	Motor	Dark-Not Lighted	Dry		J					

				Intersectin	Injury		MannerOf	LocationOf	FirstHarmf						IntersectR			
Date	Time		Milelog	gRoute	Crash	Fatalities	Collision	Impact	ulEvent	Light	Surface	DirVeh1	MnvrVeh1	U1Factors	outeType	DirVeh2	MnvrVeh2	U2Factors
3/21/2012	19:15:00	DULUTH HWY	0	STAUNTON DR	1	0	Angle	On Roadway	Motor Vehicle In Motion	Daylight	Dry	North	Straight	Failed to Yield		West	Straight	No Contributin g Factors
#########	4:39:00	DULUTH HWY NW	5.23	STAUNTON DR	1	0	Angle	On Roadway	Motor Vehicle In Motion	Dark-Not Lighted	Dry	North	Turning Left	Failed to Yield		West	Straight	No Contributin g Factors
12/3/2011	19:31:00	DULUTH HWY SR 120	5.23	STAUNTON DR	0	0	Not A Collision with Motor Vehicle	On Roadway	Deer	Dark-Not Lighted	Dry	East	Straight	No Contributin g Factors				
		DULUTH HIGHWAY	5.23	STAUNTON	0		Head On	On Shoulder		Dark-Not		West		Driver Lost Control,Ch anged Lanes Improperly, Driver				
3/15/2013 4/17/2013	7:54:00	DULUTH HIGHWAY 2370 SR		STAUNTON	0		Rear End	On Roadway	Motor Vehicle In Motion	Lighted Daylight	Dry	West	Straight Straight	Following too Close		West	Straight	No Contributin g Factors
11/8/2013		DULUTH SR 120 HWY		STAUNTON DR	0	0	Angle	On Roadway	Motor Vehicle In Motion	Daylight	Dry	West	Turning Left	Failed to Yield		South	Turning Left	
3/8/2014	7:23:00	DULUTH SR 120 HWY		STAUNTON DR	0	0	Head On	On Roadway	Guard Rail Face	Daylight	Dry	West	Straight	Driver Lost Control,Ina ttentive				
3/12/2014	16:28:00	DULUTH HWY SR 120		STAUNTON DR	0	0	Angle	On Roadway	Motor Vehicle In Motion	Daylight	Dry	East	Making U- turn	Improper Turn		West	Straight	No Contributin g Factors
3/14/2014	8:19:00	DULUTH SR 120 HWY		STAUNTON DR	0	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	East	Straight	Following too Close		East	Straight	No Contributin g Factors
5/24/2014		DULUTH HWY		STAUNTON DR	0	0	Not A Collision with Motor Vehicle	On Shoulder	Guard Rail End	Daylight	Dry	West	Straight	No Contributin g Factors		West	Straight	No Contributin g Factors
6/22/2014	10:24:00	DULUTH HWY SR 120	0	STAUNTON DR	1	0	Rear End	On Roadway	Motor Vehicle In Motion	Daylight	Dry	West	Straight	Following too Close		West	Stopped	No Contributin g Factors

				lutum stin			N4Of		Finallanus						lutuur at D			
Date	Time		Milelog	Intersectin gRoute	Injury Crash	Fatalities	MannerOf Collision	LocationOf Impact	FirstHarmf ulEvent	Light	Surface	DirVeh1	MnvrVeh1	U1Factors	IntersectR outeType	DirVeh2	MnvrVeh2	U2Factors
		DULUTH							Motor									No
		HWY SR		STAUNTON				On	Vehicle In				Turning	Failed to				Contributin
8/4/2014	9:02:00	120	0	DR	0	0	Angle	Roadway	Motion	Daylight	Dry	South	Left	Yield		West	Straight	g Factors
									Motor									No
		DULUTH		STAUNTON				On	Vehicle In					Following				Contributin
4/22/2011	15:42:00	HWY	0	DR	0	0	Rear End	Roadway	Motion	Daylight	Wet	East	Straight	too Close		East	Straight	g Factors
		DULUTH							Motor									No
		HWY		STAUNTON				On	Vehicle In					Following				Contributin
#########	7:21:00	SR120	0	DR	0	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	too Close		West	Straight	g Factors
		DULUTH							Motor					Following too				No
		HWY S R		STAUNTON				On	Vehicle In					Close,Distr				Contributin
4/21/2014	8:11:00	120	0	DR	0	0	Rear End	Roadway	Motion	Daylight	Dry	West	Straight	acted		West	Stopped	g Factors
									Motor									No
		DULUTH SR		NORTHMO				On	Vehicle In	Dark-				Following				Contributin
#########	17:35:00	120 HWY	0	NT PKWY	0	0	Rear End	Roadway	Motion	Lighted	Wet	East	Straight	too Close		East	Stopped	g Factors
									Motor									No
				NORTHMO				On	Vehicle In					Following				Contributin
#########	15:31:00	SR 120	0	NT PKWY	1	. 0	Rear End	Roadway	Motion	Daylight	Dry	East	Straight	too Close		East	Stopped	g Factors
									Motor									No
				NORTHMO				On	Vehicle In					Following				Contributin
9/6/2013	17:23:00	SR 120	5.02	NT PKWY	1	. 0	Rear End	Roadway	Motion	Daylight	Dry	East	Straight	too Close		East	Stopped	g Factors
		DULUTH					Sideswipe-		Motor									No
		HWY SR		NORTHMO			Opposite	On	Vehicle In									Contributin
5/5/2010	13:49:00	120	0	NT PKWY	0	0	Direction	Roadway	Motion	Daylight	Dry	North	Straight	Other		North	Straight	g Factors
		DULUTH							Motor									No
		HWY		NORTHMO				On	Vehicle In					Following				Contributin
2/6/2015	8:20:00	SR120	5.02	NT PKWY	1	. 0	Rear End	Roadway	Motion	Daylight	Dry	East	Straight	too Close		East	Stopped	g Factors
		DULUTH							Motor					No				No
		HWY		NORTHMO				On	Vehicle In					Contributin				Contributin
2/6/2015	8:21:00		5.02	NT PKWY	1	. 0	Rear End	Roadway	Motion	Daylight	Dry	East	Stopped	g Factors		East	Stopped	g Factors
		SR 120 DULUTH							Motor									No
		HWY SR		NORTHMO				On	Vehicle In				Turning	Improper				Contributin
9/18/2015	11:16:00	120 HWY	0	NT PKWY	0	0	Angle	Roadway	Motion	Daylight	Dry	East	Right	Turn		East	Straight	g Factors
		SR 120 DULUTH		1				1	Motor				1	1				No
		HWY SR		NORTHMO				On	Vehicle In					Following				Contributin
9/28/2015	16:22:00	120 HWY	0	NT PKWY	0	0	Rear End	Roadway	Motion	Daylight	Wet	North	Straight	too Close		North	Straight	g Factors

Processed Date:5/20/2015

Bridge Inventory Data Listing

OF OF STREET

Parameters: Bridge Serial Num

Structure ID:135-0023-0	G	winnett				SUFF. RATING: 58.70		
Location & Geography		*104 III 1 2	O Inventory Destates	n the NUIC		Signs & Attachments		
Structure ID:	135-0023-0	*104 Highway System:	0- Inventory Route is not of	II UIE NHS		005 E	00.0	
200 Brdge Information:	06	*26 Functional Classification:			0.1.00.1	225 Expansion Joint Type:	o2- Open or sealed sealant). 1- Open Scuppers.	concrete joint (silicone
6A Feature Int:	SINGLETON CREEK	*204 Federal Route Type:	F - Primary.	No:	01891	242 Deck Drains:		
6B Critical Bridge:	0000400	105 Federal Lands Highway: *110 Truck Route:	Not applicable 0			243 Parapet Location:	0- None present.	
7A Route No Carried:	SR00120	206 School Bus Route:	1			Height:	0.00	
7B Facility Carried:	DULUTH HIGHWAY	217 Benchmark Elevation:	0000.00			Width:	0.00	
Location:	1.5 MI E OF DULUTH	218 Datum:	0- Not Applicable			238 Curb Height:	1	
Dot District:	4841100000 - D1 DISTRICT ONE	****	0			Curb Material:	1- Concrete.	4. O
07 Year Photo:	2014	*19 Bypass Length:	2	Literaco		239 Handrail	1- Concrete.	1- Concrete.
91 Inspection Frequency:	24 Date: 01/31/2014	*20 Toll:	3- On a Free Road or Non-	-Highway		*240 Median Barrier Rail:	0- None.	
2A Fract Crit Insp Freq:	0 Date: 02/01/1901	*21 Maintanance:	01-State Highway Agency.			241 Bridge Median Height:	0	
2B Underwater Insp Freq:	00 Date: 02/01/1901	*22 Owner:	01-State Highway Agency.			* Bridge Median Width:	0	
2C Other Spc. Insp Freq:	00 Date: 02/01/1901	*31 Design Load:	2- H 15	nol Desister of Ut-to	orio Dioces	230 Guardrail Loc. Dir. Rear:	3- Both sides.	
4 Place Code:	00000	37 Historical Significance:	5- Not eligible for the Natio	riai Register of Histo	DIIC Places	Fwrd:	3- Both sides.	
5 Inventory Route(O/U):	1	205 Congressional District:	7 - SEVEN			Oppo. Dir. Rear:	0- None.	
Type:	3 - State	27 Year Constructed:	1938			Oppo. Fwrd:	0- None.	
Designation:	1- Mainline	106 Year Reconstructed:	0			244 Aproach Slab	0- None.	
Number:	00120	33 Bridge Median	0-None			224 Retaining Wall:	0- None.	
Direction:	0. Not applicable	34 Skew:	20			233Posted Speed Limit:	50	
16 Latitude:	33.0000- 58.7214 HMMS Prefix:SR	35 Structure Flared:	No	lad by an Annan		236 Warning Sign:	1.00	
17 Longtitude:	84.0000- 6.5700 HMMS Suffix:120	38 Navigation Control:	0- Navigation is not control	led by an Agency		234 Delineator:	1.00	
	MP: 5.13	213 Special Steel Design:	0- Not applicable or other	\ // \ // \		235 Hazard Boards:	1	
8 Border Bridge:	% Shared:00	267 Type of Paint:	5- Waterborne System (Ty	pe vi or vii)		237 Utilities Gas:	00- Not Applicable	
99 ID Number:	00000000000000	*42 Type of Service On:	1-Highway			Water:	00- Not Applicable	
100 STRAHNET:	0- The Feature is not a STRAHNET route.	Type of Service Under:	5-Waterway 0			Electric:	00- Not Applicable	
2 Base Highway Network:	1	214 Movable Bridge:		Otaal O O	rata	Telephone:	00- Not Applicable	
13A LRS Inventory Route:	1351012000	203 Type Bridge:	A- Spread - O. Concrete M 3	. Steel - O. Conc	rete	Sewer:	00- Not Applicable	
3B Sub Inventory Route:	0.00	259 Pile Encasement	4-Steel (Continuous)	2 Strings-/AA	ulti-Beam or Girder	247 Lighting Street	0	
*101 Parallel Structure:	N. No parallel structure exists	*43 Structure Type Main:	4-Steel (Continuous)	z-Suinger/M	uiu-Deam Of Gifuer	247 Lighting Street:	U	
*102 Direction of Traffic:	2- Two Way	45 No.Spans Main:		0- Other		Navigation:	0	
*264 Road Inventory Mile Post:	005.13	44 Structure Type Appr:	0- Other 0	u- Gulei		Aerial:	0- Not :	
208 Inspection Area:	Area 07 Initials: JPD	46 No Spans Appr:				*248 County Continuity No.:	00	
Engineer's Initials:	jpd	226 Bridge Curve Horz	0 Vert: 0.00	andod O at Fasting	o not a water-			
* Location ID No:	135-00120D-005.13E	111 Pier Protection	N - Navigation Control item	i coded u, or Heatur	e not a waterway			
		107 Deck Structure Type:						
		108 Wearing Structure Typ	e:					
		Membrane Type:						
		Deck Protection:						

Processed Date:5/20/2015

Parameters: Bridge Serial Num

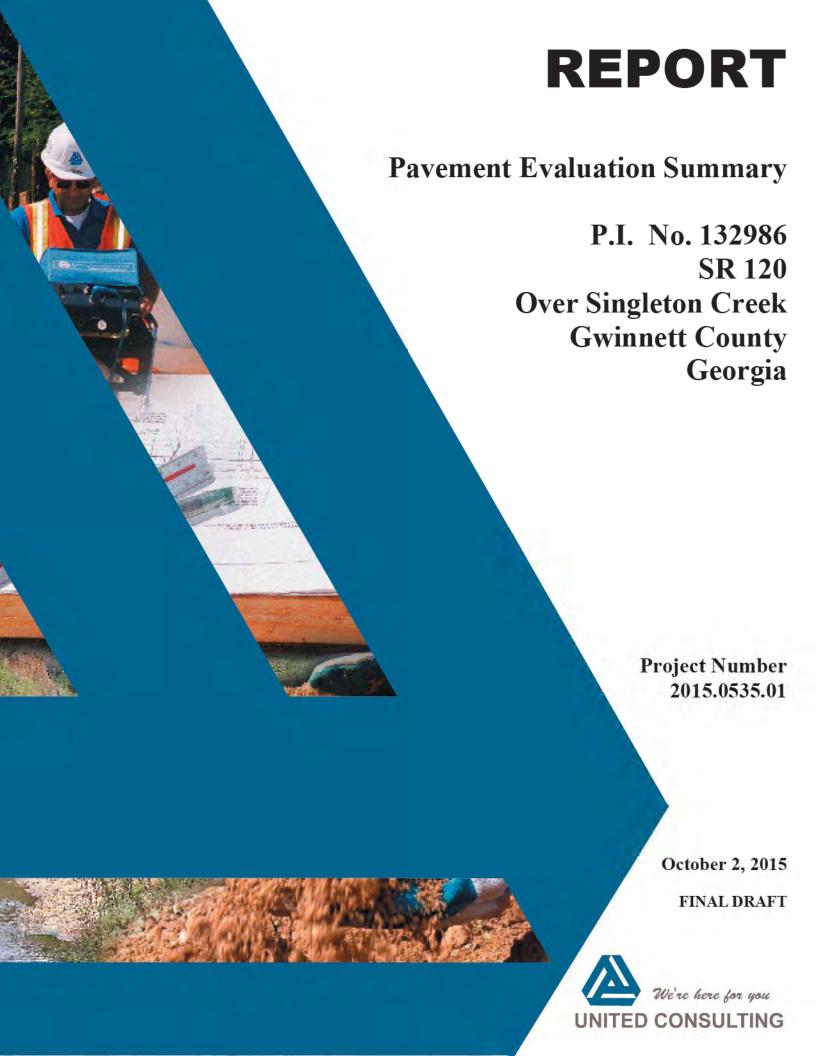
Bridge Inventory Data Listing

THE OF SEASO

Structure ID:135-0023-0

Structure ID:13	5-0023-0				
Programming Data	F-2661-B	Measurements:		65 Inventory Rating Method:	2-Allowable Stress (AS)
201 Project No: 202 Plans Available:	4- Plans in Infolmage.	*29 ADT	20360 Year: 2012	63 Operating Rating Method:	2-Allowable Stress (AS)
249 Prop Proj No:	BRST-189-1 (30)	109 %Trucks:	1	66 Inventory Type:	2 - HS loading. Rating: 22
250 Approval Status:	6102	* 28 Lanes On:	2 Under:0	64 Operating Type:	2 - HS loading. Rating: 35
251 PI Number:	132986-	210 No. Tracks On:	00 Under:00	231Calculated Loads:	
252 Contract Date:	02/01/2007	* 48 Max. Span Length	25	H-Modified:	20 0
260 Seismic No:	00000	* 49 Structure Length:	75	HS-Modified:	25 0
75 Type Work:	34- Widening 1- Work to be don	51 Br. Rwdy. Width	23.90	Type 3:	26 0
94 Bridge Imp: Cost:	with dack \$293	52 Deck Width:	26.50	Type 3s2:	40 0
95 Roadway Imp. Cost:	\$29	* 47 Tot. Horiz. Cl:	24	Timber:	35 0
96 Total Imp Cost:	\$440	50 Curb / Sidewalk Width	0.00 / 0.00	Piggyback:	40 0
76 Imp Length:	1397	32 Approach Rdwy. Width	40	261 H Inventory Rating:	15
97 Imp Year:	2013	*229 Shoulder Width:		262 H Operating Rating	21
114 Furure ADT:	30540 Year:2032	Rear Lt:	2.00 Type:3 - Rt:7	67 Structural Evaluation:	6
Hydralia Data		Fwd. Lt:	2.00 Type:2 - Rt:2	58 Deck Condition:	7 - Good Condition
Hydralic Data		Pavement Width:		59 Superstructure Condition:	7 - Good Condition
215Waterway Data: High Water Elev:	0000.0 Year:1900	Pavement width: Rear:	32.00 Type: 2- Asphalt.	* 227 Collision Damage:	0
Flood Elev:	0000.0 Fear. 1900	rteal.	36.00 Type: 2- Asphalt.	60A Substructure Condition:	6 - Satisfactory Condition
Avg Streambed Ele	•	Intersaction Rear:	1 Fwd: 0	60B Scour Condition:	8 - Very Good Condition
Drainage Area:	00000	36Safety Features Br. Rail		60C Underwater Condition	N - Not Applicable
Area of Opening:	00000	Transition:	2- Inspected feature meets acceptable construction date standards. 2- Inspected feature meets acceptable construction date standards.	71 Waterway Adequacy:	8-Equal to present desirable criteria.
113 Scour Critical	U. No Load Rating; no scour critical data		2- Inspected feature meets acceptable construction date standards. 2- Inspected feature meets acceptable construction date standards.	61 Channel Protection Cond.:	8
216 Water Depth:	2.4 Br.Height:11	App. Rail End:	2- Inspected feature meets acceptable construction date standards.	68 Deck Geometry:	2
222 Slope Protection:	0	53 Minimum Cl. Over:	99'99"	69 UnderClr. Horz/Vert:	N
221Spur Dikes Rear	0 Fwd:0	Under: N- Feature no		72 Appr. Alignment:	6-Minor reduction of vehicle operating speed required.
219 Fender System	0- None.	*228 Minimum Vertical CI		62 Culvert:	N - Not Applicable
220 Dolphin:		Act. Odm Dir::	99 ' 99"	Posting Data	
223 Culvert Cover:	000	Oppo. Dir:	99' 99"	70 Bridge Posting Required	5. Equal to or above legal loads
Type:	0- Not Applicable	Posted Odm. Dir:	00' 00"	41 Struct Open, Posted, CL:	A. Open, no restriction
No. Barrels:	0	Oppo. Dir:	00'00 "	* 103 Temporary Structure:	0
Width:	0.00 Height:0	55 Lateral Undercl. Rt:	N- Feature not a highway or railroad. 0.00	232 Posted Loads	
Length:	0 Apron:0	56 Lateral Undercl. Lt:	0.00	H-Modified:	00
*265 U/W Insp. Area	0 Diver:ZZZ	*10 Max Min Vert CI:	99' 99" Dir:0	HS-Modified:	00
*Location ID No:	135-00120D-005.13E	39 Nav Vert CI:	000 Horiz:0	Type 3:	00
		116 Nav Vert CI Closed:	000	Type 3s2:	00
		245 Deck Thickness Main	7.00	Timber:	00
		Deck Thick Approach		Piggyback	00
		246 Overlay Thickness:	5.00	253 Notification Date:	02/01/1901
		212 Year Last Painted:	Sup:2000 Sub:0000	258 Fed Notify Date:	02/01/1901







October 2, 2015

Mr. Ben Clopper, P.E Michael Baker International 420 Technology Parkway Suite 150 Norcross, Georgia 30092

Via Email: Ben.Clopper@mbakerintl.com

PROJECT: Report of Pavement Evaluation Summary

P.I. No. 132986

SR 120 Over Singleton Creek Gwinnett County, Georgia UC Project No. 2015.0535.01

Dear Mr. Clopper:

United Consulting is pleased to submit this report of the Pavement Evaluation Summary for the above referenced project site. We appreciate the opportunity to assist you with this project and look forward to working with you on future projects. If you have any questions regarding this report, or if we can of further assistance, please feel free to contact us.

Sincerely,

UNITED CONSULTING

Lonne Rucker

Lonnie Rucker, E.I.T.

Staff Engineer

a. sout

Santanu Sinharoy, P.E. Chief Geotechnical Engineer

Registration No. 20064

LR/REH/SS/nj

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20064

FINAL DRAFT

Bay E. Dalley

Ray E. Halbert, P.E.

Senior Geotechnical Engineer

PAVEMENT EVALUATION SUMMARY For PI No. 132986 Gwinnett County, Georgia

1. LOCATION / DESCRIPTION

This project is for the roadway improvement and replacement of a bridge on SR 120 (Duluth Highway) over Singleton Creek. The proposed improvement will consist of realignment of the roadway to accommodate the new bridge over Singleton Creek. The relocation of SR 120 will consist of two, 12 ft wide lanes with 10 ft wide rural shoulders (2 ft paved). The total length of the project is about 0.34 miles. The project is located within the following station limits based on the preliminary drawing provided at the time of this survey. This project is located outside the city limits of Duluth and within Gwinnett County, Georgia.

Station to Station	Location
14+00± to 32+00±	SR 120

2. PAVEMENT CONDITION SUMMARY

SR 120 (Duluth Highway) (Sta. 14+00 to Sta. 20+90 and Sta. 26+28 to Sta. 32+00)

The areas proposed to be retained on SR 120 (Duluth Highway) are in poor to good condition based on the latest COPACES rating in 2014 and on the finding of our field observations. The pavement distresses and core conditions from this evaluation are summarized in Section 6 and Section 8 of this report.

Based on our opinion, the existing pavement can be overlaid provided it is milled 2.0 inches prior to overlaying.

For additional information resulting in the provided recommendations see "Item 11 – Assumptions and Justification' section for details.

3. PAVEMENT RECOMMENDATION SUMMARY

The following types of construction are recommended along the roadway improvement for **SR 120** and associated Side Roads.





Road	Station to Station	Description	Type of Construction
SR 120	14+00± to 20+90±	Exist/ Widening	Inlay/ Overlay Construction, Full depth Construction for widening
3.1.120	20+90± to 26+28±	New Alignment and Bridge	Full Depth Construction and Replacement
	26+28± to 32+00±	Exist/ Widening	Inlay/ Overlay Construction, Full depth Construction for widening
All Side Roads	Pavemen	t Evaluation is Excluded fr	om our scope of work

Notation:

Inlay/Overlay Construction = Existing roadway, overlay conditions are acceptable.

Full Depth Construction = Widening, new roadway and/or alignment.

Full Depth Reconstruction = Existing roadway pavement is acceptable for overlay; however, the roadway is not part of the functional roadway. This section can remain in place if desired. Full Depth Replacement = Existing Roadway cannot accommodate overlay due to the existing effective structural number or due to new profile. Extension of the main line Full Depth Construction to the turnouts of the side roads is recommended

4. FULL-DEPTH SECTIONS

The following full-depth pavement structures are recommended for use on this project.

SR 120 Full Depth Design

(With Curb & Gutter) (Station 14+00 to Station 32+00 except bridge)					
PAY ITEM NUMBER	MATERIAL	COURSE	THICKNESS	SPREAD RATE	
402-4510	12.5 mm Superpave including polymer modified AC	Surface	1.50 inches	165 lbs/yd ²	
402-3190	19 mm Superpave	Binder	2.00 inches	220 lbs/yd ²	
402-3121	25 mm Superpave	Asphalt Base	6.00 inches	660 lbs/yd ²	
310-1101	Graded Aggregate Base	Base	12.00 inches	N/A	

5. OVERLAY SECTIONS

We recommend that the existing pavement along the following roadways be milled and inlayed/ overlaid to remove existing cracked asphalt as follows:





- SR 120 from Station 14+00± to Station 20+90± be partially milled 2.00 inches.
- SR 120 from Station 20+90± to Station 32+00± be partially milled 2.00 inches.

SR 120 Mill and Overlay Design*

(With Curb & Gutter) (Station 14+00 to 20+90 and Station 26+28 to 32+00)					
PAY ITEM NUMBER	MATERIAL	COURSE	THICKNESS	SPREAD RATE	
402-4510	12.5 mm Superpave including polymer modified AC	Surface	1.50 inches	165 lbs/yd ²	
402-3190	19 mm Superpave	Binder	2.00 inches	220 lbs/yd²	
402-3121	25 mm Superpave	Asphalt Base	3.00 inches	330 lbs/yd ²	

^{*}Additional quantities (e.g., around sta. 29+38±) should be set up for extra milling depth.

Please refer to Section 11 "Assumptions and Justification" section of the report.

6. PAVEMENT DISTRESSES

Except for the following, no other significant distresses were encountered during the field exploration of this project:

Load Cracking On **SR 120,** predominantly Level 1 with occasional Level 2 load cracking was observed within the evaluated sections.

Block/ Transverse On SR 120, predominantly Level 1 block cracking was observed within the evaluated sections.

7. COPACES/PACES

The "Final Pavement Evaluation" typically includes a pavement surface distress survey utilizing the GDOT Pavement Condition Evaluation System (PACES). However, the project being small and majority being of new construction, PACES study is excluded. The Georgia Department of Transportation conducted PACES rating on the stretch of SR 120 between Mile Marker (MM) 4.94 and MM 5.28. In 2014, the rating for SR 120 for MM 0.0 to MM 5.7 according to the Assistant Area Maintenance Engineer for the Georgia Department of Transportation District 1, Area 1 was 80%.





8. CORES

Cores were recovered from seven (7) separate locations in the travel lanes and turn lanes of this project to determine the thicknesses and condition of the existing pavement sections. The results of the coring operation are tabulated below:

Core/ Sample Number	Location	Station/Direction/ Location	Asphalt Core Length (inches)	Core Condition	Underlying Material Type/ Thickness
C-1	SR 120	Station 14+41 WB, Ln 1, 13' Lt, PW	5.50	Fair, vertical crack from 0.0" to 1.25", Coarse mix from 4.00" to 5.75.	Concrete=7.75", Compacted Soil and Gravel=6"
C-2	SR 120	Station 16+18 EB, Ln 1, 18' Rt, PW	18.00	Good, diagonal crack from 2.5" to 3.5", horizontal crack with some missing asphalt at 14.25" to 15.75".	Compacted Soil and Gravel=6"
C-3	SR 120	Station 18+38 EB, RTL, 43' Rt, DW	7.50	Good, minor (1.5"± long) horizontal crack at 2.5".	GAB=8.5"
C-4	SR 120	Station 19+21 WB, Ln 1, 27.25' Lt, PW	9.00	Good, vertical crack from 0.0" to 1.75".	GAB=18.5"
C-5	SR 120	Station 29+35 EB, RTL, 29.00' Rt, DW	9.00	Good. No visible stresses.	GAB=12"
C-6	SR 120	Station 29+38 WB, Ln 1, 4.50' Lt, DW	21.00	Fair to poor, vertical crack from 0.0" to 3.0", horizontal delamination at 3.0", horizontal delamination with asphalt pieces from 10.5" to 12.5" (may have been resulted from coring activities).	Compacted Soil and Gravel=6"
C-7	SR 120	Station 31+65 EB, Ln 1, 4.00° Rt, DW	10.00	Fair to poor, vertical crack from 0.0" to 2.0", horizontal delamination at 2.0", horizontal delamination between 7.0" and 7.5".	GAB=9.5"

Notation:

DW = Driver's Wheel Path

EB = Eastbound

GAB= Graded Aggregate Base

Ln = Designated Travel Lane

Lt = Left of the existing centerline, direction of travel (lower to higher station)

Rt = Right of the existing centerline, direction of travel (lower to higher station)

RTL = Right Turn Lane

PW = Passengers Wheel Path

WB = Westbound





9. OTHER INFORMATION

- The Soil Survey Summary for this project was not obtainable as of the issuance of this report. The attached pavement designs used the design values recommended in Appendix G and H of the GDOT Pavement Design Manual.
- The attached pavement designs used the design values recommended in the approved GDOT interdepartmental correspondence letter entitled, "Reviewed Summary of Design Traffic Projections Memorandum Document and Design Traffic Diagrams for SR 120/Duluth Highway @ Singleton Creek 1.5 Mi E of Duluth", dated August 14, 2015 and the traffic information provided by Michael Baker International, dated August 11, 2015. See attached **Appendix G** Traffic Data for further details.
- The full-depth design and the mill and inlay/overlay design analyses are attached to this
 report. All designs are based on a computer program named GDOT Pavement Design
 Version 2.0 developed by Georgia Department of Transportation, Pavement Management
 Branch.

Historical Information

The GDOT Geo TRAQS Historical Plans Research Website – Electronic Plans Search was reviewed to determine if any historical construction drawings were obtainable for evaluation. No additional historical information regarding previous pavement overlays, pavement management or construction dates were readily available for review for this project. In addition, United Consulting contacted the GDOT Office of Materials and Research for COPACES and any historical information regarding SR 120. GDOT responded, via telephone, the historical COPACES ratings for the segments requested.

Design Considerations for SR 120

- Number of lanes (in one-direction): 1
- With curb and gutter
- o Provided Traffic Data: A.D.T. (2020): 13,300; (2040): 16,225
- Provided Project Let Date: 2018

TRAFFIC DATA

- A.D.T. (2020): 13,300 (One-Way)
- A.D.T. (2040): 16,225 (One-Way)
- Directional Distribution: 50/50
- Lane Distribution: 100%
- % 24 Hr. Trucks: 8%
- % MU: 1.0%, % SU: 7.0%
- Function Class: Urban Minor Arterial
- Speed Design: ≤ 45 mph
- Terminal Serviceability Index: 2.50
- Soil Support: 2.5





Regional Factor: 1.8

Subgrade Reaction, k = 130 pci

• Mill 2.0 inches of the existing pavement for the project.

10. ADDITIONAL RECOMMENDATIONS

- We recommend a minimum 100 foot tie-in transition for SR 120 at the beginning and ending of the project. In addition, we recommend a minimum tie-in transition extended to the edge of turnouts for the side roads. The tie-in transition will consist of milling 2.00 inches and underlain by overlaying with 12.5 mm Superpave including polymer modified asphalt concrete mix and a 19 mm Superpave asphalt concrete mix.
- New pavements should be constructed flush with all existing and/ or new utility manholes or vaults.
- We recommend staggered joints for each asphalt concrete layer to reduce the potential moisture migration from subgrade soils.
- We recommend the application of a 2 foot wide pavement reinforcement fabric, centered on joints to reduce the potential for crack migration through the new asphalt.
- We recommend milling the asphaltic concrete pavement, as per Section 432 of the Standard Specifications.
- We recommend waterproofing the joints and cracks as the asphalt concrete pavement prior to the overlaying operation, as per Section 445 of the Standard Specifications.
- Full-Depth replacement/construction should be utilized where overlays do not conform to project specification vertical alignment requirements.
- After milling and immediately prior to inlaying/overlaying, we recommend that any surface cracks shall be sealed with a Type M crack sealant, as per Section 407 of the Standard Specifications.

11. ASSUMPTIONS AND JUSTIFICATIONS

• The provided pavement design is based on the traffic information provided by Michael Baker International. The traffic data provided was for a build/ no build for 2020 and 2040. The recommended LET DATE of 2018 plus 2 years indicated a design date for the years 2020 and 2040. The above pavement design used the 2020 and 2040 traffic data for assumption and justifications within this report.





- Based on the plans provided and the core samples taken, mill and overlay conditions are acceptable, if desired.
- Based on the plans provided, for Stations 20+90 to Station 26+28 on SR 120 full depth construction will be required due to the horizontal realignment. United Consulting did not perform pavement evaluation within this area.
- From near Station 14+00± to Station 20+90± and Station 26+28± to Station 32+00±, vertical alignment will be near or at the existing roadway. United Consulting recommend milling the existing surface at least 2.0 inches to remove the vertical load distresses within the existing roadway.
- No information regarding the Mile Marker was available on the website or in our field observations for Northmont Parkway or Staunton Drive.
- The station locations for SR 120 and all roadways associated with this project were not provided or staked in the field by a surveyor. United Consulting determined the approximate location of these stations by using a measuring wheel from the nearest identified stationary object marked on the provided plans.

12. LIMITATIONS

This report is for the exclusive use of the Georgia Department of Transportation (GDOT), its agents, and Michael Baker International, the designers of the project described herein, and may only be applied to this specific project. Our conclusions and recommendations have been prepared using generally accepted standards of Pavement Engineering practice in the State of Georgia and are valid for a period of two years from the issuance of this report. Should the implementation of the recommendations presented in this report be delayed more than two years, re-evaluation of the pavement should be performed. No other warranty is expressed or implied. Our firm is not responsible for conclusions, opinions or recommendations of others. The right to rely upon this report and the data within may not be assigned without UNITED CONSULTING'S written permission.

Our preliminary conclusions and recommendations are based upon design information furnished to us, data obtained from the previously described exploration and testing program and our past experience. They do not reflect variations in the conditions that may be present intermediate of our coring/ borings and in unexplored areas of the project. Should such variations become apparent during construction, it will be necessary to re-evaluate our conclusions and recommendations based upon "on-site" observations of the conditions.





Our conclusions and recommendation are based on out sit reconnaissance, anticipated existing pavement thickness, and our past experience. If the design or location of the project is changed, the recommendations contained herein, must be considered invalid unless our firm reviews the changes and our recommendations are either verified or modified in writing.

UNITED CONSULTING

Reported By: Lonnie Rucker

Reviewed By: Ray E. Halbert, P.E.

QC Reviewed By: Santanu Sinharoy, P.E.

Appendix A – Figures – (1 page)

Figure 1: Site Location Map and Asphalt Coring Location Plan

Appendix B – Project Photographs – (7 pages)

Appendix C – Roadway Photographs – (15 pages)

Appendix D – Example Photographs – (2 pages)

Appendix E – Core Photographs– (6 pages)

Appendix F – Pavement Rating – EXCLUDED

Appendix G – Recommended Pavement Section – (8 pages)

Approved Traffic Diagrams including approval letter (6 pages)

Full Depth Flexible Pavement Design using GAB with Curb and Gutter (1 page)

Inlay/ Overlay with Curb and Gutters – (1 page)

Appendix H – Roadway Survey and Core Properties – (4 pages)

Appendix I - Disc





APPENDIX A

FIGURES (1 PAGE)



SCALE: NTS	DATE: 06/25/2015	PROJECT NO: 2015.0535.01
PREPARED: LR	CHECKED: REH	REVISIONS: 1

S.R. 120 OVER SINGLETON CREEK P.I. No. 132986, Gwinnett County, Georgia

PROJECT LOCATION MAP AND CORING LOCATION PLAN

CLIENT:

MICHAEL BAKER INTERNATIONAL

UNITED CONSULTING

TITLE:

625 Holcomb Bridge Road, Norcross, GA 30071 Tel. 770/209-0029 FAX 770/582-2900 www.unitedconsulting.com



FIG. 1

APPENDIX B

PROJECT PHOTOGRAPHS (7 PAGES)

PHOTOGRAPH LEGEND

Photograph Type	Label Protocol	Project Information
County Number	A three digit number	135
Route Number	A four digit number followed by a two character suffix (i.e., SR 120 = 0120 00)	0120 00 BU = Business 03 = City 00 = CR or SR
Route Code	State or County or other code route	1 = State Highway 2 = County Road 3 = City Street
Direction of Travel	E or W N or S	E = Eastbound W = Westbound N = Northbound S = Southbound
Milepost	MP	MP 4.94 to MP 5.28



135 0120 00 1 W AT STATION 15+00, MP= 4.96 SR 120, WESTBOUND



135 0120 00 1 E AT STATION 15+00, MP= 4.96 SR 120 EASTBOUND



135 0120 00 1 N AT STATION 19+10, MP= 5.03 SR 120, LOOKING NORTH ALONG NORTHMONT PKWY



135 0120 00 1 S AT STATION 19+00, MP= 5.03 SR 120, LOOKING SOUTH ALONG NORTHMONT PKWY



135 0120 00 1 W AT STATION 20+00, MP= 5.05 SR 120 WESTBOUND



135 0120 00 E 1 AT STATION 20+00, MP= 5.05 SR 120 EASTBOUND



135 0120 00 1 W AT STATION 27+00, MP= 5.18 SR 120 WESTBOUND



135 0120 00 1 E AT STATION 27+00, MP= 5.18 SR 120 EASTBOUND



135 0120 00 1 N AT STATION 29+60, MP= 5.23 SR 120, LOOKING NORTH ALONG STAUNTON DRIVE



135 0120 00 1 N AT STATION 29+60, MP= 5.23 SR 120, LOOKING SOUTH ALONG STAUNTON DRIVE



135 0120 00 1 W AT STATION 31+00, MP= 5.26 SR 120 WESTBOUND



135 0120 00 E 1 AT STATION 31+00, MP= 5.26 SR 120 EASTBOUND

APPENDIX C

ROADWAY PHOTOGRAPHS (15 PAGES)

PHOTOGRAPH LEGEND

Photograph Type	Label Protocol	Project Information
County Number	A three digit number	135
Route Number	A four digit number followed by a two character suffix (i.e., SR 120 = 0120 00)	0120 00 BU = Business 03 = City 00 = CR or SR
Route Code	State or County or other code route	1 = State Highway 2 = County Road 3 = City Street
Direction of Travel	E, W, N or S	E = Eastbound W= Westbound N = Northbound S = Southbound
Lane of Travel	A one-digit number LTL RTL ML	1 LTL = Left Turn Lane RTL = Right Turn Lane ML = Merge Lane
With Traffic or Facing Traffic	W or F	W or F
Milepost	MP	MP 4.94 to MP 5.28



135 0120 00 1 E 1 F AT STATION 15+00, MP= 4.96 EASTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 E 1 W AT STATION 15+00, MP= 4.96 EASTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 W AT STATION 15+00, MP= 4.96 WESTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 F AT STATION 15+00, MP= 4.96 WESTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 W RTL W AT STATION 15+00, MP= 4.96 WESTBOUND, RIGHT TURN LANE, WITH TRAFFIC



135 0120 00 1 W RTL F AT STATION 15+00, MP= 4.96 WESTBOUND, RIGHT TURN LANE, FACING TRAFFIC



135 0120 00 1 E ML F AT STATION 20+00, MP= 5.05 EASTBOUND, MERGE LANE, FACING TRAFFIC



135 0120 00 1 E ML W AT STATION 20+00, MP= 5.05 EASTBOUND, MERGE LANE, WITH TRAFFIC



135 0120 00 1 E 1 F AT STATION 20+00, MP= 5.05 EASTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 E 1 W AT STATION 20+00, MP= 5.05 EASTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W LTL W AT STATION 20+00, MP= 5.05 WESTBOUND, LEFT TURN LANE, WITH TRAFFIC



135 0120 00 1 W LTL F AT STATION 20+00, MP= 5.05 WESTBOUND, LEFT TURN LANE, FACING TRAFFIC



135 0120 00 1 W 1 W AT STATION 20+00, MP= 5.05 WESTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 F AT STATION 20+00, MP= 5.05 WESTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 W RTL W AT STATION 20+00, MP= 5.05 WESTBOUND, RIGHT TURN LANE, WITH TRAFFIC



135 0120 00 1 W RTL F AT STATION 20+00, MP= 5.05 WESTBOUND, RIGHT TURN LANE, FACING TRAFFIC



135 0120 00 1 E RTL W AT STATION 27+30, MP= 5.19 EASTBOUND, RIGHT TURN LANE, WITH TRAFFIC



135 0120 00 1 E 1 F AT STATION 27+00, MP= 5.18 EASTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 E 1 W AT STATION 27+00, MP= 5.18 EASTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 W AT STATION 27+00, MP= 5.18 WESTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 F AT STATION 27+00, MP= 5.18 WESTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 E 1 F AT STATION 31+20, MP= 5.26 EASTBOUND, LANE 1, FACING TRAFFIC



135 0120 00 1 E 1 W AT STATION 31+13, MP= 5.26 EASTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W LTL W AT STATION 31+00, MP= 5.26 WESTBOUND, LEFT TURN LANE, WITH TRAFFIC



135 0120 00 1 W LTL F AT STATION 31+00, MP= 5.26 WESTBOUND, LEFT TURN LANE, FACING TRAFFIC



135 0120 00 1 W 1 W AT STATION 31+00, MP= 5.26 WESTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W 1 F AT STATION 31+00, MP= 5.26 WESTBOUND, LANE 1, WITH TRAFFIC



135 0120 00 1 W RTL W AT STATION 31+00, MP= 5.26 WESTBOUND, RIGHT TURN LANE, WITH TRAFFIC



135 0120 00 1 W RTL F AT STATION 31+00, MP= 5.26 WESTBOUND, RIGHT TURN LANE, FACING TRAFFIC

APPENDIX D

EXAMPLE PHOTOGRAPHS (2 PAGES)



Load Distress - Severity Level 1 at Station 14+78, MP=4.95



Load Distress - Severity Level 2 at Station 30+07, MP= 5.24



Block/ Transverse Distress - Severity Level 1 at Station 31+54, MP= 5.27



Block/ Transverse Distress - Severity Level 1 at Station 30+85, MP= 5.26

APPENDIX E

CORE PHOTOGRAPHS (6 PAGES)



CORE C-1, SR 120, Sta. 14+41, Westbound, Lane 1, Passenger Wheel Path, MP= 4.95



CORE C-1, SR 120, Sta. 14+41, Westbound, Lane 1, Passenger Wheel Path, MP= 4.95, showing the other side of the core.



CORE C-2, SR 120, Sta. 16+18, Eastbound, Lane 1, Passenger Wheel Path, MP= 4.98



CORE C-3, SR 120, Sta. 18+38, Eastbound, Right Turn Lane, Driver Wheel Path, MP= 5.02



CORE C-4, SR 120, Sta. 19+21, Westbound, Lane 1, Passenger Wheel Path, MP= 5.04



CORE C-5, SR 120, Sta. 29+35, Eastbound, Right Turn Lane, Driver Wheel Path, MP= 5.23



CORE C-6, SR 120, Sta. 29+38, Westbound, Lane 1, Driver Wheel Path, MP= 5.23



CORE C-6, SR 120, Sta. 29+38, Westbound, Lane 1, Driver Wheel Path, MP= 5.23, showing the other side of the core



CORE C-6, SR 120, Sta. 29+38, Westbound, Lane 1, Driver Wheel Path, MP= 5.23, showing the fragmented portion of the core.



CORE C-6, SR 120, Sta. 29+38, Westbound, Lane 1, Driver Wheel Path, MP= 5.23, showing the top of the core



CORE C-7, SR 120, Sta. 31+65, Eastbound, Lane 1, Driver Wheel Path, MP= 5.27



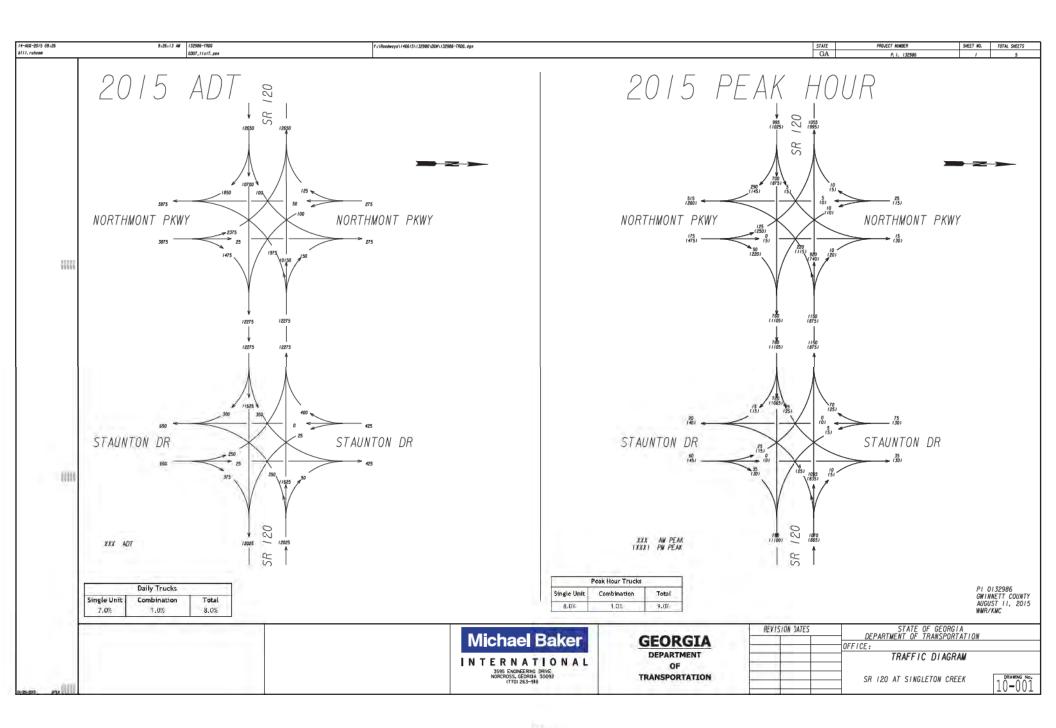
CORE C-7, SR 120, Sta. 31+65, Eastbound, Lane 1, Driver Wheel Path, MP= 5.27, showing the other side of the core

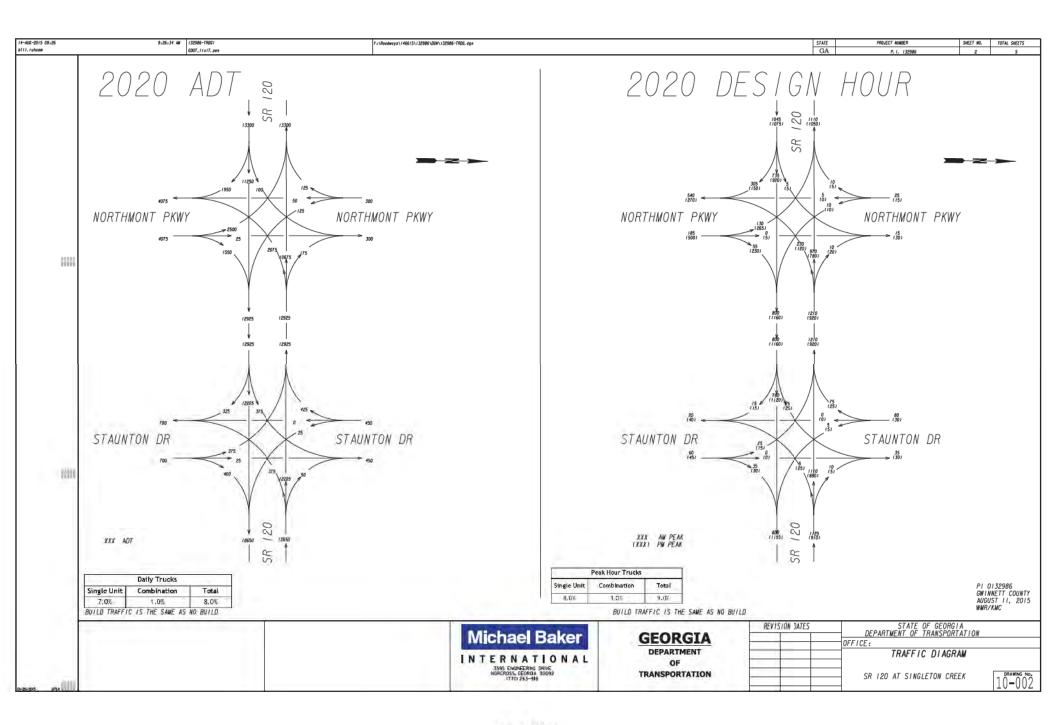
APPENDIX F

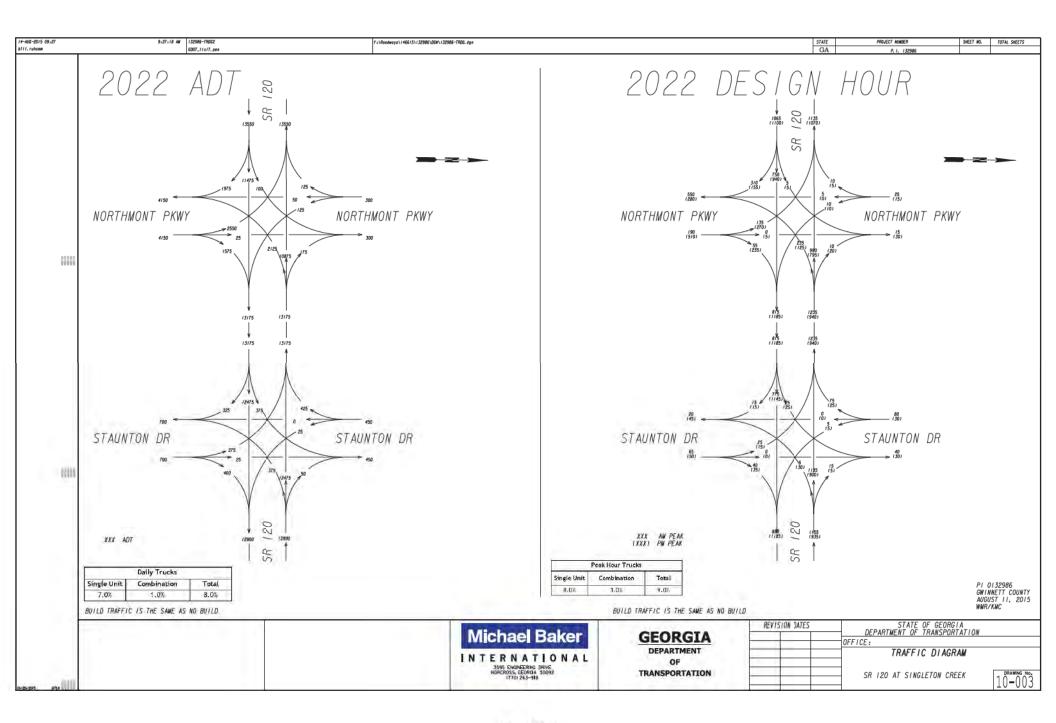
PAVEMENT RATING (EXCLUDED)

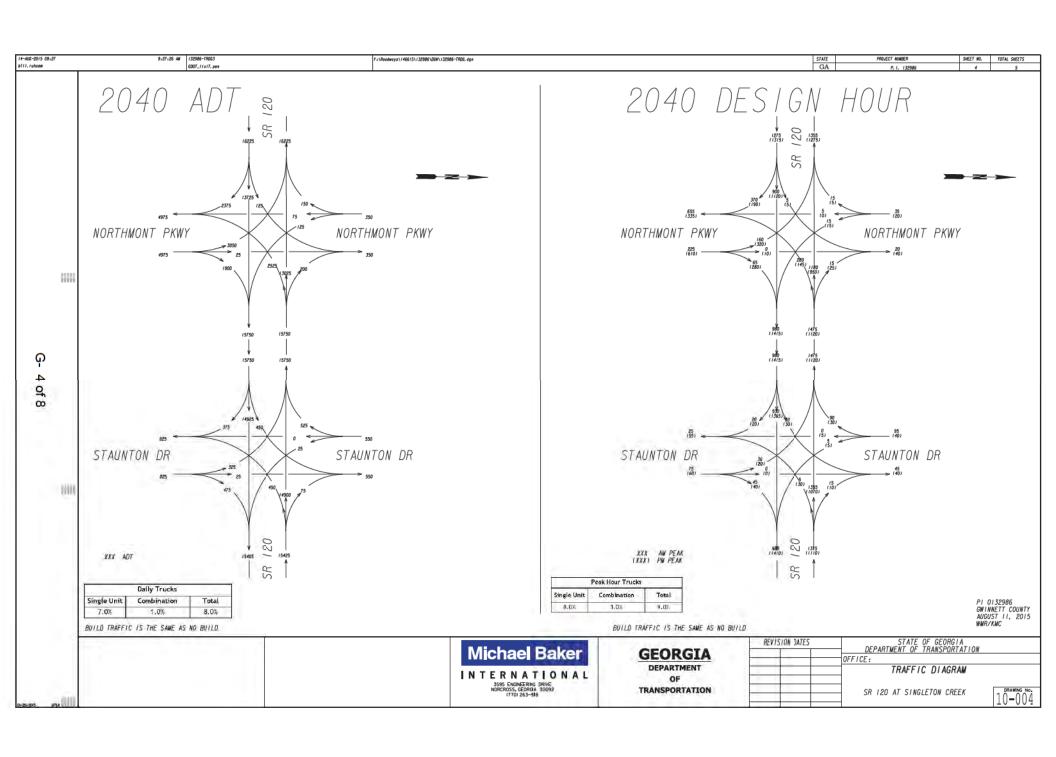
APPENDIX G

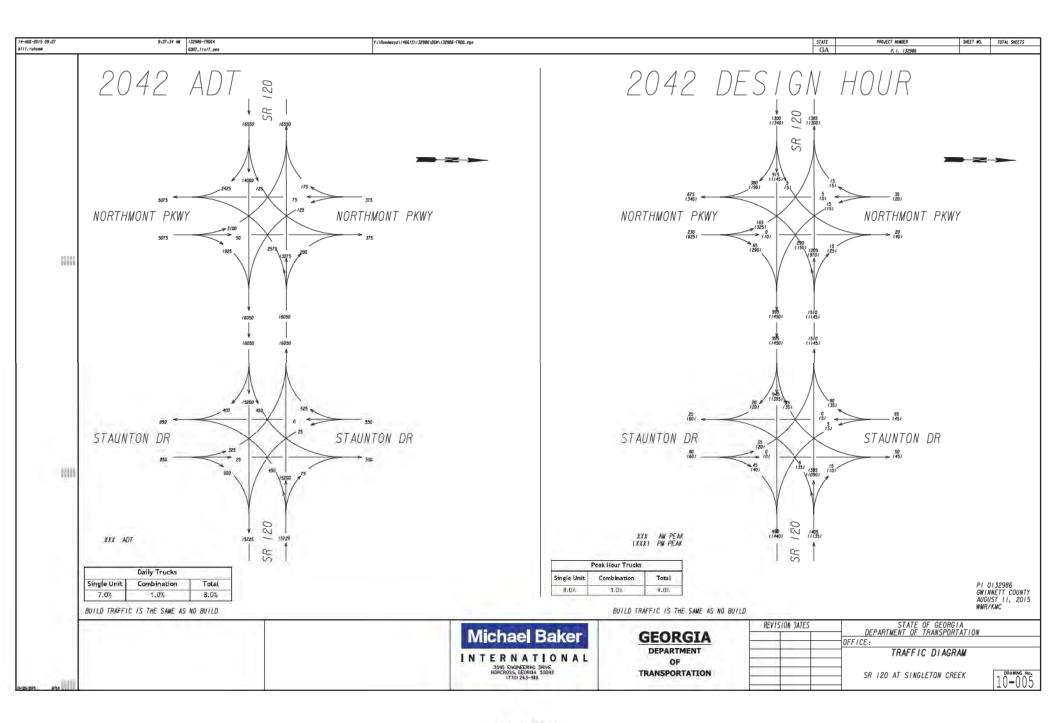
RECOMMENDED PAVEMENT SECTION (8 PAGES)











Department of Transportation State of Georgia

INTERDEPARTMENT CORRESPONDENCE

FILE BRST0-0189-01(030), Gwinnett County OFFICE Planning

P.I. # 132986

DATE August 14, 2015

FROM Cynthia L. VanDyke, State Transportation Planning Administrator

TO Albert Shelby, State Program Delivery Engineer

Attention: Anthony Tate

SUBJECT Reviewed Summary of Design Traffic Projections Memorandum Document

and Design Traffic Diagrams for SR 120/DULUTH HIGHWAY @

SINGLETON CREEK 1.5 MI E OF DULUTH

Per request, we have reviewed the consultant's summary of design traffic projections memorandum document and design traffic diagrams for the above project. Based on the information furnished, we find the summary of design projections traffic memorandum document and the design traffic projections to be satisfactory, and approve the summary of design traffic projections memorandum document and the design traffic volume.

If you have any questions concerning this information please contact Andre Washington at (404) 631-1925.

CLV/AMW

Flexible Pavement Design Analysis							
PI Number	0132986	County(s)	Gwinnett				
Project Number		Design Name	Full Depth with GAB				
Project Description	SR 120 Over Singleton Cre	eek					

Traffic Data (AADTs are one-way)						Miscellaneous Data	a
Initial Design Year	2020	Initial AADT, VPD	13,300	24 Hour Truck %	8.00	Lanes in one direction	1
Final Design Year	2040	Final AADT, VPD	16,225	SU Truck %	7.00	Curb & Gutter/Barrier	Yes
		Mean AADT, VPD	14,763	MU Truck %	1.00		

		Design Data			
Lane Distribution Factor (%)	100.00	Soil Support Value	2.50	Single Unit ESAL	0.40
Terminal Serviceability Index	2.50	.50 Regional Factor	1.80	Multiple Unit ESAL	1.50
		User Defined 18-KIP ESAL	0.00	Calculated 18-KIP ESAL	0.54
Non-Standard Value Comment	,				

Design Loading (Calculated 18-KIP ESAL)									
Mean AADT, VPD	LDF (%)	Vehicle Type	Volume (%)	ESAL Factor	Daily ESAL				
2122	100.00	Single Unit Truck	7.00	0.40	414				
14,763	100.00	Multi Unit Truck	1.00	1.50	222				
				Total Daily ESALs	636				
			Total	Design Period ESALs	4,642,800				

		Proposed Flexible Full D	epth Pavement Structure		
Course		Material	Thickness (inches)	Structural Coefficient	Structural Value
Course 1	12.5 mm Superpave, Po	olymer Modified	1.50	0.4400	0.66
Course 2	19 mm Superpave		2.00	0.4400	0.88
C 2	25		1.00	0.4400	0.44
Course 3	25 mm Superpave		5.00	0.3000	1.50
Course 4 Graded Aggregate Base		12.00	0.1600	1.92	
Required S	N 5.74	Proposed pavement is 5	5.87% Underdesigned	Proposed SN	5.40

-				
Design Remarks	Full Depth with GAB			

Prepared By		8/28/2015 1:38 PM
	UC	Date
Recommended By		
	State Roadway Design Engineer	Date
approved By		
A	State Pavement Engineer	Date

Flexible Pavement Design Analysis							
PI Number	0132986	County(s)	Gwinnett				
Project Number		Design Name	Overlay				
Project Description	SR 120 Over Singleton C	Creek					

Traffic Data (AADTs are one-way)						Miscellaneous Data	a
Initial Design Year	2020	Initial AADT, VPD	13,300	24 Hour Truck %	8.00	Lanes in one direction	1
Final Design Year	2040	Final AADT, VPD	16,225	SU Truck %	7.00	Curb & Gutter/Barrier	Yes
		Mean AADT, VPD	14,763	MU Truck %	1.00	Milling Depth (inches)	2.00

Design Data										
Lane Distribution Factor (%)	100.00	Soil Support Value	2.50	Single Unit ESAL	0.40					
Terminal Serviceability Index	2.50	2.50 Regional Factor	1.80	Multiple Unit ESAL	1.50					
		User Defined 18-KIP ESAL	0.00	Calculated 18-KIP ESAL	0.54					
Non-Standard Value Comment										

		Design Loading (Calc	culated 18-KIP ESAL)	
Mean AADT, VPD	LDF (%)	Vehicle Type	Volume (%)	ESAL Factor	Daily ESAL
44.50	100.00	Single Unit Truck	7.00	0.40	414
14,763	100.00	Multi Unit Truck	1.00	1.50	222
				Total Daily ESALs	636
			Total 1	Design Period ESALs	4,642,800

Proposed Flexible Overlay Pavement Structure									
Course		Material	Thickness (inches)	Structural Coefficient	Structural Value				
Overlay 1	12.5 mm Superpave, Polymer Modified		1.50	0.4400	0.66				
Overlay 2	19 mm Superpave		2.00	0.4400	0.88				
Orosalari 2	25 mm Cran amazza	4	1.00	0.4400	0.44				
Overlay 3	25 mm Superpave	mm Superpave		0.3000	0.60				
Existing 1	Asphaltic Concrete		5.50	0.3000	1.65				
Existing 2	Graded Aggregate Base		8.50	0.1600	1.36				
Required SN	5.74	Proposed pavement is 2	2.56% Underdesigned	Proposed SN	5.59				

22/200			_
Design Remarks	Overlay		

Prepared By		8/28/2015 1:43 PM
	UC	Date
Recommended By		
	State Roadway Design Engineer	Date
Approved By		
A 100 A	State Pavement Engineer	Date

APPENDIX H

ROADWAY SURVEY AND CORE PROPERTIES (4 PAGES)

APPENDIX H ROADWAY DESIGNATION

For **SR 120**, the roadway designation is considered an east-west oriented roadway. Travel lanes are designated with numbers. Lane 1 = Eastbound (EB), Westbound (WB), Inside Lane closest to the centerline of the existing roadway. Left Turn Lane (LTL) is to the left of Lane 1 in the direction of travel, and it separates eastbound and westbound travel lanes close to the intersections. Right Turn Lane (RTL) is the outside lane, closest to the right edge of the pavement.

EXISTING PAVEMENT SURVEY

This project consisted of evaluation of the existing roadway and shoulders for the realignment/ improvement of **SR 120 across Singleton Creek.** The total length of the existing pavement evaluation sections of the project was approximately 1,800 feet. This project began at Station 14+00, Mile Marker (MM) = 4.94. The project continues in an eastbound direction to Station 32+00, MM 5.28. The station locations and all roadways associated with this project were not provided or staked in the field by a surveyor. United Consulting determined the approximate location of these stations by using a measuring wheel from the nearest identified stationary object marked on the provided plans.

SR 120

From: Station $14+00\pm$ to Station $20+90\pm$.

The existing pavement/alignment consists of flexible asphalt concrete pavement with two (2) main travel lanes. There is one (1) eastbound and one (1) westbound non-divided travel lanes, and a left turn lanes and a right turn lanes in the areas near the intersection with Northmont Parkway.

Pavement Conditions: Fair to Good. The field observation findings rated the existing roadway conditions as follows: Severity rating, level 1 load cracking and level 1 block/transverse cracking were observed within the evaluated segmented area. The width of the main travel lanes for the section of roadway ranged from 11.5 feet to 13 feet.

Shoulder/ Structure and Drainage Conditions: The unpaved shoulder width varied from 1 foot to 10+ feet depending on location. Shoulders appeared to be well maintained. Concrete curb and gutter existed in the areas near the intersections along with two storm water catch basins.

From: Station 20+90± to Station 26+28±.

The proposed new horizontal alignment travel south of the existing roadway and therefore no pavement evaluation was performed on this section of roadway.

From: Station $26+28\pm$ to Station $32+00\pm$.

The existing pavement/alignment consists of flexible asphalt concrete pavement with two (2) main travel lanes. There is one (1) eastbound and one (1) westbound non-divided travel lanes, and a left turn lanes and right turn lanes in the areas near the intersection with Staunton Drive.

Pavement Conditions: Fair to Good. The field observation findings rated the existing roadway conditions as follows: Severity rating, level 1 and level 2 load cracking and level 1 block/transverse cracking were observed within the evaluated segmented area. The width of the main travel lanes for the section of roadway ranged from 11.5 feet to 12.5 feet.

Shoulder/ Structure and Drainage Conditions: The unpaved shoulder width varied from 1 foot to greater than 10 feet depending on location. Shoulders appeared to be well maintained. Concrete curb and gutter existed in the areas near the intersections along with two storm water catch basins.

Side Roads

No pavement evaluation was performed on the side roads during this survey.

ROADWAY EVALUATION

Note: Distresses <u>not listed</u> within the following roadway evaluated segmented areas were not observed during this survey.

Rutting

On **SR 120,** rutting measurements were evaluated at various locations. Rutting measurements ranged from a minimum of zero inches to a maximum of $\frac{1}{8}$ inches near the intersections with Northmont Parkway and Staunton Drive within the evaluated sections to be retained. Measurements are provided to the nearest $\frac{1}{8}$ inch increments.

Designation for wheel paths are as follows: Drivers Wheel Path = DW, Passenger Wheel Path = PW, Eastbound = EB, Westbound = WB, Right Turn Lane = RTL, Left Turn Lane = LTL.

SR 120

511												
Station	V	/ B	V	/ B	V	/B	E	В	E	В	E	В
	R	ΓL	La	ne 1	L	ΓL	Lī	ΓL	Lar	ie 1	R	ΓL
	PW	DW	PW	DW	PW	DW	DW	PW	DW	PW	DW	PW
14+41±	0	0	1/8	0					0	0		
16+18±			0	0					0	0		
18+38±			0	0			0	0	1/8	1/8	0	0
19+21±	0	0	0	1/8	0	0			0	0		
19+49±	0	0	0	0	0	1/8			0	0		
29+35±			0	0			0	1/8	0	0	0	0
29+38±			0	0			0	0	0	0	0	0
30+21±	0	0	0	0	0	1/8			0	0		
31+65±			0	0	1/8	0			0	0		

Load Cracking

On SR 120, Level 1 to Level 2 load cracking was observed from the following evaluated sections:

Station to Statio	Load Cracking (%)				
Evaluated Test Section	Representing	Level 1	Level 2	Level 3	Level 4
14+00 – 15+00 WB, Lane 1	14+00± to 20+90±	90	0	0	0
14+00 – 15+00 EB, Lane 1		70	0	0	0
30+00 - 31+00 WB, Lane 1	26+28± to 32+00±	60	5	0	0
30+00 - 31+00 WB, Left Turn Lane		55	0	0	0
30+00 - 31+00 EB, Lane 1		75	0	0	0

Block/Transverse Cracking

On SR 120, Level 1 block/transverse cracking was observed from the following evaluated sections:

Station to Statio	Block/ Transverse Cracking (%)				
Evaluated Test Section	Representing	Level 1	Level 2	Level 3	
14+00 – 15+00 WB, Lane 1	14+00± to 20+90±	35	0	0	
14+00 - 15+00 EB, Lane 1	30.41=0.21	0	0	0	
30+00 - 31+00 WB, Lane 1	26+28± to 32+00±	5	0	0	
30+00 - 31+00 WB, Left Turn Lane	ar ar inter	60	0	0	
30+00 - 31+00 EB, Lane 1		20	0	0	

ASPHALT CORE PROPERTIES LENGTH/TYPE

Core/ Sample Number	Location	Station/Location/ Direction	Asphalt Core Length (ins)	Asphalt Type/ Depth (ins.)
				Top to Bottom
C-1	SR 120	Station 14+41 WB, Ln 1, 13' Lt, PW	5.50	F=2.00, E=1.25, F=2.25
C-2	SR 120	Station 16+18 EB, Ln 1, 18' Rt, PW	18.00	F=1.00, F=1.25, E=1.25, F=1.25, E=3.00, B=2.75, B=1.50, B=6.00
C-3	SR 120	Station 18+38 EB, RTL, 43' Rt, DW	7.50	F=1.00, F=1.50, B=0.75, B=2.00, B=2.25
C-4	SR 120	Station 19+21 WB, Ln 1, 27.25' Lt, PW	9.00	E=1.25, F=1.00, F=1.25, E=2.00, B=3.50
C-5	SR 120	Station 29+35 EB, RTL, 29.00° Rt, DW	9.00	F=1.00, E=1.25, B=2.75, B=4.00
C-6	SR 120	Station 29+38 WB, Ln 1, 4.50° Lt, DW	21.00	E=1.50, F=1.50, F=2.00, E=1.00, E=1.50, E=2.50, E=3.00, B=3.00, B=3.00, B=2.00
C-7	SR 120	Station 31+65 EB, Ln 1, 4.00' Rt, DW	10.00	F=2.00, E=2.00, F=1.25, E=2.25, E=1.00, B=1.50

Notation:

DW = Driver's Wheel Path

EB = Eastbound

Ln = Designated Travel Lane

Lt = Left of the existing centerline, direction of travel (lower to higher station)

PW = Passengers Wheel Path

Rt = Right of the existing centerline, direction of travel (lower to higher station)

RTL = Right Turn Lane

WB = Westbound

Asphalt Type:

F= Asphalt mix with < 3/8 inch stone size matrix

E= Asphalt mix with $< \frac{3}{4}$ inch stone size matrix

Bin = Binder = Black mix

B=Base = Asphalt mix with $> \frac{3}{4}$ inch stone size matrix

APPENDIX I

Concept Team Meeting Minutes P.I. 132986

Date: December 18, 2015 @ 10:00 a.m.
Location: GDOT District 1 large conference room

RE: P.I. 132986 – SR 120 over Singleton Creek – Gwinnett County

Attendees: See attached list

Welcome:

Anthony Tate welcomed everyone and gave a brief introduction of the project. This is an old project that is being rebooted. Several years ago it went to final plans but was then shelved. Now it is back at concept stage to validate the concept and proceed through letting.

Introductions:

Everyone introduced themselves and was requested to fill out the sign in sheet

Project Identification:

Anthony Tate gave the project specifics and outlined the schedule:

PFPR - November 2016 Environmental Approval - April 2017 R/W Authorization - June 2017 FFPR - December 2017 Letting - June 2018

Concept Report:

Ben Clopper revised the concept report and invited attendees to stop him if items needed additional clarification

- Project Justification: Existing bridge was built in 1938. Sufficiency rating of 58.7 on 1/31/2014. Generally satisfactory condition but cracking and spalling on edge beams, bent 2 and abutment 4. Designed using H-15 vehicles, which is below current design standards. Unknown foundation type so there is a risk of scour. The Bridge Office has recommended the bridge for replacement for those two reasons.
- Existing conditions: Two 12-foot lanes, variable width paved shoulders. Existing bridge has no shoulders. Signalized intersection west of the bridge. There is some existing sidewalk, though on east side it is without C&G. The property along the north side of the bridge is protected by a restrictive covenant by the USACE.
- Approved Traffic: 2015 ADT: 25,300, Open (2020) ADT: 26,6600, Design (2040) ADT: 32,420
- Functional Classification: Urban Minor Arterial
- Pavement Evaluation:
 - o Full Depth: 1.5", 2", 6", 12" GAB
 - Mill/Inlay: 1.5", 2" 3" (remove cracking)
- Structures were discussed by George Manning:
 - o Existing Bridge: 75' long, 3 span, 26.5' wide with two-12' lanes and no shoulders
 - Proposed Bridge: 150' long, 3 span, 56.4' wide with two-12' lanes, 14' center turn lane,
 2' gutters and 6' raised sidewalk
 - Proposed bridge will be raised from ~904.5 to ~909.0 to get 2' clearance over 50' Yr flood elevation (902.78)

- Proposed Design Features were reviewed by Ben Clopper:
 - Two 12-foot lanes with a 14-foot center turn lane and 16' border area including sidewalks
 - 45 mph design speed which matches existing posted speed limit.
 - Design Vehicle is a WB-40 per Design Policy Manual (DPM). Comment from Office of Design Policy and Support (DP&S) concerning WB-67 given 8% truck traffic. May be useful for south leg of Northmont Pkwy, but all other sideroads are residential.
 - Discussion about a design variance for Median Usage: DPM calls for a 24' median given the Functional Classification and Design Speed. However the rest of SR 120 is only 2 lanes for 1 mile to east and through Duluth and Johns Creek almost to Alpharetta to the west. This is a bridge project so it would be desirable to get the full future width in place, but there is nothing programmed and future widening seems unlikely.
 - Justin Lott agreed that a design variance is not needed if there is no need to go to four lanes.
 - Justin will investigate and confirm that there are no plans to widen SR 120. [This
 was completed and no programmed projects were identified]
 - o 1 signalized intersection at SR 120 at Northmont Pkwy
 - No lighting
 - No detour required, staged construction. No nearby state routes are available for a detour
- Design Exception (DE)/Design Variance (DV):
 - o No DE required
 - DV may be required for median suggested by DP&S. Based on the discussions at the meeting the attendees did not think a DV was necessary.

- Utilities:

- SUE QL-B is almost completed and there are a lot of utilities in the project area. The SUE was not available prior to submitting the Concept for the Concept Team Meeting, so utilities were not taken into account, but can be discussed now.
- o Include:
 - 48" water on south side
 - 12" (new) & 4" gas on south side
 - Fiber and multi-duct telephone on south side
 - Overhead electric and telephone on south side
 - 16" water on north side
 - Buried electric on north side
 - Multi-duct telephone on north side
 - Sanitary sewer along creek
- District has been working on a Utility Cost Estimate. It is not available at this time but it will be included in the Concept Report when it is ready
- o All utilities appear to be located within the existing R/W except for the new 12" gas line and overhead electric/phone on the south side of the road
- The bridge can be designed to minimize impacts to utilities. The problem will be maintaining existing utilities underneath the realigned roadway. Utility relocations will be expensive if they are necessary for the large utilities.
- Public Interest Determination (PID). The need for a PID was discussed and the District
 Utilities Office will review and provide input to the project manager

- David Wagoner stated that AT&T would like to retain the duct bank on south side. It contains many cables and would be very costly to move. He did not think it would be a problem to maintain it underneath the new roadway because it is expected that it is located at a depth below where any work would be done. Lynn Palmer expressed concern about access to the line. David said they wouldn't need access because of the proximity of manholes along the project corridor. That line is a trunk line and local distribution is up on poles (overhead).
- o Tasheena Spearman requested more details related to the placement of the bridge relative to the 24" sanitary sewer. Ben Clopper stated that the manhole on this line south of the bridge will be impacted. Tasheena said she would send some details to the engineer about what will be required for replacing the manhole, cut, etc.
- Ben Clopper stated that Pothole testing (QL-A) will be performed later in the design process. David Wagoner asked if the utility owners can we get QL-A before the first submittal? Ben Clopper said QL-A won't be done until after the utility impact plans, generally in Final Plans. First submission is a verification submittal of the SUE plans
- o John Gay stated that Georgia Power has a relocation already designed through this area and may be able to use those plans when the time comes.

- R/W:

- o Existing varies 80-120'
- o Proposed varies 100-190'
- o Estimate 10 parcels affected with no displacements
- R/W office is working on a cost estimate and it will be included in the Concept Report when it is received.

- Roundabout:

- A roundabout was considered but was determined to be outside of the scope of this bridge replacement project.
- Context Sensitive Solutions:
 - o None currently included
- Environmental: A summary was provided by Paul Condit
 - MS4 Compliance (by Ben Clopper): The concept MS4 study included in the Concept Report shows that there are five drainage areas along the corridor, but only the one in the northeast quadrant of the bridge will require post construction BMPs. There is sufficient existing R/W at this location to install the post construction BMPs. The other drainage areas either have reduced pavement areas or the installation of permanent BMPs would require residential displacements.
 - o A Categorical Exclusion (CE) is the expected NEPA document
 - A Clean Water Act Section 404 Permit will be required and a Buffer Variance may be necessary. NPDES and FEMA coordination is required
 - Ecology 3 buffered waters and 2 wetlands. No suitable habitat for T&E species, including aquatics. Property to north has a permanent restrictive covenant for wetland preservation, and reversing this would be time consuming and costly. Extinguishment of the restrictive covenant would require a new Section 404 Individual Permit for the original impacts, and the compensatory mitigation would have to be provided at a 2:1 ratio for the current owner of the property, the Bentwood Homeowners Association.
 - History & Archaeology Surveys have been completed and no resources identified.
 - Elliot Robertson asked who is the ecologist that is reviewing the ecology study? Paul Condit replied that he did not know, he did not think one had been assigned yet. Anthony Tate stated he thought it was Christina Schmidt.

- Elliot Robertson asked what would be the change in elevation of the bridge. George Manning answered about 4 feet. Elliot reminded the team that this may need to be taken into account for the noise study. Paul Condit replied that Baker will look at the Environmental Procedures Manual to ensure the criteria are followed for noise study purposes.
- Air/Noise Exempt from conforming plan because of project type; however, screenings are required
- o Public Involvement None required or expected
- Construction:
 - o None noted in Draft CR but Utilities are probably going to be an issue
- Coordination
 - This is an old project, ICTM was held on 6/5/2002 and CR was approved on 2/11/2003.
 The consultant team was asked to relook at Concept and provide updated Concept
 Report in new format instead of just making a revision.
 - Michael Baker International is responsible for Concept Development, Design and Environmental Studies.
 - o GDOT responsible for other activities.
- Costs
 - o Construction \$2.5 million
 - o Mitigation: \$50k
 - Waiting on Util and R/W
- Other Alternatives
 - No Build does not meet project need
 - Replace to north no room because of restrictive covenant, longitudinal impacts to one stream and two buffers
 - Replace on existing alignment cannot stage due to bridge needing to be raised 4.5'.
 No nearby State Routes are available for detour

Concept Layout

Ben Clopper reviewed the Concept Layout

- SR 120 is being realigned to south. Long horizontal curve from west of Northmont across bridge, allows the superelevation to be constant through bridge
- Vertical alignment has sag curves on either side of bridge with low point on west side, off the bridge and minimal grade across bridge
- Locations of wetlands and waters are shown on the plans. The property with the restrictive covenant will be identified.
- The side streets maintain their existing lane configuration

Project Risks:

Anthony Tate led a discussion on project risks using the Comprehensive Risk Assessment for Transportation (CRAFT) tool. The heat map is attached.

Public Involvement Plan:

No public involvement is require for this project.

Comments from attendees:

- The utility companies requested to receive submissions as soon as possible. Ben Clopper replied that the SUE subconsultant was completing the QL-B plans now and the utility owners should receive plans for verification early next year.
- Justin Lott confirmed that there was no super elevation (SE) transition on the bridge
- Justin Lott asked about the maximum proposed SE rate shown in the Concept Report of 6%. Ben Clopper replied that this was to match the existing SE on SR 120 and that this would be noted in the Concept Report.
- Justin Lott suggested including the form for contingency costs so this can be captured in the estimate. Anthony Tate will provide this form to Ben Clopper
- John Gay asked when design plans will be available for utility companies. Ben Clopper stated that currently the consultant is only scoped through Concept plans but is currently negotiating for preliminary design. Based on the schedule preliminary plans would be available by the middle of 2016.

Field Visit:

The field visit was attended by Anthony Tate, Elliot Robertson, Ben Clopper, Paul Condit, George Manning and Bill Ruhsam. The relation of the proposed bridge to existing utilities was discussed. High traffic volumes were noted.

Attachments:

Sign In Sheet Agenda CRAFT tool heat map

Sign In Sheet

Concept Team Meeting

PI 132986 - Gwinnett County

SR 120 over Singleton Creek

12/18/2015

District 1 Office, Gainseville, GA

Name	GDOT Office/Company	Phone	Email
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Lynn Palmer	GDOT - Utilities	770-531-57	52 jlpalmer@dot.ga.gov
JOHN GAY	GPC	404-29/-0622	2 JCGAY@ SONTHERNOO, COM
Justin Lott	GDOT - DI	1770-531-5745	jlott@dot.ga.gov



CONCEPT TEAM MEETING AGENDA For PI 132986 - Gwinnett County

Monday December 18, 2015

10:00 a.m.

Meeting Location: District 1 Office large conference room located at

2505 Athens Highway, Gainesville, GA 30507

- 1. Welcome Anthony Tate, GDOT Project Manager
- 2. Sign-in sheet
- 3. Attendee (self) Introduction
 - a. Project Identification Georgia Department of Transportation (GDOT)
 - b. Project Name: SR 120/DULUTH HIGHWAY @ SINGLETON CREEK 1.5 MI E OF DULUTH
 - c. Project County: Gwinnett County
 - d. Project Identification Number: 132986-
- 4. Schedule Anthony Tate, GDOT Project Manager
- 5. Review Concept Report Design Team
- 6. Review Concept Layout Design Team
- 7. Assess Project Risks Project Team
- 8. Review Public Involvement Plan (if applicable) Project Team
- 9. Comments/questions (from attendees in the following order)
 - a. Local Government Officials
 - State
 - County
 - City
 - b. Office of Design Policy and Support
 - c. Office of Planning
 - d. Office of Financial Management
 - e. Office of Engineering Services
 - f. Office of Traffic Operations
 - g. Office of Environmental Services
 - h. District Preconstruction
 - i. Office of Right of Way
 - j. Office of Construction
 - k. GDOT Office of Utilities
 - I. Individual Utility Companies (in attendance)
 - n. Other attendees

Note: Project Site Visit to follow concept team meeting

Heat MAP

Bridge Design	Construction	Design Policy	District	Environmental	OMAT	Project Management	Roadway Design	Right Of Way	Traffic Operation	Utilities	Risk Legend
Hydraulic Issues.	Constructability Issues.	Survey Availability Issues.	Local Government Support.	Major Natural Environment Issues.	Project is at Areas with less than Desirable Soil.	Funding Issues.	Geometric Issues.	Project in Residential Area.	Safety Issues.	Railroad Involvement.	Low
Structural or Foundation Issues.	Access Issues.	Erosion Control Issues.	Local Stakeholder (citizens) Support.	Major Human Environment Issues.	Pavement Design Issues.	Schedule Issues.	Potential Drainage Issues.	Project in Commercial Area.	Traffic Signal Justifications or Permits.	Major Utilities.	Medium Low
Constructability Issues.	Issues with Payment.	MS4 Issues.	Coordination Among different Entities.	Significant Coordination Issues.		Scope Issues.	Traffic Analysis or Capacity Issues.	Access Issues in the Project Corridor.	New Equipment.	Relocation of Major Utilities.	Medium
Environmental Issues.				Significant Time Constraints for Studies or Permits.			Utility Conflict Issues.	Displacement Issues in the Project Corridor.		Known Utility Coordination Issues.	Medium High
				Environmental Impact Statement (EIS).			Staging or Constructability Issues.	Properties with Potential Contaminated Soils.		SUE or PID.	High

Environmental Issues